# JDT

# **700MHZ, CYRSTAL-TO-3.3V DIFFERENTIAL LVPECL FREQUENCY SYNTHESIZER**

*ICS8432-51*

# **GENERAL DESCRIPTION**

The ICS8432-51 is a general purpose, dual output Crystal-to-3.3V Differential LVPECL High Frequency Synthesizer. The ICS8432-51 has a selectable REF\_CLK or crystal input. The VCO operates at a frequency range of 250MHz to 700MHz. The VCO frequency is programmed in steps equal to the value of the input reference or crystal frequency. The VCO and output frequency can be programmed using the serial or parallel interface to the configuration logic. The low phase noise characteristics of the ICS8432-51 make it an ideal clock source for Gigabit Ethernet, Fibre Channel 1 and 2, and Infiniband applications.

# **FEATURES**

- Dual differential 3.3V LVPECL outputs
- Selectable crystal oscillator interface or LVCMOS/LVTTL REF\_CLK
- Output frequency range: 31.25MHz to 700MHz
- Crystal input frequency range: 12MHz to 25MHz
- VCO range: 250MHz to 700MHz
- Parallel or serial interface for programming counter and output dividers
- RMS period jitter: 3.5ps (maximum)
- Cycle-to-cycle jitter: 25ps (maximum)
- 3.3V supply voltage
- 0°C to 70°C ambient operating temperature
- Available in both standard (RoHS 5) and lead-free (RoHS 6) packages
- Replaces the ICS8432-01



# **BLOCK DIAGRAM PIN ASSIGNMENT**



#### **FUNCTIONAL DESCRIPTION**

*NOTE: The functional description that follows describes operation using a 25MHz crystal. Valid PLL loop divider values for different crystal or input frequencies are defined in the Input Frequency Characteristics, Table 5, NOTE 1.*

The ICS8432-51 features a fully integrated PLL and therefore, requires no external components for setting the loop bandwidth. A fundamental crystal is used as the input to the on-chip oscillator. The output of the oscillator is fed into the phase detector. A 25MHz crystal provides a 25MHz phase detector reference frequency. The VCO of the PLL operates over a range of 250MHz to 700MHz. The output of the M divider is also applied to the phase detector.

The phase detector and the M divider force the VCO output frequency to be M times the reference frequency by adjusting the VCO control voltage. Note that for some values of M (either too high or too low), the PLL will not achieve lock. The output of the VCO is scaled by a divider prior to being sent to each of the LVPECL output buffers. The divider provides a 50% output duty cycle.

The programmable features of the ICS8432-51 support two input modes to program the M divider and N output divider. The two input operational modes are parallel and serial. *Figure 1* shows the timing diagram for each mode. In parallel mode, the nP\_LOAD input is initially LOW. The data on inputs M0 through M8 and N0 and N1 is passed directly to the M divider and N output divider. On the LOW-to-HIGH transition of the nP\_LOAD input, the data is latched and the M divider remains loaded until the next LOW transition on nP\_LOAD or until a serial event occurs. As a result, the M and N bits can be hardwired to set the M divider and N output divider to a specific default state that will automatically occur during power-up. The TEST output is LOW when operating in the parallel input mode. The relationship between the VCO frequency, the crystal frequency and the M divider is defined as follows: fVCO = fxtal x M

The M value and the required values of M0 through M8 are shown in Table 3B, Programmable VCO Frequency Function Table. Valid M values for which the PLL will achieve lock for a 25MHz reference are defined as  $10 \le M \le 28$ . The frequency out is defined as follows:  $FOUT = \frac{fVCO}{N} = fxtal \times \frac{M}{N}$ 

Serial operation occurs when nP\_LOAD is HIGH and S\_LOAD is LOW. The shift register is loaded by sampling the S\_DATA bits with the rising edge of S\_CLOCK. The contents of the shift reg-ister are loaded into the M divider and N output divider when S\_LOAD transitions from LOW-to-HIGH. The M divide and N output divide values are latched on the HIGH-to-LOW transition of S\_LOAD. If S\_LOAD is held HIGH, data at the S\_DATA input is passed directly to the M divider and N output divider on each ris-ing edge of S\_CLOCK. The serial mode can be used to program the M and N bits and test bits T1 and T0. The internal registers T0 and T1 determine the state of the TEST output as follows:





**FIGURE 1. PARALLEL & SERIAL LOAD OPERATIONS**

**\*NOTE:** The NULL timing slot must be observed.

#### **TABLE 1. PIN DESCRIPTIONS**



NOTE: *Pullup* and *Pulldown* refer to internal input resistors. See Table 2, Pin Characteristics, for typical values.

#### **TABLE 2. PIN CHARACTERISTICS**





**TABLE 3A. PARALLEL AND SERIAL MODE FUNCTION TABLE**

NOTE:  $L = LOW$ 

 $H = HIGH$  $X = Don't care$ 

 $\uparrow$  = Rising edge transition  $\downarrow$  = Falling edge transition



#### **TABLE 3B. PROGRAMMABLE VCO FREQUENCY FUNCTION TABLE**

NOTE 1: These M divide values and the resulting frequencies correspond to crystal or TEST\_CLK input frequency of 25MHz.

**TABLE 3C. PROGRAMMABLE OUTPUT DIVIDER FUNCTION TABLE**

<b>Inputs</b>			<b>Output Frequency (MHz)</b>		
N1	N <sub>0</sub>	N Divider Value	<b>Minimum</b>	<b>Maximum</b>	
			250	700	
			125	350	
			62.5	175	
			31.25	87.5	

#### **ABSOLUTE MAXIMUM RATINGS**



NOTE: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These ratings are stress specifications only. Functional operation of product at these conditions or any conditions beyond those listed in the *DC Characteristics* or *AC Characteristics* is not implied. Exposure to absolute maximum rating conditions for extended periods may affect product reliability.

### **TABLE 4A. POWER SUPPLY DC CHARACTERISTICS,**  $V_{CC} = V_{CCO} = 3.3V \pm 5\%$ **,**  $T_A = 0^{\circ}C$  **to 70°C**

<b>Symbol</b>	<b>Parameter</b>	<b>Test Conditions</b>	<b>Minimum</b>	<b>Typical</b>	<b>Maximum</b>	<b>Units</b>
$V_{cc}$	Core Supply Voltage		3.135	3.3	3.465	$\vee$
$V_{\text{CCA}}$	Analog Supply Voltage		$V_{\rm cc}$ – 0.15	3.3	3.465	V
$V_{\rm cco}$	Output Supply Voltage		3.135	3.3	3.465	$\vee$
'EE	Power Supply Current				135	mA
<sup>'</sup> CCA	Analog Supply Current				15	mA

**TABLE 4B. LVCMOS / LVTTL DC CHARACTERISTICS,**  $V_{CC} = V_{CCO} = 3.3V \pm 5\%$ **, TA = 0°C TO 70°C** 



NOTE 1: Outputs terminated with 50Ω to  $V_{cc}$ <sup>2</sup>.



#### **TABLE 4C. LVPECL DC CHARACTERISTICS,**  $V_{CC} = V_{CCO} = 3.3V \pm 5\%$ ,  $T_A = 0^\circ C$  to 70°C

NOTE 1: Outputs terminated with 50  $\Omega$  to V<sub>cco</sub> - 2V. See "Parameter Measurement Information" section, figure "3.3V Output Load Test Circuit".

#### **TABLE 5. INPUT FREQUENCY CHARACTERISTICS,**  $V_{cc} = V_{cco} = 3.3V \pm 5\%$ **, TA = 0°C to 70°C**



NOTE 1: For the input crystal and REF\_CLK frequency range, the M value must be set for the VCO to operate within the 250MHz to 700MHz range. Using the minimum input frequency of 12MHz, valid values of M are 21  $\leq M \leq$  58. Using the maximum frequency of 25MHz, valid values of M are  $10 \le M \le 28$ .

#### **TABLE 6. CRYSTAL CHARACTERISTICS**



#### **TABLE 7. AC CHARACTERISTICS,**  $V_{CC} = V_{CCO} = 3.3V \pm 5\%$ ,  $T_A = 0^{\circ}C$  to 70°C



See Parameter Measurement Information section.

NOTE 1: Jitter performance using XTAL inputs.

NOTE 2: Defined as skew between outputs at the same supply voltage and with equal load conditions.

Measured at the output differential cross points.

NOTE 3: This parameter is defined in accordance with JEDEC Standard 65.

# **PARAMETER MEASUREMENT INFORMATION**



# **APPLICATION INFORMATION**

## **STORAGE AREA NETWORKS**

A variety of technologies are used for interconnection of the elements within a SAN. The tables below lists the common frequencies used as well as the settings for the ICS8432-51 to generate the appropriate frequency.

#### **Table 8. Common SANs Application Frequencies**



#### **Table 9. Configuration Details for SANs Applications**



## **POWER SUPPLY FILTERING TECHNIQUES**

As in any high speed analog circuitry, the power supply pins are vulnerable to random noise. To achieve optimum jitter performance, power supply isolation is required. The ICS8432-51 provides separate power supplies to isolate any high switching noise from the outputs to the internal PLL.  $V_{cc}$ ,  $V_{cc}$  and  $V_{cc}$  should be individually connected to the power supply plane through vias, and 0.01µF bypass capacitors should be used for each pin. *Figure 2* illustrates this for a generic  $V_{cc}$  pin and also shows that V<sub>CCA</sub> requires that an additional 10Ω resistor along with a 10µF bypass capacitor be connected to the V<sub>CCA</sub> pin. **FIGURE 2. POWER SUPPLY FILTERING** 



#### **CRYSTAL INPUT INTERFACE**

The ICS8432-51 has been characterized with 18pF parallel resonant crystals. The capacitor values, C1 and C2, shown in *Figure 3* below were determined using a 25MHz, 18pF parallel resonant crystal and were chosen to minimize the ppm error. The optimum C1 and C2 values can be slightly adjusted for different board layouts.



**FIGURE 3. CRYSTAL INPUt INTERFACE**

## **LVCMOS TO XTAL INTERFACE**

The XTAL\_IN input can accept a single-ended LVCMOS signal through an AC coupling capacitor. A general interface diagram is shown in *Figure 4.* The XTAL\_OUT pin can be left floating. The input edge rate can be as slow as 10ns. For LVCMOS inputs, it is recommended that the amplitude be reduced from full swing to half swing in order to prevent signal interference with the power rail and to reduce noise. This configuration requires that the output impedance of the driver (Ro) plus the series resistance (Rs) equals the transmission line impedance. In addition, matched termination at the crystal input will attenuate the signal in half. This can be done in one of two ways. First, R1 and R2 in parallel should equal the transmission line impedance. For most  $50Ω$  applications, R1 and R2 can be 100Ω. This can also be accomplished by removing R1 and making R2 50Ω.



**FIGURE 4. GENERAL DIAGRAM FOR LVCMOS DRIVER TO XTAL INPUT INTERFACE**

## **RECOMMENDATIONS FOR UNUSED INPUT AND OUTPUT PINS**

#### **INPUTS:**

#### **CRYSTAL INPUTS**

For applications not requiring the use of the crystal oscillator input, both XTAL\_IN and XTAL\_OUT can be left floating. Though not required, but for additional protection, a 1kΩ resistor can be tied from XTAL\_IN to ground.

#### **REF\_CLK INPUT**

For applications not requiring the use of the test clock, it can be left floating. Though not required, but for additional protection, a 1kΩ resistor can be tied from the REF\_CLK to ground.

#### **LVCMOS CONTROL PINS**

All control pins have internal pull-ups or pull-downs; additional resistance is not required but can be added for additional protection. A 1kΩ resistor can be used.

#### **OUTPUTS:**

#### **LVPECL OUTPUTS**

All unused LVPECL outputs can be left floating. We recommend that there is no trace attached. Both sides of the differential output pair should either be left floating or terminated.

#### **TERMINATION FOR LVPECL OUTPUTS**

The clock layout topology shown below is a typical termination for LVPECL outputs. The two different layouts mentioned are recommended only as guidelines.

FOUTx and nFOUTx are low impedance follower outputs that generate ECL/LVPECL compatible outputs. Therefore, terminating resistors (DC current path to ground) or current sources must be used for functionality. These outputs are designed to

drive 50Ω transmission lines. Matched impedance techniques should be used to maximize operating frequency and minimize signal distortion. *Figures 5A and 5B* show two different layouts which are recommended only as guidelines. Other suitable clock layouts may exist and it would be recommended that the board designers simulate to guarantee compatibility across all printed circuit and clock component process variations.





**FIGURE 5A. LVPECL OUTPUT TERMINATION FIGURE 5B. LVPECL OUTPUT TERMINATION**

## **VFQFN EPAD THERMAL RELEASE PATH**

In order to maximize both the removal of heat from the package and the electrical performance, a land pattern must be incorporated on the Printed Circuit Board (PCB) within the footprint of the package corresponding to the exposed metal pad or exposed heat slug on the package, as shown in *Figure 6.* The solderable area on the PCB, as defined by the solder mask, should be at least the same size/shape as the exposed pad/slug area on the package to maximize the thermal/electrical performance. Sufficient clearance should be designed on the PCB between the outer edges of the land pattern and the inner edges of pad pattern for the leads to avoid any shorts.

While the land pattern on the PCB provides a means of heat transfer and electrical grounding from the package to the board through a solder joint, thermal vias are necessary to effectively conduct from the surface of the PCB to the ground plane(s). The land pattern must be connected to ground through these vias. The vias act as "heat pipes". The number of vias (i.e. "heat pipes")

are application specific and dependent upon the package power dissipation as well as electrical conductivity requirements. Thus, thermal and electrical analysis and/or testing are recommended to determine the minimum number needed. Maximum thermal and electrical performance is achieved when an array of vias is incorporated in the land pattern. It is recommended to use as many vias connected to ground as possible. It is also recommended that the via diameter should be 12 to 13mils (0.30 to 0.33mm) with 1oz copper via barrel plating. This is desirable to avoid any solder wicking inside the via during the soldering process which may result in voids in solder between the exposed pad/ slug and the thermal land. Precautions should be taken to eliminate any solder voids between the exposed heat slug and the land pattern. Note: These recommendations are to be used as a guideline only. For further information, refer to the Application Note on the *Surface Mount Assembly* of Amkor's Thermally/ Electrically Enhance Leadfame Base Package, Amkor Technology.



**FIGURE 6. P.C.ASSEMBLY FOR EXPOSED PAD THERMAL RELEASE PATH –SIDE VIEW (DRAWING NOT TO SCALE)**

#### **LAYOUT GUIDELINE**

The schematic of the ICS8432-51 layout example used in this layout guideline is shown in *Figure 7A.* The ICS8432-51 recommended PCB board layout for this example is shown in *Figure 7B.* This layout example is used as a general guideline.

The layout in the actual system will depend on the selected component types, the density of the components, the density of the traces, and the stack up of the P.C. board.



**FIGURE 7A. SCHEMATIC OF RECOMMENDED LAYOUT**

The following component footprints are used in this layout example:

All the resistors and capacitors are size 0603.

#### **POWER AND GROUNDING**

Place the decoupling capacitors C14 and C15, as close as possible to the power pins. If space allows, placement of the decoupling capacitor on the component side is preferred. This can reduce unwanted inductance between the decoupling capacitor and the power pin caused by the via.

Maximize the power and ground pad sizes and number of vias capacitors. This can reduce the inductance between the power and ground planes and the component power and ground pins. The RC filter consisting of R7, C11, and C16 should be placed as close to the  $V_{\text{cc}a}$  pin as possible.

## **CLOCK TRACES AND TERMINATION**

Poor signal integrity can degrade the system performance or cause system failure. In synchronous high-speed digital systems, the clock signal is less tolerant to poor signal integrity than other signals. Any ringing on the rising or falling edge or excessive ring back can cause system failure. The shape of the trace and the trace delay might be restricted by the available space on the board and the component location. While routing the traces, the clock signal traces should be routed first and should be locked prior to routing other signal traces.

- The differential 50 $\Omega$  output traces should have the same length.
- Avoid sharp angles on the clock trace. Sharp angle turns cause the characteristic impedance to change on the transmission lines.
- Keep the clock traces on the same layer. Whenever possible, avoid placing vias on the clock traces. Placement of vias on the traces can affect the trace characteristic impedance and hence degrade signal integrity.
- To prevent cross talk, avoid routing other signal traces in parallel with the clock traces. If running parallel traces is unavoidable, allow a separation of at least three trace widths between the differential clock trace and the other signal trace.
- Make sure no other signal traces are routed between the clock trace pair.
- The matching termination resistors should be located as close to the receiver input pins as possible.

#### **CRYSTAL**

The crystal X1 should be located as close as possible to the pins 24 (XTAL\_OUT) and 25 (XTAL\_IN). The trace length between the X1 and U1 should be kept to a minimum to avoid unwanted parasitic inductance and capacitance. Other signal traces should not be routed near the crystal traces.



**FIGURE 7B. PCB BOARD LAYOUT FOR ICS8432-51**

# **POWER CONSIDERATIONS**

This section provides information on power dissipation and junction temperature for the ICS8432-51. Equations and example calculations are also provided.

#### *1. Power Dissipation.*

The total power dissipation for the ICS8432-51 is the sum of the core power plus the power dissipated in the load(s). The following is the power dissipation for V<sub>cc</sub> = 3.3V + 5% = 3.465V, which gives worst case results. **NOTE:** Please refer to Section 3 for details on calculating power dissipated in the load.

- Power (core)<sub>MAX</sub> =  $V_{CC_MAX}$  \*  $I_{EE_MAX}$  = 3.465V \* 135mA = **467.8mW**
- Power (outputs)<sub>MAX</sub> = 30mW/Loaded Output pair If all outputs are loaded, the total power is 2 \* 30mW = **60mW**

**Total Power**  $\alpha_{\text{max}}$  (3.465V, with all outputs switching) = 467.8mW + 60mW = 527.8mW

#### *2. Junction Temperature.*

Junction temperature, Tj, is the temperature at the junction of the bond wire and bond pad and directly affects the reliability of the device. The maximum recommended junction temperature for devices is 125°C.

The equation for Tj is as follows: Tj =  $\theta_{\text{A}}$  \* Pd\_total + T<sub>A</sub>

Tj = Junction Temperature

 $\theta_{\mu}$  = Junction-to-Ambient Thermal Resistance

Pd\_total = Total Device Power Dissipation (example calculation is in section 1 above)

 $T<sub>a</sub>$  = Ambient Temperature

In order to calculate junction temperature, the appropriate junction-to-ambient thermal resistance  $\theta_{\rm A}$  must be used. Assuming a moderate air flow of 200 linear feet per minute and a multi-layer board, the appropriate value is 42.1°C/W per Table 10A below.

Therefore, Tj for an ambient temperature of 70°C with all outputs switching is:  $70^{\circ}$ C + 0.528W \* 42.1 $^{\circ}$ C/W = 92.2 $^{\circ}$ C. This is well below the limit of 125 $^{\circ}$ C.

This calculation is only an example. Tj will obviously vary depending on the number of loaded outputs, supply voltage, air flow, and the type of board (single layer or multi-layer).

#### **TABLE 10A. THERMAL RESISTANCE**  $\theta$ **<sub>14</sub>** For 32-PIN LQFP, FORCED CONVECTION



#### **TABLE 10B. THERMAL RESISTANCE** θ**JA FOR 32-PIN VFQFN, FORCED CONVECTION**



#### *3. Calculations and Equations.*

The purpose of this section is to derive the power dissipated into the load.

LVPECL output driver circuit and termination are shown in *Figure 8.*



**FIGURE 7. LVPECL DRIVER CIRCUIT AND TERMINATION**

To calculate worst case power dissipation into the load, use the following equations which assume a 50Ω load, and a termination voltage of V<sub>cco</sub> – 2V.

 $\bullet$  For logic high,  $\mathsf{V}_{_{\mathsf{OUT}}} = \mathsf{V}_{_{\mathsf{OH_{\_MAX}}}} = \mathsf{V}_{_{\mathsf{CCO_{\_MAX}}} - 0.9\mathsf{V}}$ 

$$
(V_{_{\textrm{CCO\_MAX}}} - V_{_{\textrm{OH\_MAX}}}) = 0.9V
$$

 $\bullet$  For logic low,  $V_{\text{out}} = V_{\text{out}} = V_{\text{co,max}} - 1.7V$  $(V_{\text{cco\_max}} - V_{\text{oL\_max}}) = 1.7V$ 

Pd\_H is power dissipation when the output drives high. Pd\_L is the power dissipation when the output drives low.

 $\mathsf{Pd\_H} = \left[(\mathsf{V}_{\mathsf{CH\_MAX}} - (\mathsf{V}_{\mathsf{CCO\_MAX}} - 2 \mathsf{V})) / \mathsf{R} \right] \cdot \left. (\mathsf{V}_{\mathsf{CCO\_MAX}} - \mathsf{V}_{\mathsf{OH\_MAX}} \right) = \left[ (2 \mathsf{V} - (\mathsf{V}_{\mathsf{CCO\_MAX}} - \mathsf{V}_{\mathsf{OH\_MAX}}) / \mathsf{R} \right] \cdot \left. (\mathsf{V}_{\mathsf{CCO\_MAX}} - \mathsf{V}_{\mathsf{OH\_MAX}} \right) = \left[ (2 \mathsf{V} - (\mathsf{V}_{\mathsf{CCO\_MAX}}$  $[(2V - 0.9V)/50\Omega) * 0.9V = 19.8mW$ 

 $\mathsf{Pd}\_\mathsf{L} = [(\mathsf{V}_{\mathsf{OL}_{\mathsf{MAX}}} - (\mathsf{V}_{\mathsf{CCO\_MAX}} - 2 \mathsf{V})) / \mathsf{R}]$  \*  $(\mathsf{V}_{\mathsf{CCO\_MAX}} - \mathsf{V}_{\mathsf{OL\_MAX}}) = [(\mathsf{2V} - (\mathsf{V}_{\mathsf{CCO\_MAX}} - \mathsf{V}_{\mathsf{OL\_MAX}})) / \mathsf{R}]$  \*  $(\mathsf{V}_{\mathsf{CCO\_MAX}} - \mathsf{V}_{\mathsf{OL\_MAX}}) =$ [(2V – 1.7V)/50Ω) \* 1.7V = **10.2mW**

Total Power Dissipation per output pair = Pd\_H + Pd\_L = **30mW**

# **RELIABILITY INFORMATION**

## **TABLE 11A.**  $\theta_{\text{A}}$ **vs. Air Flow Table for 32 Lead LQFP**



## **TABLE 11B.**  $\theta_{\text{A}}$ vs. Air Flow Table for 32 Lead VFQFN Package



#### **TRANSISTOR COUNT**

The transistor count for ICS8432-51 is: 3743

**PACKAGE OUTLINE - Y SUFFIX FOR 32 LEAD LQFP**







Reference Document: JEDEC Publication 95, MS-026

#### **PACKAGE OUTLINE - K SUFFIX 32 LEAD VFQFN**



NOTE: The following package mechanical drawing is a generic drawing that applies to any pin count VFQFN package. This drawing is not intended to convey the actual pin count or pin layout of this device. The pin count and pinout are shown on the front page. The package dimensions are in Table 8 below.



#### **TABLE 12B. PACKAGE DIMENSIONS**

Reference Document: JEDEC Publication 95, MO-220

#### **TABLE 13. ORDERING INFORMATION**



NOTE: "LF" suffix to the part number are the PB-free configuration, RoHS compliant



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