

# 18-Bit, 1.5 LSB INL, 250 kSPS PulSAR Differential ADC in MSOP/LFCSP

# Data Sheet **[AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf)**

### <span id="page-0-0"></span>**FEATURES**

**18-bit resolution with no missing codes Throughput: 250 kSPS INL: ±0.75 LSB typical, ±1.5 LSB maximum (±6 ppm of FSR) Dynamic range: 102 dB typical at 250 kSPS Oversampled dynamic range: 125 dB at1 kSPS Noise-free code resolution: 20 bits at 1 kSPS Effective resolution: 22.7 bits at 1 kSPS SINAD: 101.5 dB typical at 1 kHz THD: −125 dB typical at 1 kHz**  True differential analog input range:  $\pm V_{REF}$ **0 V to VREF with VREF up to VDD on both inputs No pipeline delay Single-supply 2.3 V to 5 V operation with 1.8 V/2.5 V/3 V/5 V logic interface Proprietary serial interface SPI/QSPI/MICROWIRE™/DSP compatible Ability to daisy-chain multiple ADCs Optional busy indicator feature Power dissipation 1.35 mW at 2.5 V/100 kSPS, 4 mW at 5 V/100 kSPS 1.4 µW at 2.5 V/100 SPS Standby current: 1 nA 10-lead packages: MSOP (MSOP-8 size) and 3 mm × 3 mm LFCSP (SOT-23 size) Pin-for-pin compatible with the18-bi[t AD7690](http://www.analog.com/AD7690?doc=AD7691.pdf) and 16-bi[t AD7693,](http://www.analog.com/AD7693?doc=AD7691.pdf) [AD7688,](http://www.analog.com/AD7688?doc=AD7691.pdf) an[d AD7687](http://www.analog.com/AD7687?doc=AD7691.pdf)**

### <span id="page-0-1"></span>**APPLICATIONS**

**Battery-powered equipment Data acquisitions Seismic data acquisition systems Instrumentation Medical instruments**





**Rev. E [Document Feedback](https://form.analog.com/Form_Pages/feedback/documentfeedback.aspx?doc=AD7691.pdf&product=AD7691&rev=E)**

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#### **APPLICATION DIAGRAM**

<span id="page-0-2"></span>

#### **Table 1. MSOP, LFCSP/SOT-23 14-/16-/18-Bit PulSAR® ADC**



## <span id="page-0-3"></span>**GENERAL DESCRIPTION**

The  $AD7691<sup>1</sup>$  is an 18-bit, charge redistribution, successive approximation, analog-to-digital converter (ADC) that operates from a single power supply, VDD, between 2.3 V and 5 V. It contains a low power, high speed, 18-bit sampling ADC with no missing codes, an internal conversion clock, and a versatile serial interface port. On the CNV rising edge, it samples the voltage difference between the IN+ and IN− pins. The voltages on these pins swing in opposite phases between 0 V and REF. The reference voltage, REF, is applied externally and can be set up to the supply voltage.

The part's power scales linearly with throughput.

The SPI-compatible serial interface also features the ability, using the SDI input, to daisy-chain several ADCs on a single 3-wire bus and provides an optional busy indicator. It is compatible with 1.8 V, 2.5 V, 3 V, or 5 V logic, using the separate VIO supply.

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is housed in a 10-lead MSOP or a 10-lead LFCSP with operation specified from −40°C to +85°C.

<sup>1</sup> Protected by U.S. Patent 6,703,961.

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## <span id="page-1-0"></span>**REVISION HISTORY**



## **7/14—Rev. C to Rev. D**



## **3/12—Rev. B to Rev. C**



### **7/11—Rev. A to Rev. B**





## **11/07—Rev. 0 to Rev. A**



**7/06—Revision 0: Initial Version** 

# <span id="page-2-0"></span>SPECIFICATIONS

VDD = 2.3 V to 5.25 V, VIO = 2.3 V to VDD,  $V_{REF}$  = VDD, all specifications  $T_{MIN}$  to  $T_{MAX}$ , unless otherwise noted.

#### **Table 2.**



<sup>1</sup> See th[e Analog Inputs](#page-14-1) section.

 $^2$  LSB means least significant bit. With the  $\pm 5$  V input range, one LSB is 38.15  $\mu$ V.

 $3$  See th[e Terminology](#page-12-0) section. These specifications include full temperature range variation but not the error contribution from the external reference.

<sup>4</sup> All ac accuracy specifications in dB are referred to a full-scale input FSR. Tested with an input signal at 0.5 dB below full scale, unless otherwise specified. <sup>5</sup> Dynamic range obtained by oversampling the ADC running at a throughput fs of 250 kSPS, followed by postdigital filtering with an output word rate fo.

 $6 f_{\text{IN1}} = 21.4 \text{ kHz}$  and  $f_{\text{IN2}} = 18.9 \text{ kHz}$ , with each tone at -7 dB below full scale.

VDD = 2.3 V to 5.25 V, VIO = 2.3 V to VDD,  $V_{REF}$  = VDD, all specifications  $T_{MIN}$  to  $T_{MAX}$ , unless otherwise noted.



<sup>1</sup> Conversion results are available immediately after completed conversion.<br><sup>2</sup> With all digital inputs forced to VIO or GND as required.

<sup>3</sup> During acquisition phase.

<sup>4</sup> Contact an Analog Devices, Inc., sales representative for the extended temperature range.

# <span id="page-4-0"></span>**TIMING SPECIFICATIONS**

VDD = 4.5 V to 5.25 V, VIO = 2.3 V to VDD,  $V_{REF}$  = VDD, all specifications  $T_{MIN}$  to  $T_{MAX}$ , unless otherwise noted.<sup>1</sup>



<sup>1</sup> Se[e Figure 3](#page-5-0) an[d Figure 4](#page-5-1) for load conditions.

VDD = 2.3 V to 4.5 V, VIO = 2.3 V to VDD,  $V_{REF}$  = VDD, all specifications  $T_{MIN}$  to  $T_{MAX}$ , unless otherwise noted.<sup>1</sup>



<sup>1</sup> Se[e Figure 3](#page-5-0) an[d Figure 4](#page-5-1) for load conditions.



<span id="page-5-0"></span>*Figure 3. Load Circuit for Digital Interface Timing Figure 4. Voltage Levels for Timing*



<span id="page-5-1"></span>

# <span id="page-6-0"></span>ABSOLUTE MAXIMUM RATINGS

#### **Table 6.**



<sup>1</sup> See th[e Analog Inputs](#page-14-1) section.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## <span id="page-6-1"></span>*Thermal Resistance*

 $\theta_{JA}$  is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages.

#### **Table 7. Thermal Resistance**



## <span id="page-6-2"></span>**ESD CAUTION**



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

# <span id="page-7-0"></span>PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS





#### **Table 8. Pin Function Descriptions**



 $A = 1$  analog input, DI = digital input, DO = digital output, and P = power.

# <span id="page-8-0"></span>TYPICAL PERFORMANCE CHARACTERISTICS



*Figure 8. Histogram of a DC Input at the Code Center, 5 V* 





*Figure 10. Differential Nonlinearity vs. Code, 5 V*









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*Figure 21. Operating Current vs. Supply*

06146-044

Σŕ,

06146-047

06146-034

<span id="page-11-0"></span>



# <span id="page-12-0"></span>**TERMINOLOGY**

### **Least Significant Bit (LSB)**

The least significant bit, or LSB, is the smallest increment that can be represented by a converter. For an analog-to-digital converter with *N* bits of resolution, the LSB expressed in volts is

$$
LSB(\mathbf{V}) = \frac{V_{INpp}}{2^N}
$$

### **Integral Nonlinearity Error (INL)**

INL refers to the deviation of each individual code from a line drawn from negative full scale through positive full scale. The point used as negative full scale occurs ½ LSB before the first code transition. Positive full scale is defined as a level 1½ LSB beyond the last code transition. The deviation is measured from the middle of each code to the true straight line (se[e Figure 28\)](#page-13-3).

### **Differential Nonlinearity Error (DNL)**

In an ideal ADC, code transitions are 1 LSB apart. DNL is the maximum deviation from this ideal value. It is often specified in terms of resolution for which no missing codes are guaranteed.

### **Zero Error**

Zero error is the difference between the ideal midscale voltage, that is, 0 V, from the actual voltage producing the midscale output code, that is, 0 LSB.

### **Gain Error**

The first transition (from 100 . . . 00 to 100 . . . 01) should occur at a level ½ LSB above nominal negative full scale (−4.999981 V for the ±5 V range). The last transition (from 011 … 10 to 011 … 11) should occur for an analog voltage 1½ LSB below the nominal full scale (+4.999943 V for the ±5 V range). The gain error is the deviation in LSBs (or % of full-scale range) of the difference between the actual level of the last transition and the actual level of the first transition from the difference between the ideal levels. The closely related full-scale error, which is expressed also in LSBs or % of full-scale range, includes the contribution from the zero error.

### **Spurious-Free Dynamic Range (SFDR)**

SFDR is the difference, in decibels, between the rms amplitude of the input signal and the peak spurious signal.

## **Effective Number of Bits (ENOB)**

ENOB is a measurement of the resolution with a sine wave input. It is related to SINAD by the following formula:

 $ENOB = (SIMAD<sub>dB</sub> - 1.76)/6.02$ 

and is expressed in bits.

### **Noise-Free Code Resolution**

It is the number of bits beyond which it is impossible to resolve individual codes distinctly. It is calculated as

*Noise-Free Code Resolution* =  $log_2(2^N/Peak-to-Peak Noise)$ and is expressed in bits.

### **Effective Resolution**

It is calculated as

*Effective Resolution* =  $log_2(2^N/RMS \text{ Input Noise})$ 

and is expressed in bits.

### **Total Harmonic Distortion (THD)**

THD is the ratio of the rms sum of the first five harmonic components to the rms value of a full-scale input signal and is expressed in decibels.

### **Dynamic Range**

Dynamic range is the ratio of the rms value of the full scale to the total rms noise measured with the inputs shorted together. The value for dynamic range is expressed in decibels.

### **Signal-to-Noise Ratio (SNR)**

SNR is the ratio of the rms value of the actual input signal to the rms sum of all other spectral components below the Nyquist frequency, excluding harmonics and dc. The value for SNR is expressed in decibels.

### **Signal-to-(Noise + Distortion) Ratio (SINAD)**

SINAD is the ratio of the rms value of the actual input signal to the rms sum of all other spectral components below the Nyquist frequency, including harmonics but excluding dc. The value for SINAD is expressed in decibels.

### **Aperture Delay**

Aperture delay is the measure of the acquisition performance. It is the time between the rising edge of the CNV input and when the input signal is held for a conversion.

### **Transient Response**

Transient response is the time required for the ADC to acquire its input accurately after a full-scale step function is applied.

# <span id="page-13-0"></span>THEORY OF OPERATION



*Figure 27. ADC Simplified Schematic*

# <span id="page-13-4"></span><span id="page-13-1"></span>**CIRCUIT INFORMATION**

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is a fast, low power, single-supply, precise, 18-bit ADC using a successive approximation architecture.

The part is capable of converting 250,000 samples per second (250 kSPS) and powers down between conversions. When operating at 1 kSPS, for example, it consumes 50 µW typically, which is ideal for battery-powered applications.

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) provides the user with an on-chip track-and-hold and does not exhibit pipeline delay or latency, making it ideal for multiple multiplexed channel applications.

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is specified from 2.3 V to 5.25 V and can be interfaced to any 1.8 V to 5 V digital logic family. It is housed in a 10-lead MSOP or a tiny 10-lead LFCSP that combines space savings and allows flexible configurations.

The part is pin-for-pin compatible with the 18-bi[t AD7690](http://www.analog.com/AD7690?doc=AD7691.pdf) as well as the 16-bit [AD7687](http://www.analog.com/AD7687?doc=AD7691.pdf) an[d AD7688.](http://www.analog.com/AD7688?doc=AD7691.pdf)

# <span id="page-13-2"></span>**CONVERTER OPERATION**

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is a successive approximation ADC based on a charge redistribution DAC[. Figure](#page-13-4) 27 shows the simplified schematic of the ADC. The capacitive DAC consists of two identical arrays of 18 binary-weighted capacitors, which are connected to the two comparator inputs.

During the acquisition phase, terminals of the array tied to the comparator's input are connected to GND via SW+ and SW−. All independent switches are connected to the analog inputs. Thus, the capacitor arrays are used as sampling capacitors and acquire the analog signal on the IN+ and IN− inputs. When the acquisition phase is complete and the CNV input goes high, a conversion phase is initiated. When the conversion phase begins, SW+ and SW− are opened first. The two capacitor arrays are then disconnected from the inputs and connected to the GND input. Therefore, the differential voltage between the inputs IN+ and IN− captured at the end of the acquisition phase is applied to the comparator inputs, causing the comparator to become unbalanced. By switching each element of the capacitor array between GND and REF, the comparator input varies by binary-weighted voltage steps ( $V_{REF}/2$ ,  $V_{REF}/4$  ...  $V_{REF}/262,144$ ).

The control logic toggles these switches, starting with the MSB, to bring the comparator back into a balanced condition. After the completion of this process, the part returns to the acquisition phase, and the control logic generates the ADC output code and a busy signal indicator.

Because the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) has an on-board conversion clock, the serial clock, SCK, is not required for the conversion process.

## *Transfer Functions*

The ideal transfer characteristic for th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is shown in [Figure 28](#page-13-3) an[d Table 9.](#page-13-5) 



*Figure 28. ADC Ideal Transfer Function*

<span id="page-13-5"></span><span id="page-13-3"></span>



<sup>1</sup> This is also the code for an overranged analog input (V<sub>IN+</sub> − V<sub>IN</sub>− above V<sub>REF</sub> − V<sub>GND</sub>). <sup>2</sup> This is also the code for an underranged analog input ( $V_{IN+} - V_{IN-}$  below  $V_{GND}$ ).

## <span id="page-14-0"></span>**TYPICAL CONNECTION DIAGRAM**

[Figure 29](#page-14-2) shows an example of the recommended connection diagram for th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) when multiple supplies are available.



#### <span id="page-14-2"></span><span id="page-14-1"></span>**ANALOG INPUTS**

[Figure 30](#page-14-3) shows an equivalent circuit of the input structure of the [AD7691.](http://www.analog.com/AD7691?doc=AD7691.pdf)

The two diodes, D1 and D2, provide ESD protection for the analog inputs, IN+ and IN−. Care must be taken to ensure that the analog input signal does not exceed the supply rails by more than 0.3 V because this causes the diodes to become forward biased and start conducting current. These diodes can handle a forward-biased current of 130 mA maximum. For instance, these conditions could eventually occur if the input buffer (U1) supplies are different from VDD. In such a case (for example, an input buffer with a short circuit), the current limitation can be used to protect the part.



*Figure 30. Equivalent Analog Input Circuit*

<span id="page-14-3"></span>The analog input structure allows the sampling of the true differential signal between IN+ and IN−. By using these differential inputs, signals common to both inputs are rejected.

During the acquisition phase, the impedance of the analog inputs (IN+ and IN−) can be modeled as a parallel combination of the capacitor, C<sub>PIN</sub>, and the network formed by the series connection of  $R_{\text{IN}}$  and  $C_{\text{IN}}$ . C<sub>PIN</sub> is primarily the pin capacitance. R<sub>IN</sub> is typically 3 k $\Omega$  and is a lumped component composed of serial resistors and the on resistance of the switches.  $C_{\text{IN}}$  is typically 30 pF and is mainly the ADC sampling capacitor.

During the conversion phase, where the switches are opened, the input impedance is limited to CPIN. RIN and CIN make a 1-pole, low-pass filter that reduces undesirable aliasing effects and limits noise.

When the source impedance of the driving circuit is low, the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) can be driven directly. Large source impedances significantly affect the ac performance, especially total harmonic distortion (THD). The dc performances are less sensitive to the input impedance. The maximum source impedance depends on the amount of THD that can be tolerated.

The THD degrades as a function of the source impedance and the maximum input frequency as shown in [Figure 31.](#page-14-4)



<span id="page-14-4"></span>*Figure 31. THD vs. Analog Input Frequency and Source Resistance*

# <span id="page-15-0"></span>**DRIVER AMPLIFIER CHOICE**

Although th[e AD7691 i](http://www.analog.com/AD7691?doc=AD7691.pdf)s easy to drive, the driver amplifier must meet the following requirements:

 The noise generated by the driver amplifier needs to be kept as low as possible to preserve the SNR and transition noise performance of the [AD7691.](http://www.analog.com/AD7691?doc=AD7691.pdf) The noise coming from the driver is filtered by the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) analog input circuit's 1-pole, low-pass filter made by  $R_{IN}$  and  $C_{IN}$  or by the external filter, if one is used. The SNR degradation due to the amplifier is as follows:

*SNRLOSS* =

 $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$ J  $\backslash$ L L L L l ſ  $20 \log \left( \frac{N_{NADC}^2}{\sqrt{V_{NADC}^2 + \frac{\pi}{2} f_{-3\,\text{dB}} (Ne_{N+})^2 + \frac{\pi}{2} f_{-3\,\text{dB}} (Ne_{N-})^2}} \right)$ *NADC*  $V_{\text{NADC}}^{2} + \frac{1}{2} f_{-3 \text{ dB}} (\text{Ne}_{N+})^2 + \frac{1}{2} f_{-3 \text{ dB}} (\text{Ne}_{N})^2$ *V*

where:

*VNADC* is the noise of the ADC, in μV, given by the following:

$$
V_{NADC} = \frac{\frac{V_{INpp}}{2\sqrt{2}}}{10^{\frac{SNR}{20}}}
$$

*f*−3 dB is the input bandwidth, in MHz, of th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) (2 MHz) or the cutoff frequency of the input filter, if one is used. *N* is the noise gain of the amplifier (for example, 1 in buffer configuration).

*eN+* and *eN−* are the equivalent input noise voltage densities of the op amps connected to IN+ and IN−, in nV/√Hz.

This approximation can be used when the resistances around the amplifier are small. If larger resistances are used, their noise contributions should also be root-sum-squared.

- For ac applications, the driver should have a THD performance commensurate with th[e AD7691.](http://www.analog.com/AD7691?doc=AD7691.pdf)
- For multichannel multiplexed applications, the driver amplifier and th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) analog input circuit must settle for a full-scale step onto the capacitor array at an 18-bit level (0.0004%, 4 ppm). In the amplifier's data sheet, settling at 0.1% to 0.01% is more commonly specified. This may differ significantly from the settling time at an 18-bit level and should be verified prior to driver selection.



### **Table 10. Recommended Driver Amplifiers**

### <span id="page-15-1"></span>**SINGLE-TO-DIFFERENTIAL DRIVER**

For applications using a single-ended analog signal, either bipolar or unipolar, th[e ADA4941-1](http://www.analog.com/ADA4941-1?doc=AD7691.pdf) single-ended-to-differential driver allows for a differential input into the part. The schematic is shown in [Figure 32.](#page-15-3)



Figure 32. Single-Ended-to-Differential Driver Circuit

<span id="page-15-3"></span>R1 and R2 set the attenuation ratio between the input range and the ADC range ( $V_{REF}$ ). R1, R2, and  $C_F$  are chosen depending on the desired input resistance, signal bandwidth, antialiasing, and noise contribution. For example, for the  $\pm 10$  V range with a 4 k $\Omega$ impedance,  $R2 = 1$  kΩ and  $R1 = 4$  kΩ.

R3 and R4 set the common mode on the IN− input, and R5 and R6 set the common mode on the IN+ input of the ADC. The common mode should be set close to VREF/2; however, if single supply is desired, it can be set slightly above  $V_{REF}/2$  to provide some headroom for the [ADA4941-1 o](http://www.analog.com/ADA4941-1?doc=AD7691.pdf)utput stage. For example, for the  $\pm 10$  V range with a single supply, R3 = 8.45 k $\Omega$ , R4 = 11.8 kΩ, R5 = 10.5 kΩ, and R6 = 9.76 kΩ.

## <span id="page-15-2"></span>**VOLTAGE REFERENCE INPUT**

The [AD7691 v](http://www.analog.com/AD7691?doc=AD7691.pdf)oltage reference input, REF, has a dynamic input impedance and should therefore be driven by a low impedance source with efficient decoupling between the REF and GND pins, as explained in the [Layout](#page-23-1) section.

When REF is driven by a very low impedance source, for example, a reference buffer using the [AD8031](http://www.analog.com/AD8031?doc=AD7691.pdf) or th[e AD8605,](http://www.analog.com/AD8605?doc=AD7691.pdf) a 10 μF (X5R, 0805 size) ceramic chip capacitor is appropriate for optimum performance.

If an unbuffered reference voltage is used, the decoupling value depends on the reference used. For instance, a 22 μF (X5R, 1206 size) ceramic chip capacitor is appropriate for optimum performance using a low temperature drif[t ADR431,](http://www.analog.com/ADR431?doc=AD7961.pdf) [ADR433,](http://www.analog.com/ADR433?doc=AD7961.pdf) [ADR434,](http://www.analog.com/ADR434?doc=AD7961.pdf) and [ADR435](http://www.analog.com/ADR435?doc=AD7961.pdf) reference.

If desired, smaller reference decoupling capacitor values as low as 2.2 μF can be used with a minimal impact on performance, especially DNL.

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Regardless, there is no need for an additional lower value ceramic decoupling capacitor (for example, 100 nF) between the REF and GND pins.

## <span id="page-16-0"></span>**POWER SUPPLY**

Th[e AD7691 u](http://www.analog.com/AD7691?doc=AD7691.pdf)ses two power supply pins: a core supply (VDD) and a digital input/output interface supply (VIO). VIO allows direct interface with any logic between 1.8 V and VDD. To reduce the supplies needed, the VIO and VDD pins can be tied together. The [AD7691 i](http://www.analog.com/AD7691?doc=AD7691.pdf)s independent of power supply sequencing between VIO and VDD. Additionally, it is very insensitive to power supply variations over a wide frequency range, as shown i[n Figure 25.](#page-11-0) 

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) powers down automatically at the end of each conversion phase, and therefore, the power scales linearly with the sampling rate. This makes the part ideal for low sampling rate (as low as a few hertz) and low battery-powered applications.



# <span id="page-16-1"></span>**SUPPLYING THE ADC FROM THE REFERENCE**

For simplified applications, th[e AD7691,](http://www.analog.com/AD7691?doc=AD7691.pdf) with its low operating current, can be supplied directly using the reference circuit shown in [Figure 34.](#page-16-3) The reference line can be driven by

- The system power supply directly.
- A reference voltage with enough current output capability, such as th[e ADR431,](http://www.analog.com/ADR431?doc=AD7961.pdf) [ADR433,](http://www.analog.com/ADR433?doc=AD7961.pdf) [ADR434,](http://www.analog.com/ADR434?doc=AD7961.pdf) and [ADR435.](http://www.analog.com/ADR435?doc=AD7961.pdf)
- A reference buffer, such as the [AD8031,](http://www.analog.com/AD8031?doc=AD7691.pdf) which can also filter the system power supply, as shown i[n Figure 34.](#page-16-3)



# <span id="page-16-3"></span><span id="page-16-2"></span>**DIGITAL INTERFACE**

Though th[e AD7691 h](http://www.analog.com/AD7691?doc=AD7691.pdf)as a reduced number of pins, it offers flexibility in its serial interface modes.

When in  $\overline{CS}$  mode, th[e AD7691 i](http://www.analog.com/AD7691?doc=AD7691.pdf)s compatible with SPI, QSPI<sup>™</sup>, digital hosts, and DSPs, for example, the Blackfin® processors or the high performance, mixed-signal DSP family. In this mode, the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) can use either a 3-wire or 4-wire interface. A 3 wire interface using the CNV, SCK, and SDO signals minimizes wiring connections and is useful, for instance, in isolated applications. A 4-wire interface using the SDI, CNV, SCK, and SDO signals allows CNV, which initiates the conversions, to be independent of the readback timing (SDI). This is useful in low jitter sampling or simultaneous sampling applications.

When in chain mode, th[e AD7691 p](http://www.analog.com/AD7691?doc=AD7691.pdf)rovides a daisy-chain feature using the SDI input for cascading multiple ADCs on a single data line similar to a shift register.

The mode in which the device operates depends on the SDI level when the CNV rising edge occurs. The CS mode is selected if SDI is high, and the chain mode is selected if SDI is low. The SDI hold time is such that when SDI and CNV are connected together, the chain mode is selected.

The initial state of SDO on power up is indeterminate. Therefore, in order to put SDO in a known state, a conversion must be initiated and all data bits clocked out.

In either mode, the [AD7691 o](http://www.analog.com/AD7691?doc=AD7691.pdf)ffers the option of forcing a start bit in front of the data bits. This start bit can be used as a busy signal indicator to interrupt the digital host and trigger the data reading. Otherwise, without a busy indicator, the user must timeout the maximum conversion time prior to readback.

The busy indicator feature is enabled

- In the  $\overline{\text{CS}}$  mode if CNV or SDI is low when the ADC conversion ends (se[e Figure 38 a](#page-18-1)nd [Figure 42\)](#page-20-1).
- In the chain mode if SCK is high during the CNV rising edge (see [Figure 46\)](#page-22-1).

# <span id="page-17-0"></span>**CS MODE, 3-WIRE WITHOUT BUSY INDICATOR**

This mode is usually used when a singl[e AD7691 i](http://www.analog.com/AD7691?doc=AD7691.pdf)s connected to an SPI-compatible digital host. The connection diagram is shown in [Figure 35,](#page-17-1) and the corresponding timing is given in [Figure 36.](#page-17-2) 

With SDI tied to VIO, a rising edge on CNV initiates a conversion, selects the  $\overline{CS}$  mode, and forces SDO to high impedance. Once a conversion is initiated, it continues until completion irrespective of the state of CNV. This can be useful, for instance, to bring CNV low to select other SPI devices, such as analog multiplexers, but CNV must be returned high before the minimum conversion time elapses and then held high for the maximum possible conversion time to avoid the generation of the busy signal indicator. When the conversion is complete, the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) enters the acquisition phase and powers down. When CNV goes low, the MSB is output onto SDO. The remaining data bits are clocked by subsequent SCK falling

edges. The data is valid on both SCK edges. Although the rising edge can be used to capture the data, a digital host using the SCK falling edge can allow a faster reading rate, provided it has an acceptable hold time. After the 18<sup>th</sup> SCK falling edge, or when CNV goes high, whichever occurs first, SDO returns to high impedance.



<span id="page-17-1"></span>Figure 35. 3-Wire  $\overline{CS}$  Mode Without Busy Indicator Connection Diagram (SDI High)



<span id="page-17-2"></span>Figure 36. 3-Wire  $\overline{CS}$  Mode Without Busy Indicator Serial Interface Timing (SDI High)

# <span id="page-18-0"></span>**CS MODE, 3-WIRE WITH BUSY INDICATOR**

This mode is usually used when a singl[e AD7691 i](http://www.analog.com/AD7691?doc=AD7691.pdf)s connected to an SPI-compatible digital host having an interrupt input.

The connection diagram is shown in [Figure 37,](#page-18-2) and the corresponding timing is given i[n Figure 38.](#page-18-1) 

With SDI tied to VIO, a rising edge on CNV initiates a conversion, selects the CS mode, and forces SDO to high impedance. SDO is maintained in high impedance until the completion of the conversion irrespective of the state of CNV. Prior to the minimum conversion time, CNV can select other SPI devices, such as analog multiplexers, but CNV must be returned low before the minimum conversion time elapses and then held low for the maximum possible conversion time to guarantee the generation of the busy signal indicator. When the conversion is complete, SDO goes from high impedance to low impedance. With a pull-up on the SDO line, this transition is used as an interrupt signal to initiate the data reading controlled by the digital host. When using this option, select the value of the pull-up resistor such that it maintains an appropriate rise time on the SDO line for the application. This is a function of the resistance of the pull-up and the capacitance of the SDO line. Th[e AD7691 t](http://www.analog.com/AD7691?doc=AD7691.pdf)hen enters the acquisition phase and powers down. The data bits are clocked out, MSB first, by subsequent

SCK falling edges. The data is valid on both SCK edges. Although the rising edge can be used to capture the data, a digital host using the SCK falling edge can allow a faster reading rate, provided it has an acceptable hold time. After the optional 19<sup>th</sup> SCK falling edge, or when CNV goes high, whichever occurs first, SDO returns to high impedance.

If multiple [AD7691 d](http://www.analog.com/AD7691?doc=AD7691.pdf)evices are selected at the same time, the SDO output pin handles this contention without damage or induced latch-up. Meanwhile, it is recommended to keep this contention as short as possible to limit extra power dissipation.



<span id="page-18-2"></span>Figure 37. 3-Wire  $\overline{CS}$  Mode with Busy Indicator Connection Diagram (SDI High)



<span id="page-18-1"></span>Figure 38. 3-Wire  $\overline{CS}$  Mode with Busy Indicator Serial Interface Timing (SDI High)

# <span id="page-19-0"></span>**CS MODE, 4-WIRE WITHOUT BUSY INDICATOR**

This mode is usually used when multiple [AD7691 d](http://www.analog.com/AD7691?doc=AD7691.pdf)evices are connected to an SPI-compatible digital host.

A connection diagram example using two [AD7691d](http://www.analog.com/AD7691?doc=AD7691.pdf)evices is shown in [Figure 39,](#page-19-1) and the corresponding timing is given in [Figure 40.](#page-19-2) 

With SDI high, a rising edge on CNV initiates a conversion, selects the CS mode, and forces SDO to high impedance. In this mode, CNV must be held high during the conversion phase and the subsequent data readback. (If SDI and CNV are low, SDO is driven low.) Prior to the minimum conversion time, SDI can be used to select other SPI devices, such as analog multiplexers,

but SDI must be returned high before the minimum conversion time elapses and then held high for the maximum possible conversion time to avoid the generation of the busy signal indicator. When the conversion is complete, th[e AD7691 e](http://www.analog.com/AD7691?doc=AD7691.pdf)nters the acquisition phase and powers down. Each ADC result can be read by bringing its SDI input low, which consequently outputs the MSB onto SDO. The remaining data bits are clocked by subsequent SCK falling edges. The data is valid on both SCK edges. Although the rising edge can be used to capture the data, a digital host using the SCK falling edge allows a faster reading rate, provided it has an acceptable hold time. After the 18<sup>th</sup> SCK falling edge, or when SDI goes high, whichever occurs first, SDO returns to high impedance and anothe[r AD7691 i](http://www.analog.com/AD7691?doc=AD7691.pdf)s read.



Figure 39. 4-Wire  $\overline{\text{CS}}$  Mode Without Busy Indicator Connection Diagram

<span id="page-19-1"></span>

<span id="page-19-2"></span>Figure 40. 4-Wire  $\overline{\text{CS}}$  Mode Without Busy Indicator Serial Interface Timing

# <span id="page-20-0"></span>**CS MODE, 4-WIRE WITH BUSY INDICATOR**

This mode is normally used when a singl[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is connected to an SPI-compatible digital host with an interrupt input, and it is desired to keep CNV, which is used to sample the analog input, independent of the signal used to select the data reading. This requirement is particularly important in applications where low jitter on CNV is desired.

The connection diagram is shown in [Figure 41,](#page-20-2) and the corresponding timing is given i[n Figure 42.](#page-20-1) 

With SDI high, a rising edge on CNV initiates a conversion, selects the  $\overline{CS}$  mode, and forces SDO to high impedance. In this mode, CNV must be held high during the conversion phase and the subsequent data readback. (If SDI and CNV are low, SDO is driven low.) Prior to the minimum conversion time, SDI can be used to select other SPI devices, such as analog multiplexers, but SDI must be returned low before the minimum conversion time elapses and then held low for the maximum possible conversion time to guarantee the generation of the busy signal indicator. When the conversion is complete, SDO goes from high impedance to low impedance. With a pull-up on the SDO line, this transition is used as an interrupt signal to initiate the data readback controlled by the digital host. When using this option, select the value of the pull-up resistor such that it

maintains an appropriate rise time on the SDO line for the application. This is a function of the resistance of the pull-up and the capacitance of the SDO line. The [AD7691 t](http://www.analog.com/AD7691?doc=AD7691.pdf)hen enters the acquisition phase and powers down. The data bits are clocked out, MSB first, by subsequent SCK falling edges. The data is valid on both SCK edges. Although the rising edge is used to capture the data, a digital host using the SCK falling edge can allow a faster reading rate, provided it has an acceptable hold time. After the optional 19th SCK falling edge, or SDI going high, whichever occurs first, SDO returns to high impedance.



<span id="page-20-2"></span>Figure 41. 4-Wire  $\overline{CS}$  Mode with Busy Indicator Connection Diagram



<span id="page-20-1"></span>Figure 42. 4-Wire  $\overline{\text{CS}}$  Mode with Busy Indicator Serial Interface Timing

## <span id="page-21-0"></span>**CHAIN MODE WITHOUT BUSY INDICATOR**

This mode can be used to daisy-chain multiple [AD7691 d](http://www.analog.com/AD7691?doc=AD7691.pdf)evices on a 3-wire serial interface. This feature is useful for reducing component count and wiring connections, for example, in isolated multiconverter applications or for systems with a limited interfacing capacity. Data readback is analogous to clocking a shift register.

A connection diagram example using two [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) devices is shown in [Figure 43,](#page-21-1) and the corresponding timing is given in [Figure 44.](#page-21-2) 

When SDI and CNV are low, SDO is driven low. With SCK low, a rising edge on CNV initiates a conversion, selects the chain mode, and disables the busy indicator. In this mode, CNV is held high during the conversion phase and the subsequent data

readback. When the conversion is complete, the MSB is output onto SDO and the [AD7691 e](http://www.analog.com/AD7691?doc=AD7691.pdf)nters the acquisition phase and powers down. The remaining data bits stored in the internal shift register are clocked by subsequent SCK falling edges. For each ADC, SDI feeds the input of the internal shift register and is clocked by the SCK falling edge. Each ADC in the chain outputs its data MSB first, and  $18 \times N$  clocks are required to read back the N ADCs. The data is valid on both SCK edges. Although the rising edge can be used to capture the data, a digital host using the SCK falling edge can allow a faster reading rate and, consequently, mor[e AD7691 d](http://www.analog.com/AD7691?doc=AD7691.pdf)evices in the chain, provided the digital host has an acceptable hold time. The maximum conversion rate may be reduced due to the total readback time.



Figure 43. Chain Mode Without Busy Indicator Connection Diagram

<span id="page-21-1"></span>

<span id="page-21-2"></span>Figure 44. Chain Mode Without Busy Indicator Serial Interface Timing

# <span id="page-22-0"></span>**CHAIN MODE WITH BUSY INDICATOR**

This mode can also be used to daisy-chain multiple [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) devices on a 3-wire serial interface while providing a busy indicator. This feature is useful for reducing component count and wiring connections, for example, in isolated multiconverter applications or for systems with a limited interfacing capacity. Data readback is analogous to clocking a shift register.

A connection diagram example using thre[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) devices is shown i[n Figure 45,](#page-22-2) and the corresponding timing is given in [Figure 46.](#page-22-1) 

When SDI and CNV are low, SDO is driven low. With SCK high, a rising edge on CNV initiates a conversion, selects the chain mode, and enables the busy indicator feature. In this mode, CNV is held high during the conversion phase and the subsequent data readback. When all ADCs in the chain have

completed their conversions, the SDO pin of the ADC closest to the digital host (see the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) ADC labeled C i[n Figure 45\)](#page-22-2) is driven high. This transition on SDO can be used as a busy indicator to trigger the data readback controlled by the digital host. Th[e AD7691 t](http://www.analog.com/AD7691?doc=AD7691.pdf)hen enters the acquisition phase and powers down. The data bits stored in the internal shift register are clocked out, MSB first, by subsequent SCK falling edges. For each ADC, SDI feeds the input of the internal shift register and is clocked by the SCK falling edge. Each ADC in the chain outputs its data MSB first, and  $18 \times N + 1$  clocks are required to readback the N ADCs. Although the rising edge can be used to capture the data, a digital host using the SCK falling edge allows a faster reading rate and, consequently, more [AD7691 d](http://www.analog.com/AD7691?doc=AD7691.pdf)evices in the chain, provided the digital host has an acceptable hold time.



Figure 45. Chain Mode with Busy Indicator Connection Diagram

<span id="page-22-2"></span>

<span id="page-22-1"></span>Figure 46. Chain Mode with Busy Indicator Serial Interface Timing

# <span id="page-23-1"></span><span id="page-23-0"></span>APPLICATION HINTS **LAYOUT**

The printed circuit board that houses th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) should be designed so that the analog and digital sections are separated and confined to certain areas of the board. The pin configuration of the [AD7691,](http://www.analog.com/AD7691?doc=AD7691.pdf) with its analog signals on the left side and its digital signals on the right side, eases this task.

Avoid running digital lines under the device because this couples noise onto the die unless a ground plane under th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) is used as a shield. Fast switching signals, such as CNV or clocks, should not run near analog signal paths. Crossover of digital and analog signals should be avoided.

At least one ground plane should be used. It can be common or split between the digital and analog sections. In the latter case, the planes should be joined underneath the [AD7691.](http://www.analog.com/AD7691?doc=AD7691.pdf)

The [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) voltage reference input, REF, has a dynamic input impedance and should be decoupled with minimal parasitic inductances. This is done by placing the reference decoupling ceramic capacitor close to, ideally right up against, the REF and GND pins and connecting them with wide, low impedance traces.

Finally, the power supplies, VDD and VIO, of th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) should be decoupled with ceramic capacitors, typically 100 nF, placed close to the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) and connected using short, wide traces to provide low impedance paths and to reduce the effect of glitches on the power supply lines.

An example layout following these rules is shown i[n Figure 47](#page-23-3) an[d Figure 48.](#page-23-4)

# <span id="page-23-2"></span>**EVALUATING TH[E AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) PERFORMANCE**

Other recommended layouts for th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) are outlined in the documentation of the evaluation board for the [AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) [\(EVAL-AD7691SDZ\)](http://www.analog.com/eval-AD7691sdz?doc=AD7691.pdf). The evaluation board package includes a fully assembled and tested evaluation board, documentation, and software for controlling the board from a PC via the [EVAL-SDP-CB1Z.](http://www.analog.com/EVAL-SDP-CB1Z?doc=AD7691.pdf)



*Figure 47. Example Layout of th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) (Top Layer)*

<span id="page-23-4"></span><span id="page-23-3"></span>

*Figure 48. Example Layout of th[e AD7691](http://www.analog.com/AD7691?doc=AD7691.pdf) (Bottom Layer)*

# <span id="page-24-0"></span>OUTLINE DIMENSIONS



*Dimensions shown in millimeters*

## <span id="page-24-1"></span>**ORDERING GUIDE**



 $1 Z =$  RoHS Compliant Part.

<sup>2</sup> Th[e EVAL-AD7691SDZ](http://www.analog.com/eval-AD7691sdz?doc=AD7691.pdf) can be used as a standalone evaluation board or in conjunction with th[e EVAL-SDP-CB1Z](http://www.analog.com/EVAL-SDP-CB1Z?doc=AD7691.pdf) for evaluation/demonstration purposes.

<sup>3</sup> Th[e EVAL-SDP-CB1Z](http://www.analog.com/EVAL-SDP-CB1Z?doc=AD7691.pdf) allows a PC to control and communicate with all Analog Devices evaluation boards ending in the SD designator.

# **NOTES**

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