

Data Sheet

OP177

FEATURES

Ultralow offset voltage

$T_A = 25^\circ\text{C}$, 25 μV maximum

Outstanding offset voltage drift 0.3 $\mu\text{V}/^\circ\text{C}$ maximum

Excellent open-loop gain and gain linearity

12 V/ μV typical

CMRR: 130 dB minimum

PSRR: 115 dB minimum

Low supply current 2.0 mA maximum

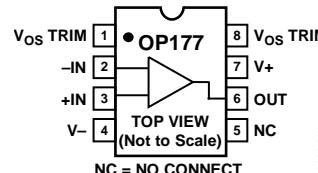
Fits industry-standard precision op amp sockets

GENERAL DESCRIPTION

The OP177 features one of the highest precision performance of any op amp currently available. Offset voltage of the OP177 is only 25 μV maximum at room temperature. The ultralow V_{os} of the OP177 combines with its exceptional offset voltage drift (TC V_{os}) of 0.3 $\mu\text{V}/^\circ\text{C}$ maximum to eliminate the need for external V_{os} adjustment and increases system accuracy over temperature.

The OP177 open-loop gain of 12 V/ μV is maintained over the full ± 10 V output range. CMRR of 130 dB minimum, PSRR of 120 dB minimum, and maximum supply current of 2 mA are just a few examples of the excellent performance of this

PIN CONFIGURATION



00289-001

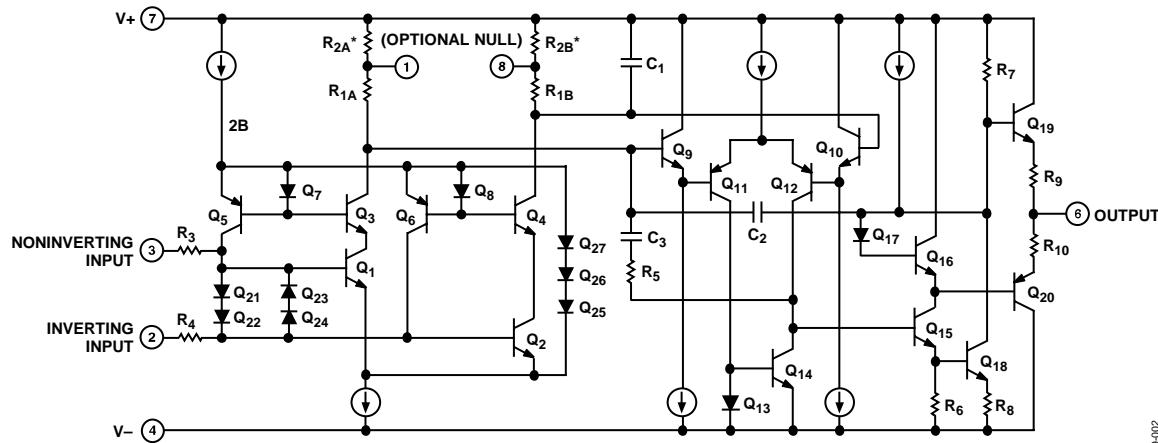
Figure 1. 8-Lead PDIP (P-Suffix),
8-Lead SOIC (S-Suffix)

operational amplifier. The combination of outstanding specifications of the OP177 ensures accurate performance in high closed-loop gain applications.

This low noise, bipolar input op amp is also a cost effective alternative to chopper-stabilized amplifiers. The OP177 provides chopper-type performance without the usual problems of high noise, low frequency chopper spikes, large physical size, limited common-mode input voltage range, and bulky external storage capacitors.

The OP177 is offered in the -40°C to $+85^\circ\text{C}$ extended industrial temperature ranges. This product is available in 8-lead PDIP, as well as the space saving 8-lead SOIC.

FUNCTIONAL BLOCK DIAGRAM



00289-002

Figure 2. Simplified Schematic

Rev. G

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3/09—Rev. E to Rev. F

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5/06—Rev. D to Rev. E

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1/05—Rev. B to Rev. C

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11/95—Rev. 0: Initial Version

SPECIFICATIONS

ELECTRICAL CHARACTERISTICS

@ $V_S = \pm 15$ V, $T_A = 25^\circ\text{C}$, unless otherwise noted.

Table 1.

| Parameter | Symbol | Conditions | OP177F | | | OP177G | | | Unit |
|-------------------------------------|-----------------------------|--|------------|------------|-----|------------|------------|------|-------------------------|
| | | | Min | Typ | Max | Min | Typ | Max | |
| INPUT OFFSET VOLTAGE | V_{os} | | | 10 | 25 | | 20 | 60 | μV |
| LONG-TERM INPUT OFFSET ¹ | | | | | | | | | |
| Voltage Stability | $\Delta V_{os}/\text{time}$ | | | 0.3 | | | 0.4 | | $\mu\text{V}/\text{mo}$ |
| INPUT OFFSET CURRENT | I_{os} | | | 0.3 | 1.5 | | 0.3 | 2.8 | nA |
| INPUT BIAS CURRENT | I_B | | -0.2 | +1.2 | +2 | -0.2 | +1.2 | +2.8 | nA |
| INPUT NOISE VOLTAGE | e_n | $f_0 = 1 \text{ Hz to } 100 \text{ Hz}^2$ | | 118 | 150 | | 118 | 150 | nV rms |
| INPUT NOISE CURRENT | i_n | $f_0 = 1 \text{ Hz to } 100 \text{ Hz}^2$ | | 3 | 8 | | 3 | 8 | pA rms |
| INPUT RESISTANCE | | | | | | | | | |
| Differential Mode ³ | R_{IN} | | 26 | 45 | | 18.5 | 45 | | $\text{M}\Omega$ |
| INPUT RESISTANCE COMMON MODE | R_{INCM} | | | 200 | | | 200 | | $\text{G}\Omega$ |
| INPUT VOLTAGE RANGE ⁴ | IVR | | ± 13 | ± 14 | | ± 13 | ± 14 | | V |
| COMMON-MODE REJECTION RATIO | $CMRR$ | $V_{CM} = \pm 13 \text{ V}$ | 130 | 140 | | 115 | 140 | | dB |
| POWER SUPPLY REJECTION RATIO | $PSRR$ | $V_S = \pm 3 \text{ V to } \pm 18 \text{ V}$ | 115 | 125 | | 110 | 120 | | dB |
| LARGE SIGNAL VOLTAGE GAIN | A_{vo} | $R_L \geq 2 \text{ k}\Omega, V_O = \pm 10 \text{ V}^5$ | 5000 | 12,000 | | 2000 | 6000 | | V/mV |
| OUTPUT VOLTAGE SWING | V_o | $R_L \geq 10 \text{ k}\Omega$ | ± 13.5 | ± 14.0 | | ± 13.5 | ± 14.0 | | V |
| | | $R_L \geq 2 \text{ k}\Omega$ | ± 12.5 | ± 13.0 | | ± 12.5 | ± 13.0 | | V |
| | | $R_L \geq 1 \text{ k}\Omega$ | ± 12.0 | ± 12.5 | | ± 12.0 | ± 12.5 | | V |
| SLEW RATE ² | SR | $R_L \geq 2 \text{ k}\Omega$ | 0.1 | 0.3 | | 0.1 | 0.3 | | $\text{V}/\mu\text{s}$ |
| CLOSED-LOOP BANDWIDTH ² | BW | $A_{VCL} = 1$ | 0.4 | 0.6 | | 0.4 | 0.6 | | MHz |
| OPEN-LOOP OUTPUT RESISTANCE | R_o | | | 60 | | | 60 | | Ω |
| POWER CONSUMPTION | P_D | $V_S = \pm 15 \text{ V, no load}$ | 50 | 60 | | 50 | 60 | | mW |
| | | $V_S = \pm 3 \text{ V, no load}$ | 3.5 | 4.5 | | 3.5 | 4.5 | | mW |
| SUPPLY CURRENT | I_{SY} | $V_S = \pm 15 \text{ V, no load}$ | 1.6 | 2 | | 1.6 | 2 | | mA |
| OFFSET ADJUSTMENT RANGE | | $R_P = 20 \text{ k}\Omega$ | | ± 3 | | | ± 3 | | mV |

¹ Long-term input offset voltage stability refers to the averaged trend line of V_{os} vs. time over extended periods after the first 30 days of operation. Excluding the initial hour of operation, changes in V_{os} during the first 30 operating days are typically less than 2.0 μV .

² Sample tested.

³ Guaranteed by design.

⁴ Guaranteed by CMRR test condition.

⁵ To ensure high open-loop gain throughout the $\pm 10 \text{ V}$ output range, A_{vo} is tested at $-10 \text{ V} \leq V_o \leq 0 \text{ V}, 0 \text{ V} \leq V_o \leq +10 \text{ V}$, and $-10 \text{ V} \leq V_o \leq +10 \text{ V}$.

@ $V_S = \pm 15$ V, $-40^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$, unless otherwise noted.

Table 2.

| Parameter | Symbol | Conditions | OP177F | OP177G | | | |
|---|------------|--|----------|------------|----------|------------|------------------------------|
| | | | Min | Typ | Max | Unit | |
| INPUT | | | | | | | |
| Input Offset Voltage | V_{OS} | | 15 | 40 | 20 | 100 | μV |
| Average Input Offset Voltage Drift ¹ | TCV_{OS} | | 0.1 | 0.3 | 0.7 | 1.2 | $\mu\text{V}/^\circ\text{C}$ |
| Input Offset Current | I_{OS} | | 0.5 | 2.2 | 0.5 | 4.5 | nA |
| Average Input Offset Current Drift ² | TCI_{OS} | | 1.5 | 40 | 1.5 | 85 | $\text{pA}/^\circ\text{C}$ |
| Input Bias Current | I_B | | -0.2 | +2.4 | +4 | +2.4 | ± 6 |
| Average Input Bias Current Drift ² | TCI_B | | 8 | 40 | 15 | 60 | $\text{pA}/^\circ\text{C}$ |
| Input Voltage Range ³ | IVR | | ± 13 | ± 13.5 | ± 13 | ± 13.5 | V |
| COMMON-MODE REJECTION RATIO | CMRR | $V_{CM} = \pm 13$ V | 120 | 140 | 110 | 140 | dB |
| POWER SUPPLY REJECTION RATIO | PSRR | $V_S = \pm 3$ V to ± 18 V | 110 | 120 | 106 | 115 | dB |
| LARGE-SIGNAL VOLTAGE GAIN ⁴ | A_{VO} | $R_L \geq 2 \text{ k}\Omega, V_0 = \pm 10$ V | 2000 | 6000 | 1000 | 4000 | V/mV |
| OUTPUT VOLTAGE SWING | V_O | $R_L \geq 2 \text{ k}\Omega$ | ± 12 | ± 13 | ± 12 | ± 13 | V |
| POWER CONSUMPTION | P_D | $V_S = \pm 15$ V, no load | 60 | 75 | 60 | 75 | mW |
| SUPPLY CURRENT | I_{SV} | $V_S = \pm 15$ V, no load | 20 | 2.5 | 2 | 2.5 | mA |

¹ TCV_{OS} is sample tested.

² Guaranteed by endpoint limits.

³ Guaranteed by CMRR test condition.

⁴ To ensure high open-loop gain throughout the ± 10 V output range, A_{VO} is tested at $-10 \text{ V} \leq V_0 \leq 0 \text{ V}, 0 \text{ V} \leq V_0 \leq +10 \text{ V}$, and $-10 \text{ V} \leq V_0 \leq +10 \text{ V}$.

TEST CIRCUITS

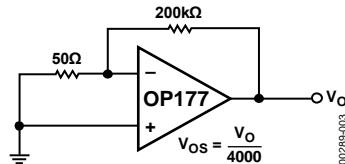


Figure 3. Typical Offset Voltage Test Circuit

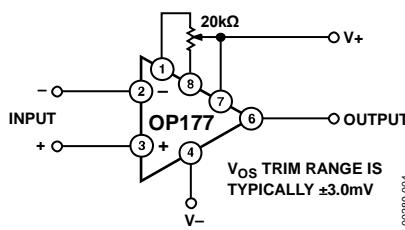


Figure 4. Optional Offset Nulling Circuit

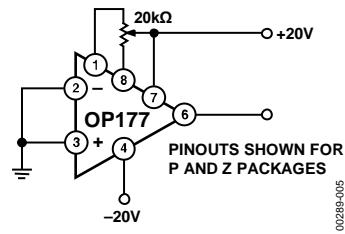


Figure 5. Burn-In Circuit

ABSOLUTE MAXIMUM RATINGS

Table 3.

| Parameter | Ratings |
|---|---|
| Supply Voltage | $\pm 22\text{ V}$ |
| Internal Power Dissipation ¹ | 500 mW |
| Differential Input Voltage | $\pm 30\text{ V}$ |
| Input Voltage | $\pm 22\text{ V}$ |
| Output Short-Circuit Duration | Indefinite |
| Storage Temperature Range | -65°C to $+125^\circ\text{C}$ |
| Operating Temperature Range | -40°C to $+85^\circ\text{C}$ |
| Lead Temperature (Soldering, 60 sec) | 300°C |
| DICE Junction Temperature (T_j) | -65°C to $+150^\circ\text{C}$ |

¹ For supply voltages less than $\pm 22\text{ V}$, the absolute maximum input voltage is equal to the supply voltage.

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

THERMAL RESISTANCE

θ_{JA} is specified for worst-case mounting conditions, that is, θ_{JA} is specified for device in socket for PDIP; θ_{JA} is specified for device soldered to printed circuit board for SOIC package.

Table 4. Thermal Resistance

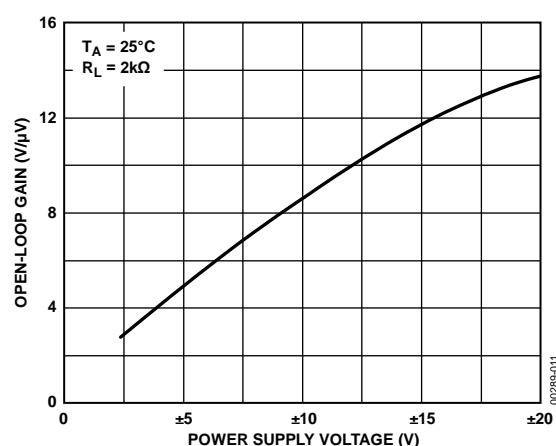
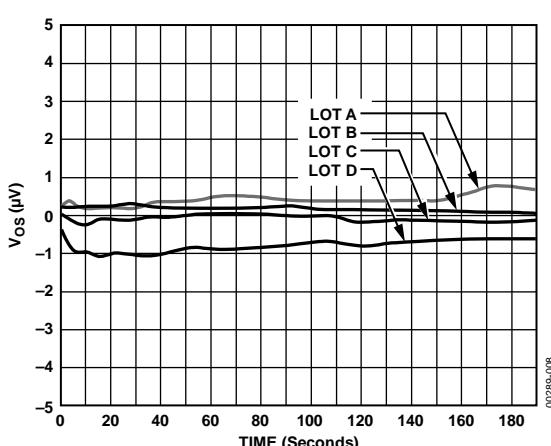
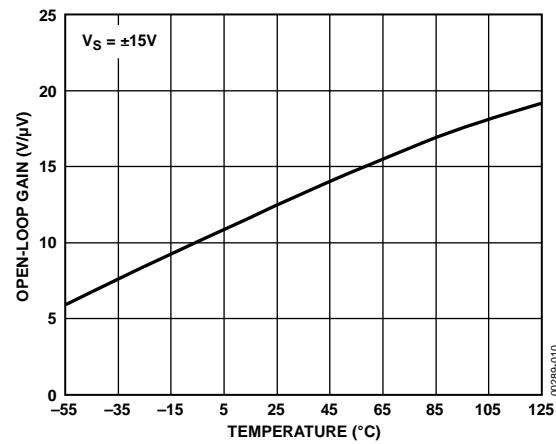
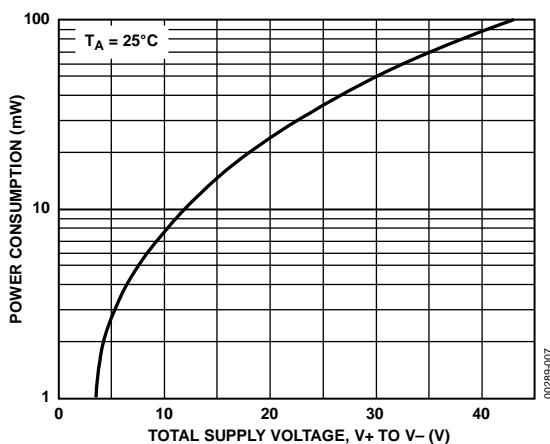
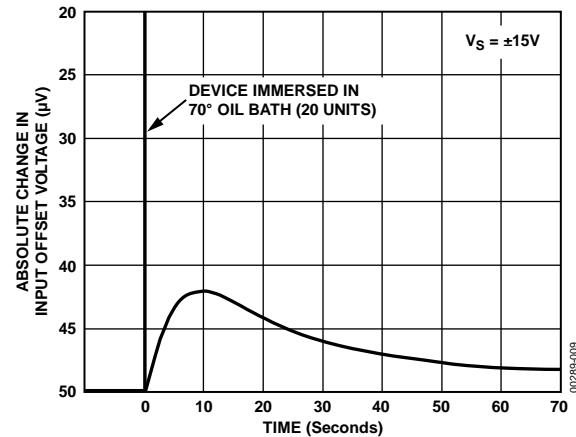
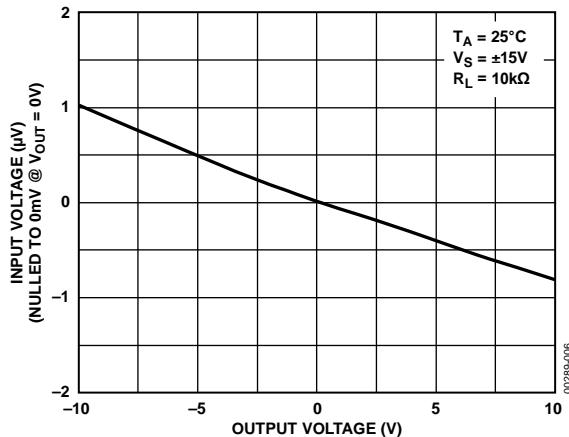
| Package Type | θ_{JA} | θ_{JC} | Unit |
|------------------------|---------------|---------------|------|
| 8-Lead PDIP (P-Suffix) | 103 | 43 | °C/W |
| 8-Lead SOIC (S-Suffix) | 158 | 43 | °C/W |

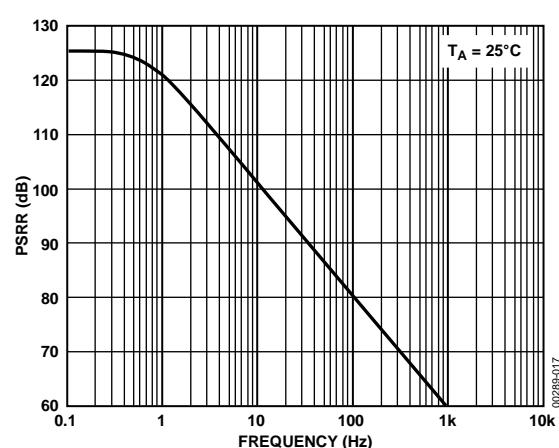
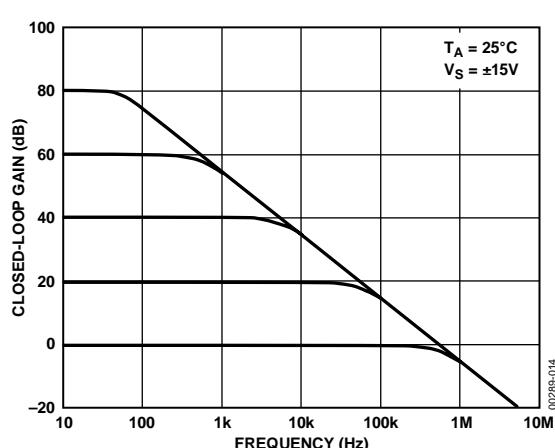
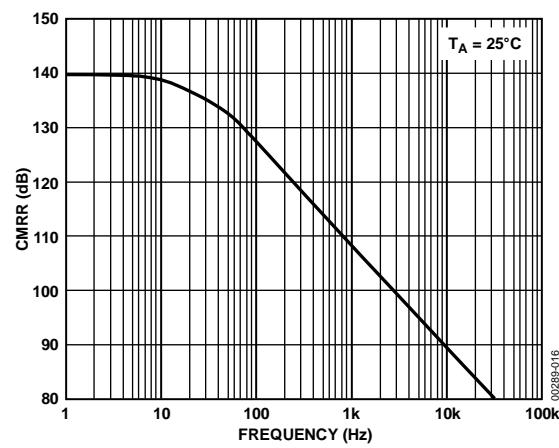
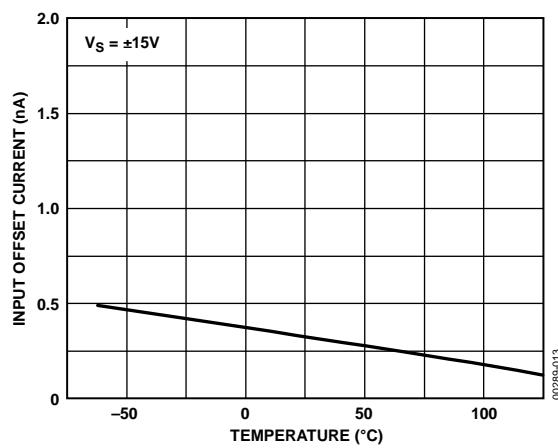
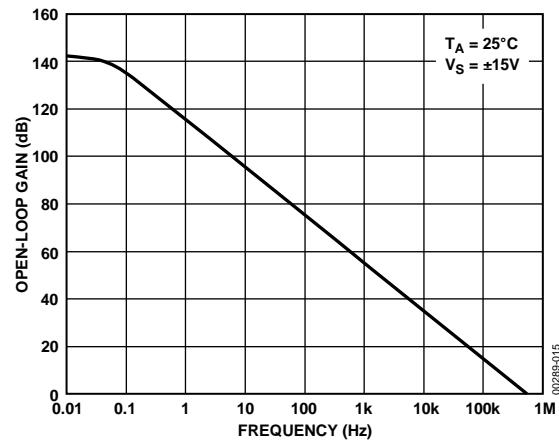
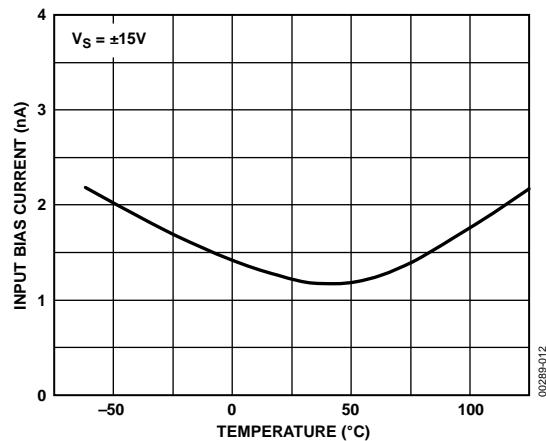
ESD CAUTION

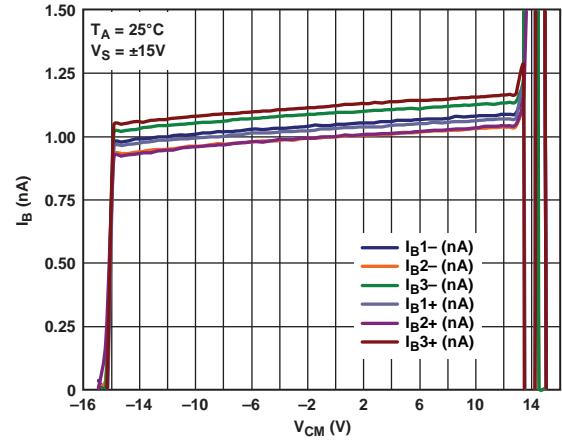
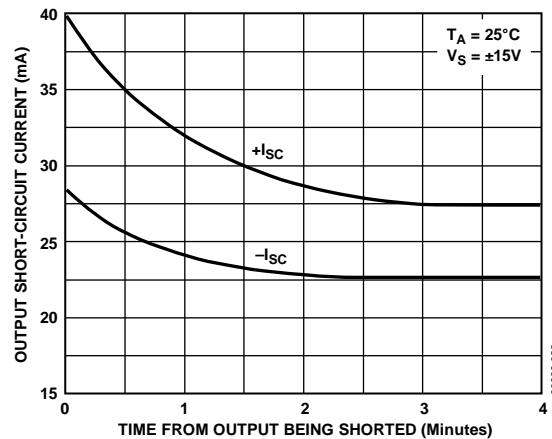
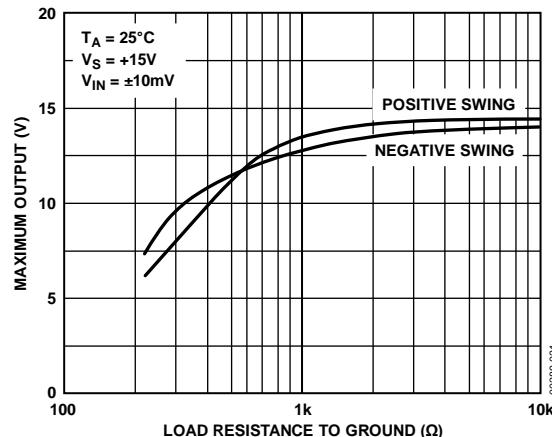
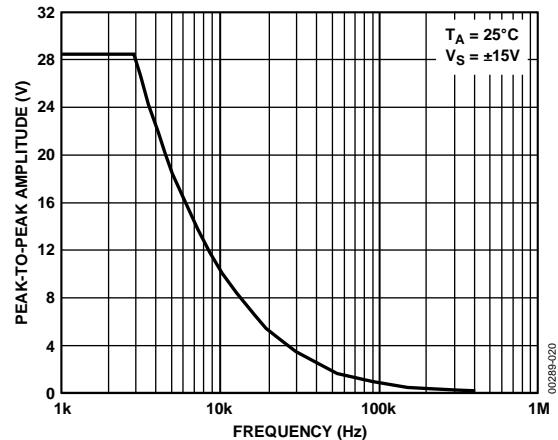
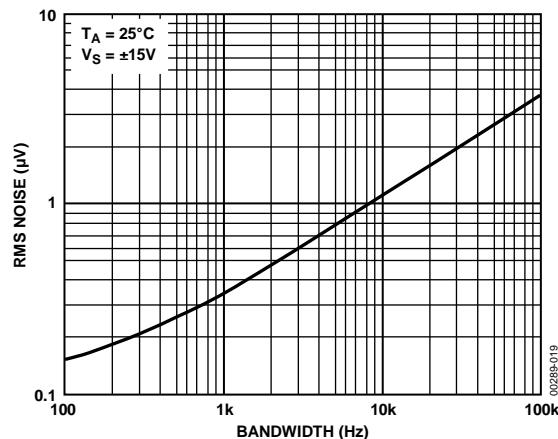
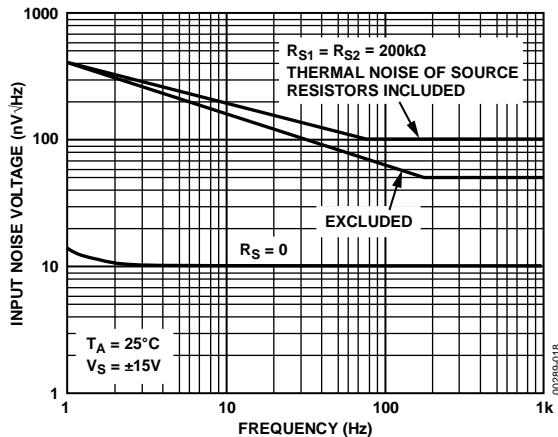
ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.



TYPICAL PERFORMANCE CHARACTERISTICS







APPLICATIONS INFORMATION

GAIN LINEARITY

The actual open-loop gain of most monolithic op amps varies at different output voltages. This nonlinearity causes errors in high closed-loop gain circuits.

It is important to know that the manufacturer's Avo specification is only a part of the solution because all automated testers use endpoint testing and, therefore, show only the average gain. For example, Figure 24 shows a typical precision op amp with a respectable open-loop gain of 650 V/mV. However, the gain is not constant through the output voltage range, causing nonlinear errors. An ideal op amp shows a horizontal scope trace.

Figure 25 shows the OP177 output gain linearity trace with its truly impressive average Avo of 12,000 V/mV. The output trace is virtually horizontal at all points, assuring extremely high gain accuracy. Analog Devices also performs additional testing to ensure consistent high open-loop gain at various output voltages. Figure 26 is a simple open-loop gain test circuit.

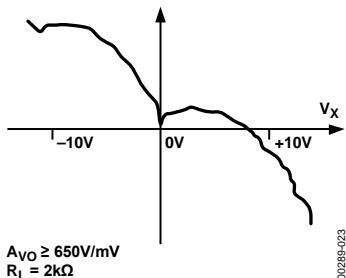


Figure 24. Typical Precision Op Amp

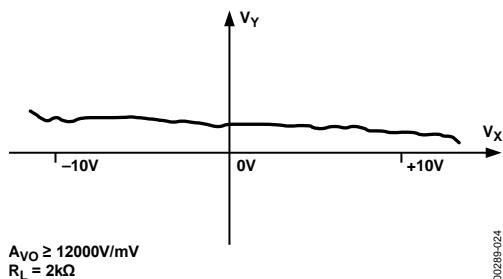


Figure 25. Output Gain Linearity Trace

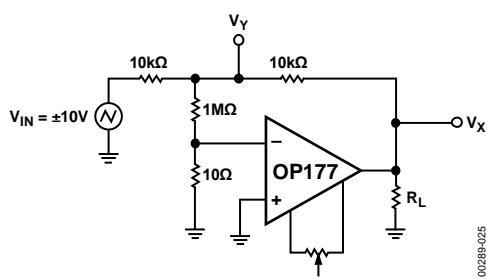


Figure 26. Open-Loop Gain Linearity Test Circuit

THERMOCOUPLE AMPLIFIER WITH COLD-JUNCTION COMPENSATION

An example of a precision circuit is a thermocouple amplifier that must accurately amplify very low level signals without introducing linearity and offset errors to the circuit. In this circuit, an S-type thermocouple with a Seebeck coefficient of $10.3 \mu\text{V}/^\circ\text{C}$ produces 10.3 mV of output voltage at a temperature of 1000°C . The amplifier gain is set at 973.16, thus, it produces an output voltage of 10.024 V . Extended temperature ranges beyond 1500°C are accomplished by reducing the amplifier gain. The circuit uses a low cost diode to sense the temperature at the terminating junctions and, in turn, compensates for any ambient temperature change. The OP177, with its high open-loop gain plus low offset voltage and drift, combines to yield a precise temperature sensing circuit. Circuit values for other thermocouple types are listed in Table 5.

Table 5.

| Thermocouple Type | Seebeck Coefficient | R1 | R2 | R7 | R9 |
|-------------------|-----------------------------------|--------------|------------------------|------------------------|------------------------|
| K | $39.2 \mu\text{V}/^\circ\text{C}$ | 110Ω | $5.76 \text{ k}\Omega$ | $102 \text{ k}\Omega$ | $269 \text{ k}\Omega$ |
| J | $50.2 \mu\text{V}/^\circ\text{C}$ | 100Ω | $4.02 \text{ k}\Omega$ | $80.6 \text{ k}\Omega$ | $200 \text{ k}\Omega$ |
| S | $10.3 \mu\text{V}/^\circ\text{C}$ | 100Ω | $20.5 \text{ k}\Omega$ | $392 \text{ k}\Omega$ | $1.07 \text{ M}\Omega$ |

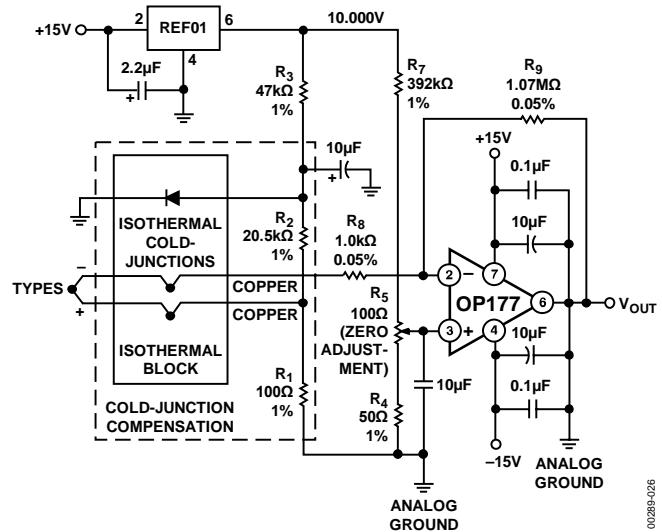


Figure 27. Thermocouple Amplifier with Cold Junction Compensation

PRECISION HIGH GAIN DIFFERENTIAL AMPLIFIER

The high gain, gain linearity, CMRR, and low TCV_{os} of the OP177 make it possible to obtain performance not previously available in single stage, very high gain amplifier applications. See Figure 28.

For best CMR, $\frac{R1}{R2}$ must equal $\frac{R3}{R4}$

In this example, with a 10 mV differential signal, the maximum errors are listed in Table 6.

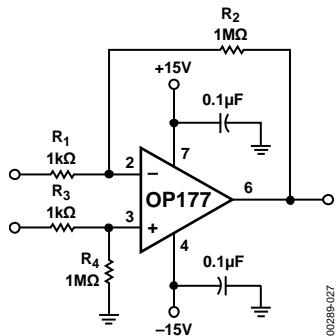


Figure 28. Precision High Gain Differential Amplifier

Table 6. High Gain Differential Amp Performance

| Type | Amount |
|----------------------------|-------------------------|
| Common-Mode Voltage | 0.1%/V |
| Gain Linearity, Worst Case | 0.02% |
| TCV _{os} | 0.0003%/ [°] C |
| TCI _{os} | 0.008%/ [°] C |

ISOLATING LARGE CAPACITIVE LOADS

The circuit shown in Figure 29 reduces maximum slew rate but allows driving capacitive loads of any size without instability. Because the 100 Ω resistor is inside the feedback loop, its effect on output impedance is reduced to insignificance by the high open loop gain of the OP177.

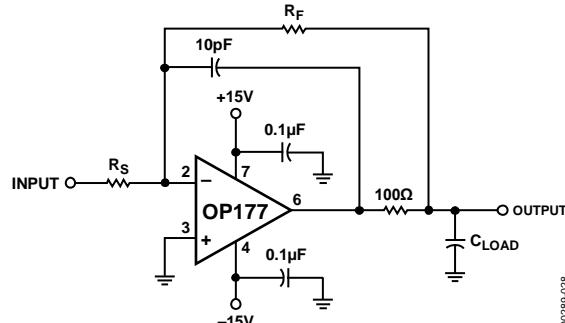


Figure 29. Isolating Capacitive Loads

BILATERAL CURRENT SOURCE

The current sources shown in Figure 30 supply both positive and negative currents into a grounded load.

Note that

$$Z_o = \frac{R5 \left(\frac{R4}{R2} + 1 \right)}{\frac{R5 + R4}{R2} - \frac{R3}{R1}}$$

and that for Z_o to be infinite

$$\frac{R5 + R4}{R2} \text{ must} = \frac{R3}{R1}$$

PRECISION ABSOLUTE VALUE AMPLIFIER

The high gain and low TCV_{os} assure accurate operation with inputs from microvolts to volts. In this circuit, the signal always appears as a common-mode signal to the op amps (for details, see Figure 31).

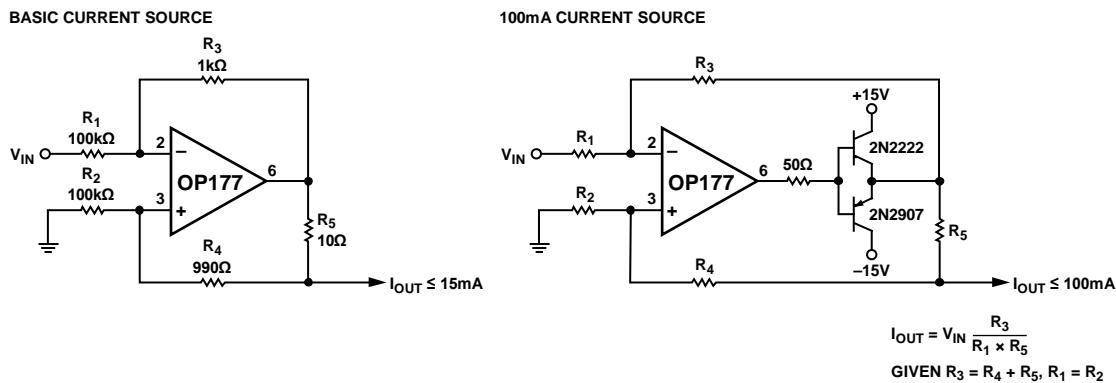


Figure 30. Bilateral Current Source

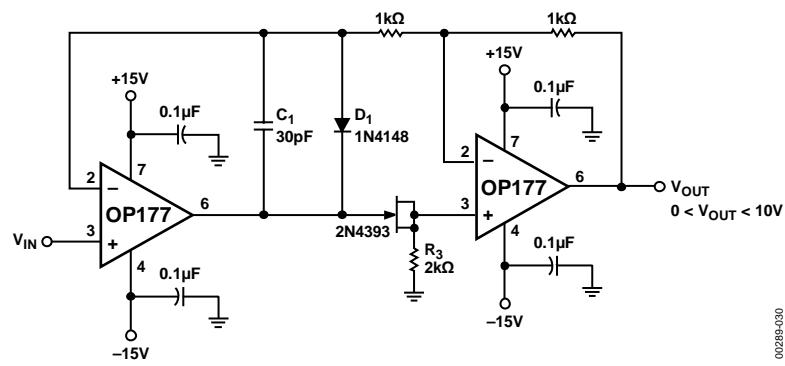


Figure 31. Precision Absolute Value Amplifier

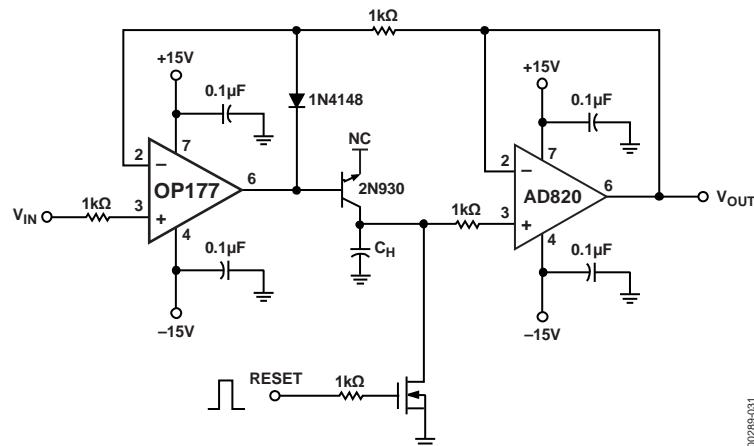


Figure 32. Precision Positive Peak Detector

PRECISION POSITIVE PEAK DETECTOR

In Figure 32, C_H must be polystyrene, Teflon®, or polyethylene to minimize dielectric absorption and leakage. The droop rate is determined by the size of C_H and the bias current of the AD820.

PRECISION THRESHOLD DETECTOR/AMPLIFIER

In Figure 33, when $V_{IN} < V_{TH}$, amplifier output swings negative, reverse biasing diode D₁. $V_{OUT} = V_{TH}$ if $R_L = \infty$. When $V_{IN} \geq V_{TH}$, the loop closes.

$$V_{OUT} = V_{TH} + (V_{IN} - V_{TH}) \left(1 + \frac{R_F}{R_S} \right)$$

C_C is selected to smooth the response of the loop.

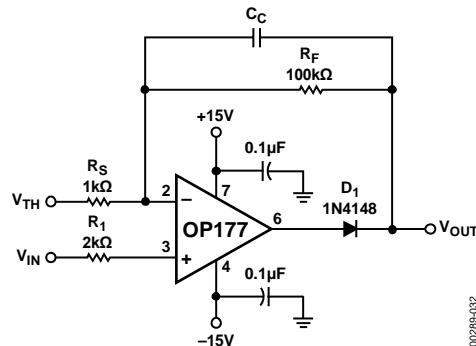
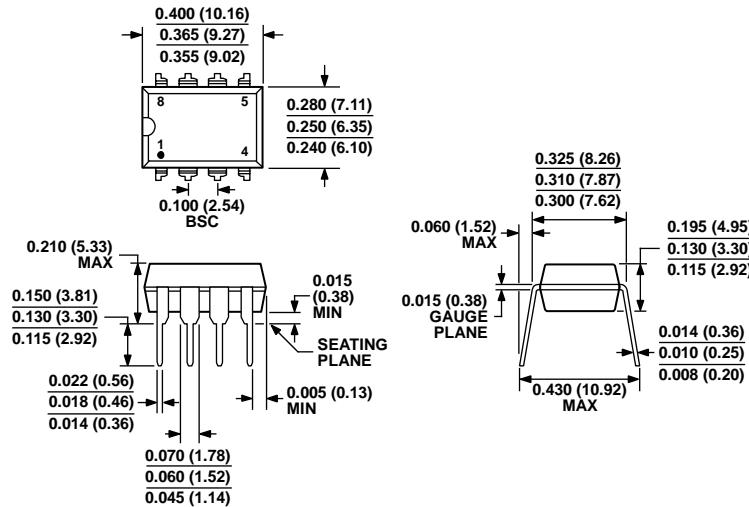


Figure 33. Precision Threshold Detector/Amplifier

00288-032

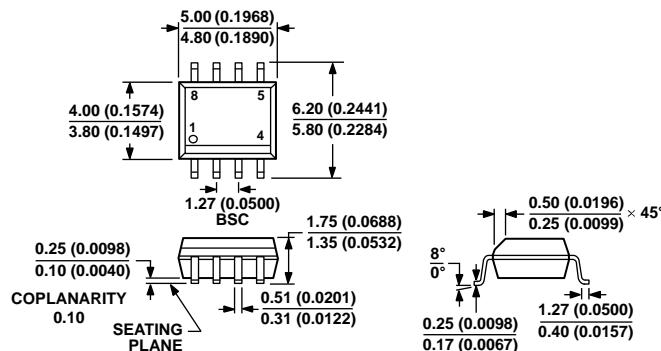
OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-001
 CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETER DIMENSIONS
 (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR
 REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.
 CORNER LEADS MAY BE CONFIGURED AS WHOLE OR HALF LEADS.

070606-A

Figure 34. 8-Lead Plastic Dual In-Line Package (PDIP)
 P-Suffix
 (N-8)
 Dimensions show in inches and (millimeters)



COMPLIANT TO JEDEC STANDARDS MS-012-AA
 CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS
 (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR
 REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

012407-A

Figure 35. 8-Lead Standard Small Outline Package (SOIC_N)
 S-Suffix
 (R-8)
 Dimensions shown in millimeters and (inches)

ORDERING GUIDE

| Model ¹ | Temperature Range | Package Description | Package Option |
|--------------------|-------------------|---------------------|----------------|
| OP177FPZ | -40°C to +85°C | 8-Lead PDIP | P-Suffix (N-8) |
| OP177GPZ | -40°C to +85°C | 8-Lead PDIP | P-Suffix (N-8) |
| OP177FSZ | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177FSZ-REEL | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177FSZ-REEL7 | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177GS | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177GS-REEL | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177GS-REEL7 | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177GSZ | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177GSZ-REEL | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |
| OP177GSZ-REEL7 | -40°C to +85°C | 8-Lead SOIC_N | S-Suffix (R-8) |

¹ Z = RoHS Compliant Part.

NOTES

NOTES



Компания «ЭлектроПласт» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Оперативные поставки широкого спектра электронных компонентов отечественного и импортного производства напрямую от производителей и с крупнейших мировых складов;
- Поставка более 17-ти миллионов наименований электронных компонентов;
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Техническая поддержка проекта, помошь в подборе аналогов, поставка прототипов;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- Лицензия ФСБ на осуществление работ с использованием сведений, составляющих государственную тайну;
- Поставка специализированных компонентов (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Aeroflex, Peregrine, Syfer, Eurofarad, Texas Instrument, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Помимо этого, одним из направлений компании «ЭлектроПласт» является направление «Источники питания». Мы предлагаем Вам помошь Конструкторского отдела:

- Подбор оптимального решения, техническое обоснование при выборе компонента;
- Подбор аналогов;
- Консультации по применению компонента;
- Поставка образцов и прототипов;
- Техническая поддержка проекта;
- Защита от снятия компонента с производства.



Как с нами связаться

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