## AL8807A <br> HIGH EFFICIENCY LOW EMI WIDE ANALOG DIMMING RANGE 36V 1A/1.3A BUCK LED DRIVER

## Pin Assignments



## Applications

- General Illumination Lamps
- 12V Powered LED Lamps
- Wide Analog Dimming Range LED Lamps

Notes: 1. No purposely added lead. Fully EU Directive 2002/95/EC (RoHS) \& 2011/65/EU (RoHS 2) compliant.
2. See http://www.diodes.com for more information about Diodes Incorporated's definitions of Halogen and Antimony free, "Green" and Lead-Free.
3. Halogen and Antimony free "Green" products are defined as those which contain <900ppm bromine, <900ppm chlorine ( $<1500 \mathrm{ppm}$ total $\mathrm{Br}+\mathrm{Cl}$ ) and <1000ppm antimony compounds.

## Typical Applications Circuit



## Pin Descriptions

| Pin Name | Pin Number |  | Function |
| :---: | :---: | :---: | :---: |
|  | SOT25 | MSOP-8EP |  |
| SW | 1 | 5,6 | Switch Pin. Connect inductor/freewheeling diode here, minimizing track length at this pin to reduce EMI. |
| GND | 2 | 2, 3 | GND Pin |
| CTRL | 3 | 4 | LED current Analog Dimming Control Input. - No PWM dimming function. <br> Connected to internal $2.5 \mathrm{~V} \mathrm{~V}_{\text {REF }}$ via $50 \mathrm{k} \Omega$ resistor. So if left open circuit $\mathrm{V}_{\mathrm{CTRL}}=\mathrm{V}_{\mathrm{REF}}=2.5 \mathrm{~V}$ and $100 \%$ LED current is achieved - giving nominal average output current loutnom $=0.1 / \mathrm{Rs}$ <br> For Analog dimming drive with analog voltage $<2.5 \mathrm{~V}$ <br> ( $0.25 \mathrm{~V}<\mathrm{V}_{\text {CTRL }}<2.5 \mathrm{~V}$ adjusts output current from $10 \%$ to $100 \%$ of $\mathrm{I}_{\text {OUTnom. }}$. Device will dim the LED current lower than this level but at reduced accuracy. Some devices will not totally turn off the LED current. <br> Soft-start can be implemented by connecting a capacitor to CTRL pin. The amount of soft-start is dependent on ramp-up of input supply voltage and capacitor on CTRL pin. See apps section. |
| SET | 4 | 1 | Set Nominal Output Current Pin. Configure the output current of the device. |
| VIN | 5 | 8 | Input Supply Pin. Must be locally decoupled to GND with $\geq 2.2 \mu \mathrm{~F}$ X7R ceramic capacitor - see applications section for more information. |
| EP | - | EP | Exposed pad/TAB. It should be connected to GND and thermal mass for enhanced thermal impedance. It should not be used as electrical ground conduction path. |
| N/C | - | 7 | No connection - may be connected to GND. |

## Functional Block Diagram



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Absolute Maximum Ratings ( $\varrho_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)

| Symbol | Parameter | Ratings | Unit |
| :---: | :---: | :---: | :---: |
| ESD HBM | Human Body Model ESD Protection | 2.5 | kV |
| ESD MM | Machine Model ESD Protection | 200 | V |
| $\mathrm{V}_{\text {IN }}$ | Continuous $\mathrm{V}_{\text {IN }}$ Pin Voltage Relative to GND | -0.3 to +40 | V |
| $\mathrm{V}_{\text {Sw }}$ | SW Voltage Relative to GND | -0.3 to +40 | V |
| $\mathrm{V}_{\text {CTRL }}$ | CTRL Pin Input Voltage | -0.3 to +6 | V |
|  | DC or RMS Switch Current ${ }^{\text {SOT25 }}$ | 1.25 | A |
| ISW-RMS | DC or RMS Switch Current | 1.5 |  |
| ISW-PK | Peak Switch Current (< 10\% duty cycle) | 2.5 | A |
| $\mathrm{T}_{\mathrm{J}}$ | Junction Temperature | 150 | ${ }^{\circ} \mathrm{C}$ |
| TLEAD | Lead Temperature Soldering | 300 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {ST }}$ | Storage Temperature Range | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |

Caution: Stresses greater than the 'Absolute Maximum Ratings' specified above, may cause permanent damage to the device. These are stress ratings only; functional operation of the device at these or any other conditions exceeding those indicated in this specification is not implied. Device reliability may be affected by exposure to absolute maximum rating conditions for extended periods of time.
Semiconductor devices are ESD sensitive and may be damaged by exposure to ESD events. Suitable ESD precautions should be taken when handling and transporting these devices.

Recommended Operating Conditions (@T $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)

| Symbol | Parameter |  | Min | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | Operating Input Voltage |  | 6.0 | 36 | V |
| $\mathrm{V}_{\text {CTRL }}$ | CTRL Pin Input Voltage Range for 10\% to 100\% ANALOG Dimming (Note 4) |  | 0.25 | 2.50 | V |
| $\mathrm{f}_{\text {sw }}$ | Maximum Switching Frequency at 100\% dimming |  |  | 0.7 | MHz |
| Isw | Continuous Switch Current (Note 5) | SOT25 |  | 1 | A |
|  |  | MSOP-8EP |  | 1.3 |  |
| $\mathrm{T}_{\mathrm{J}}$ | Junction Temperature Range |  | -40 | +125 | ${ }^{\circ} \mathrm{C}$ |

Notes: 4. AL8807A analog dimming range extends below $10 \%$ but at reduced LED current accuracies and may not turn completely off. Switching frequencies will also be increased.
5. Maximum switch current is dependent on power dissipation and junction temperature.

Electrical Characteristics (@T $\mathrm{A}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)


Notes: 6. AL8807A does not have a low power standby mode but current consumption is reduced when output is not being switched.
7. Refer to Figure 40 for the device derating curve.
8. Test condition for SOT25: Device mounted on FR-4 PCB ( $25 \mathrm{~mm} \times 25 \mathrm{~mm} 10 z$ copper, minimum recommended pad layout on top layer and thermal vias to bottom layer ground plane. For better thermal performance, larger copper pad for heat-sink is needed
9. Test condition for MSOP-8EP: Device mounted on FR-4 PCB ( $51 \mathrm{~mm} \times 51 \mathrm{~mm} 20 \mathrm{z}$ copper, minimum recommended pad layout on top layer and thermal vias to bottom layer with maximum area ground plane. For better thermal performance, larger copper pad for heat-sink is needed
10. Dominant conduction path via Gnd pin (pin 2).
11. Dominant conduction path via exposed pad.

## Typical Performance Characteristics ( $@ \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)



Figure 1 Supply Current (not switching) vs. Input Voltage


Figure $3 \mathrm{~V}_{\mathrm{CTRL}}$ vs. Input Voltage
(CTRL pin open circuit)


Figure 5 SW R $\mathrm{DS}_{(\mathrm{ON})}$ vs. Input Voltage


Figure $2 \mathrm{I}_{\mathrm{CTRL}} \mathrm{vs} . \mathrm{V}_{\mathrm{CTRL}}$


Figure $4 \mathrm{~V}_{\text {CTRL }}$ vs. Temperature


Figure 6 SW $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}$ vs. Temperature

Typical Performance Characteristics (cont.) (@ $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)


Figure 7 SW Output Rise Time


Figure 9 LED Current (Different Sense Resistor) vs. $\mathrm{V}_{\mathrm{CTRL}}$


Figure 11 LED Current (Zoomed In) vs. $\mathrm{V}_{\text {CTRL }}$


Figure 8 SW Output Fall Time


Figure 10 LED Current (Different Inductor) vs. $\mathrm{V}_{\mathrm{CTRL}}$


Figure 12 Switching Frequency vs. $\mathrm{V}_{\mathrm{CTRL}}$

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## Typical Performance Characteristics (cont.) (@T $\mathrm{A}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)



Figure 13 Duty Cycle vs. Input Voltage


Figure 15 Switching Frequency vs. Input Voltage


Figure 17 670mALED Current vs. Input Voltage


Figure 14 Efficiency vs. Input Voltage


Figure 16 330mA LED Current vs. Input Voltage


Figure 18 1A LED Current vs. Input Voltage

## Typical Performance Characteristics ( 670 mA LED Current) ( $@ T_{A}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)



Figure 19 LED Current Deviation vs. Input Voltage


Figure 21 LED Current Deviation vs. Input Voltage


Figure 23 LED Current Deviation vs. Input Voltage


Figure 20 Switching Frequency vs. Input Voltage


Figure 22 Switching Frequency vs. Input Voltage


Figure 24 Switching Frequency vs. Input Voltage

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## Typical Performance Characteristics (1A LED Current) (@T $\mathrm{A}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)



Figure 25 LED Current Deviation vs. Input Voltage


Figure 27 LED Current Deviation vs. Input Voltage


Figure 29 LED Current Deviation vs. Input Voltage


Figure 26 Switching Frequency vs. Input Voltage


Figure 28 Switching Frequency vs. Input Voltage


Figure 30. Switching Frequency vs. Input Voltage

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## Application Information

## AL8807A Operation

The AL8807A is a hysteretic LED current switching regulator sometimes known as an equal ripple switching regulator. In normal operation, when voltage is applied at $+\mathrm{V}_{\mathrm{IN}}$ (See Figure 31), the AL8807A internal switch is turned on. Current starts to flow through sense resistor $\mathrm{R}_{1}$, inductor L1, and the LEDs. The current ramps up linearly, and the ramp rate is determined by the input voltage $+\mathrm{V}_{\mathrm{IN}}$, and the inductor L 1 (See Figure 32 ).

This rising current produces a voltage ramp across $R_{1}$. The internal circuit of the AL8807A senses the voltage across $R_{1}$ and applies a proportional voltage to the input of the internal comparator.

When this voltage reaches an internally set upper threshold, the internal switch is turned off. The inductor current continues to flow through $\mathrm{R}_{1}$, L1, the LEDs and the schottky diode D1, and back to the supply rail, but it decays, with the rate of decay determined by the forward voltage drop of the LEDs and the schottky diode.

This decaying current produces a falling voltage at $R_{1}$, which is sensed by the AL8807A. A voltage proportional to the sense voltage across $R_{1}$ is applied at the input of the internal comparator. When this voltage falls to the internally set lower threshold, the internal switch is turned on again. This switch-on-and-off cycle continues to provide the average LED current set by the sense resistor $\mathrm{R}_{1}$, with a switching current determined by the input voltage and LED chain voltage

In normal operation the off time is relatively constant (determined mainly by the LED chain voltage) with only the on-time varying as the input voltage changes. At duty cycles up to around $80 \%$ the ramp of the LED/switch current is very linear; however, as the duty cycle approaches $95 \%$ the LED current ramp starts to become more exponential. This has two effects:

1. The overall on time starts to increase lowering the overall switching frequency.
2. The average LED current starts to increase - which may impact accuracy.


Figure 31 Typical Application Circuit


Figure 32 Typical Operating Waveform (C2 not fitted)

## LED Current Control

With the CTRL pin open circuit, the LED current is determined by the resistor, R1, (see Figure 31), connected between VIN and SET. The nominal average output current in the LED(s) is defined as:

$$
\mathrm{I}_{\mathrm{LED}}=\frac{\mathrm{V}_{\mathrm{TH}}}{\mathrm{R} 1} \quad \text { where } \mathrm{V}_{\mathrm{TH}} \text { is nominally } 100 \mathrm{mV}
$$

For example for a desired LED current of 660 mA the resulting resistor is:

$$
\mathrm{R} 1=\frac{\mathrm{V}_{\mathrm{TH}}}{\mathrm{l}_{\mathrm{LED}}}=\frac{0.1}{0.66} \approx 150 \mathrm{~m} \Omega
$$

## Application Information (cont.)

## Analog Dimming

Further control of the LED current can be achieved by driving the CTRL pin with an external voltage lower than 2.5 V ; the average LED current becomes:

$$
\mathrm{I}_{\mathrm{LED}}=\frac{\mathrm{V}_{\mathrm{CTRL}}}{\mathrm{~V}_{\mathrm{REF}}} \frac{\mathrm{~V}_{\mathrm{TH}}}{\mathrm{R}_{\mathrm{SET}}}
$$

Where $V_{\text {REF }}$ is nominally 2.5 V
The LED current decreases linearly with the CTRL voltage when $\mathrm{V}_{\text {CTRL }} \leq 2.5 \mathrm{~V}$, as in Figure 9 for 2 different current levels.

Note that $100 \%$ brightness setting corresponds to $\mathrm{V}_{\mathrm{CTRL}}=\mathrm{V}_{\mathrm{REF}}$, nominally 2.5 V

If a voltage greater than 2.6 V is applied to the CTRL pin an internal clamp is activated which results in the internal reference voltage being applied to the hysteresis control circuitry. This prevents the LED current from being overdriven and will still set the LED current to approximately.

$$
I_{\text {LED }}=\frac{V_{\text {TH }}}{R_{\text {SET }}}
$$



Figure 33 LED Current vs. CTRL Pin Voltage
As the CTRL pin is reduced below 2.5 V the sense voltage will proportionally decrease. This means that the time taken for the LED/Switch current to ramp up to the upper threshold will decrease. The AL8807A, being a hysteretic converter, automatically compensates for the reduction in LED current by reducing its lower threshold voltage and therefore its off-time. It therefore remains in continuous conduction mode maintaining a better dimming accuracy than other peak-switch current control topologies.

A result of the reduced on- and off-times results in an increase of the switching frequency. This phenomenon can be seen in Figure 34.


Figure 34 Switching Frequency vs. $\mathrm{V}_{\mathrm{CTRL}}$

Ultimately at very small CTRL pin voltages the AL8807A will switch much faster than its nominal switching frequency which due to propagation delays leads to a non-linear degrading of accuracy.

The degradation in linear dimming accuracy at small CTRL pin voltages can be improved by using larger value inductors which cause the AL8807A to oscillate at lower frequencies.

A further cause of loss of linearity as small CTRL pin voltages is the internal offsets of the control loop; at a CTRL pin voltage of 0.25 V the nominal LED current sense voltage has been reduced to 10 mV

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## Application Information (cont.)

## Soft Start

The AL8807A does not have in-built soft-start action; this can be seen in Figure 35.


Figure 35 Start up without any capacitor on CTRL Pin ( $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{I}_{\mathrm{LED}}=667 \mathrm{~mA}, 2$ LEDs $)$

At power-up $\mathrm{V}_{\mathrm{IN}}$ rises exponentially, due to the bulk capacitor, the internal reference will reach 2.5 V before $\mathrm{V}_{\mathrm{IN}}$ reaches the Under-Voltage LockOut turn-on threshold at around 5.6 V . This causes the CTRL pin voltage to rise and reaches $2.5 \mathrm{~V}-100 \%$ LED current - before the AL8807A fully turns on. When the AL8807A turns on, its output switch turns causing the inductor current to increase until it reaches the upper threshold of the sense current level and the switching process begins.
Adding an external capacitor from the CTRL pin to ground will provide a soft-start delay (see Figures 36 and 37 ).


Figure 36 Soft Start


Figure 37 Soft Start with 100nF Capacitor on CTRL Pin

Adding a capacitor to the CTRL pin provides a soft-start by increasing the time taken for the CTRL voltage to rise to 2.5 V and by slowing down the rate of rise of the control voltage at the input of the comparator in the hysteresis control block (refer to Figure 36). This capacitor has 2 effects:

1. It reduces the minimum start-up current. The bigger the capacitor the lower the CTRL pin voltage will be when UVLO level is exceeded and the output switch turns on..
2. The rate at which the inductor/LED current is ramped up is dependent on the size of the capacitor.

As can been seen in Figure 37 adding a capacitor increases the time taken for the output to reach $90 \%$ of its final value.
There are many factors which set the initial current and ramp rate. Some practical examples are shown below with conditions Vin 12 V L=68uH 2 LEDs at 667 mA ,

| $\mathbf{C}_{\text {DIM }}$ | Initial Current 90\% | Rise Time |
| :---: | :---: | :---: |
| 0 nF | 80 mA | 0.45 ms |
| 10 nF | 80 mA | 0.55 ms |
| 22 nF | 80 mA | 0.8 ms |
| 47 nF | 80 mA | 1.8 ms |
| 100 nF | 80 mA | 4.2 ms |
| 470 nF | 40 mA | 42 ms |

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## Application Information (cont.)

## Input Bulk Capacitor Selection

The small size of ceramic capacitors makes them ideal for AL8807A applications. X5R and X7R types are recommended because they retain their capacitance over wider voltage and temperature ranges than other types such as Z 5 U .
A $2.2 \mu \mathrm{~F}$ input capacitor is sufficient for most intended applications of AL8807A; however a $4.7 \mu \mathrm{~F}$ input capacitor is suggested for input voltages approaching 36 V .

## Diode Selection

For maximum efficiency and performance, the rectifier (D1) should be a fast low capacitance Schottky diode with low reverse leakage at the maximum operating voltage and temperature. The Schottky diode also provides better efficiency than silicon PN diodes, due to a combination of lower forward voltage and reduced recovery time.

It is important to select parts with a peak current rating above the peak coil current and a continuous current rating higher than the maximum output load current. In particular, it is recommended to have a diode voltage rating at least $15 \%$ higher than the operating voltage to ensure safe operation during the switching and a current rating at least $10 \%$ higher than the average diode current. The power rating is verified by calculating the power loss through the diode.

Schottky diodes, e.g. B240 or B140, with their low forward voltage drop and fast reverse recovery, are the ideal choice for AL8807A applications.

## Inductor Selection

Recommended inductor values for the AL8807A are in the range $33 \mu \mathrm{H}$ to $100 \mu \mathrm{H}$.
Higher values of inductance are recommended at higher supply voltages as they result in lower switching frequencies which in turn reduce the errors due to switching delays. Higher values of inductance also result in a smaller change in output current over the supply voltage range. (See graphs).


Figure 38 Inductor Value with Input Voltage and Number of LEDs

The inductor should be mounted as close to the device as possible with low resistance/stray inductance connections to the SW pin.
The chosen coil should have a saturation current higher than the peak output current and a continuous current rating above the required mean output current.
Suitable coils for use with the AL8807A are listed in the table below:

| Part No. | $\begin{gathered} \mathrm{L} \\ (\mu \mathrm{H}) \end{gathered}$ | DCR <br> (V) | ISAT <br> (A) | Manufacturer |
| :---: | :---: | :---: | :---: | :---: |
| MSS1038-333 | 33 | 0.093 | 2.3 | CoilCraft www.coilcraft.com |
| MSS1038-683 | 68 | 0.213 | 1.5 |  |
| NPIS64D330MTRF | 33 | 0.124 | 1.1 | NIC www.niccomp.com |

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## Application Information (cont.)

The inductor value should be chosen to maintain operating duty cycle and switch 'on'/'off' times over the supply voltage and load current range. The following equations can be used as a guide, with reference to Figure 39 - typical switching waveform.

## Switch 'On’ time

$$
\mathrm{toN}_{\mathrm{O}}=\frac{\mathrm{L} \Delta \mathrm{I}}{\mathrm{~V}_{\mathrm{IN}}-\mathrm{V}_{\mathrm{LED}}-\mathrm{I}_{\mathrm{AVG}} \times\left(\mathrm{R}_{\mathrm{S}}+\mathrm{r}_{\mathrm{L}}+\mathrm{RSW}\right)}
$$

## Switch 'Off' time

$$
\mathrm{t}_{\mathrm{OFF}}=\frac{\mathrm{L} \Delta \mathrm{I}}{\mathrm{~V}_{\mathrm{LED}}+\mathrm{V}_{\mathrm{D}}+\mathrm{I}_{\mathrm{AVG}} \times\left(\mathrm{R}_{\mathrm{S}}+\mathrm{r}_{\mathrm{L}}\right)}
$$

Where:
L is the coil inductance ( H )
$r_{L}$ is the coil resistance ( $\Omega$ )
$\mathrm{R}_{\mathrm{s}}$ is the current sense resistance ( $\Omega$ )


Figure 39 Typical Switching Waveform
$l_{\text {avg }}$ is the required LED current (A)
$\Delta I$ is the coil peak-peak ripple current (A)
\{Internally set to $0.3 \times$ lavg\}
$\mathrm{V}_{\text {IN }}$ is the supply voltage $(\mathrm{V})$
$V_{\text {LED }}$ is the total LED forward voltage ( V )
$\mathrm{R}_{\text {SW }}$ is the switch resistance $(\Omega)\{=0.25 \Omega$ nominal (SOT25) $\}$
$V_{D}$ is the diode forward voltage at the required load current $(\mathrm{V})$

## Thermal Considerations

For continuous conduction mode of operation, the absolute maximum junction temperature must not be exceeded. The maximum power dissipation depends on several factors: the thermal resistance of the IC package $\theta_{\mathrm{JA}}$, PCB layout, airflow surrounding the IC, and difference between junction and ambient temperature.
The maximum power dissipation can be calculated using the following formula:

$$
P_{D(M A X)}=\left(T_{J(M A X)}-T_{A}\right) / \theta_{J A}
$$

where
$\mathrm{T}_{\mathrm{J}(\mathrm{MAX})}$ is the maximum operating junction temperature,
$\mathrm{T}_{\mathrm{A}}$ is the ambient temperature,
$\theta_{\mathrm{JA}}$ is the junction to ambient thermal resistance.

The recommended maximum operating junction temperature, $\mathrm{T}_{\mathrm{J}}$, is $+125^{\circ} \mathrm{C}$ and so maximum ambient temperature is determined by the AL8807A's junction to ambient thermal resistance, $\theta_{\mathrm{JA}}$ and device power dissipation.
$\theta_{\mathrm{JA}}$, is layout dependent and package dependent; the AL8807AW5's $\theta_{\mathrm{JA}}$ on a $25 \times 25 \mathrm{~mm}$ single layer PCB with $10 z$ copper standing in still air is approximately $+250^{\circ} \mathrm{C} / \mathrm{W}$ and around $130^{\circ} \mathrm{C} / \mathrm{W}$ on a $51 \mathrm{~mm} \times 51 \mathrm{~mm}$ dual layer board with maximum coverage top and bottom and 3 vias.

The maximum power dissipation at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ can be calculated by the following formulas:


Figure 40 Derating Curve for Different PCB
$\mathrm{P}_{\mathrm{D}(\mathrm{MAX})}=\left(+125^{\circ} \mathrm{C}-+25^{\circ} \mathrm{C}\right) /\left(250^{\circ} \mathrm{C} / \mathrm{W}\right)=0.4 \mathrm{~W}$ for single-layer $25 \mathrm{~mm} \times 25 \mathrm{~mm}$ PCB
$\mathrm{P}_{\mathrm{D}(\mathrm{MAX})}=\left(+125^{\circ} \mathrm{C}-+25^{\circ} \mathrm{C}\right) /\left(130^{\circ} \mathrm{C} / \mathrm{W}\right)=0.77 \mathrm{~W}$ for dual layer $51 \mathrm{~mm} \times 51 \mathrm{~mm}$ PCB

Figure 40, shows the power derating of the AL8807AW5 on two different PCBs and the AL8807AMP on one PCB.

## SOT25-25mm x 25mm: AL8807AW5's $\theta_{\mathrm{JA}}$ on a $25 \times 25 \mathrm{~mm}$ single layer PCB with 10 z copper

SOT25-25mm x 25mm: AL8807AW5's $\theta_{\mathrm{JA}}$ on a $51 \mathrm{~mm} \times 51 \mathrm{~mm}$ dual layer board with maximum coverage top and bottom and 3 vias MSOP-8EP - 51mm x 51mm: AL8807AMP's $\theta_{\mathrm{JA}}$ on a 51mm x 51mm dual layer board with maximum coverage top and bottom and 4 vias

Figure 40 shows that the MSOP-8EP version of the AL8807A can handle more power than its SOT25 version. So the AL8807AMP is the preferred variant when operating at larger supply voltage rails ( $>24 \mathrm{~V}$ ) and/or driving larger LED currents. This is especially true in high power density/space constraint applications such as high power 24VAC MR16 applications.

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## Application Information (cont.)

## EMI and Layout Considerations

The AL8807A is a switching regulator with fast edges and measures small differential voltages; as a result of this care has to be taken with decoupling and layout of the PCB.To help with these effects the AL8807A has been developed to minimise radiated emissions by controlling the switching speeds of the internal power MOSFET.

The rise and fall times are controlled to get the right compromise between power dissipation due to switching losses and radiated EMI. The turnon edge (falling edge) dominates the radiated EMI which is due to an interaction between the Schottky diode (D1), Switching MOSFET and PCB tracks. After the Schottky diode reverse recovery time of around 5 ns has occurred; the falling edge of the SW pin sees a resonant loop between the Schottky diode capacitance and the track inductance, Ltrack, See Figure 41.

The tracks from the SW pin to the Anode of the Schottky diode, D1, and then from D1's cathode to the decoupling capacitors C1 should be as short as possible.

There is an inductance internally in the AL8807A this can be assumed to be around 1 nH . For PCB tracks a figure of 0.5 nH per mm can be used to estimate the primary resonant frequency. If the track is capable of handling 1 A increasing the thickness will have a minor effect on the inductance and length will dominate the size of the inductance.

The resonant frequency of any oscillation is determined by the combined inductance in the track and the effective capacitance of the Schottky diode.


Figure 41 PCB Loop Resonance

An example of good layout is shown in Figure 42 - the stray track inductance should be less than 5 nH .
 nductor as close as possible to minimize ringing

Figure 42 Recommended PCB Layout

Recommendations for minimising radiated EMI and other transients and thermal considerations are:

1. The decoupling capacitor (C1) has to be placed as close as possible to the $\mathrm{V}_{\mathrm{IN}}$ pin and D1 Cathode.
2. The freewheeling diode's (D1) anode, the SW pin and the inductor have to be placed as close as possible to each other to avoid ringing.
3. The Ground return path from C1 must be a low impedance path with the ground plane as large as possible.
4. The LED current sense resistor (R1) has to be placed as close as possible to the $\mathrm{V}_{\mathrm{IN}}$ and SET pins.
5. The majority of the conducted heat from the AL8807A is through the GND pin 2. A maximum earth plane with thermal vias into a second earth plane will minimise self-heating.
6. To reduce emissions via long leads on the supply input and LEDs low RF impedance capacitors (C2 and C5) should be used at the point the wires are joined to the PCB.

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## Application Information (cont.)

## Fault Condition Operation

Open circuit LEDs
The AL8807A has by default open LED protection. If the LEDs should become open circuit the AL8807A will stop oscillating; the SET pin will rise to $\mathrm{V}_{\mathrm{IN}}$ and the SW pin will then fall to GND. No excessive voltages will be seen by the AL8807A.

## LED Chain Shorted Together

If the LED chain should become shorted together (the anode of the top LED becomes shorted to the cathode of the bottom LED) the AL8807A will continue to switch and the current through the AL8807A's internal switch will still be at the expected current - so no excessive heat will be generated within the AL8807A. However, the duty cycle at which it operates will change dramatically and the switching frequency will most likely decrease. See Figure 43 for an example of this behavior at 24 V input voltage driving 3 LEDs.

The on-time of the internal power MOSFET switch is significantly reduced because almost all of the input voltage is now developed across the inductor. The off-time is significantly increased because the reverse voltage across the inductor is now just the Schottky diode voltage (See Figure 43) causing a much slower decay in inductor current.


Figure 43 Switching Characteristics (normal operation to LED chain shorted out)

## High Temperature Operation and Protection

The AL8807A is a high efficiency switching LED driver capable of operating junction temperatures up to $+125^{\circ} \mathrm{C}$. This allows it operate with ambient temperature in excess of $100^{\circ} \mathrm{C}$ given the correct thermal impedance to free air. If a fault should occur that leads to increased ambient temperatures and hence junction temperature then the Over-Temperature Protection (OTP) of the AL8807A will cut in turning the output of the AL8807A off. This will allow the junction temperature of the AL8807A to cool down and potentially giving an opportunity for the fault to clear itself.

The OTP shutdown junction temperature of the AL8807A is approximately $+150^{\circ} \mathrm{C}$ with a hysteresis of $+25^{\circ} \mathrm{C}$. This means that the AL8807A will never switch-off with a junction temperature below $+125^{\circ} \mathrm{C}$ allowing the designer to design the system thermally to fully utilize the wide operating junction temperature of the AL8807A.

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## Ordering Information



| Part Number | Status | Package Code | Packaging | 7" Tape and Reel |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Part Number Suffix |  |
| AL8807AW5-7 | Preview (Note 11) | W5 | SOT25 | 3000/Tape \& Reel | -7 |
| AL8807AMP-13 | New Product | MP | MSOP-8EP | $2500 /$ Tape \& Reel | -13 |

Note: 11. Expected release in $4 Q 2012$.

## Marking Information

(1) SOT25
(Top View)

| 5 |  | 4 |  |
| :---: | :---: | :---: | :---: |
| $\underline{X X} \underline{Y} \underline{W} \underline{X}$ |  |  |  |
|  |  |  | W : Week : A~Z : 1~26 week; <br> a-z : 27~52 week; z represents 52 and 53 week <br> X: A~Z: Internal code |
|  |  |  |  |
| 1 | 2 | 3 |  |


| Part Number | Package | Identification Code |
| :---: | :---: | :---: |
| AL8807AW5-7 | SOT25 | C6 |

(2) MSOP-8EP


| Part Number | Package |
| :---: | :---: |
| AL8807AMP-13 | MSOP-8EP |

Package Outline Dimensions (All dimensions in mm.)
Please see AP02002 at http://www.diodes.com/datasheets/ap02002.pdf for latest version.
(1) SOT25


| SOT25 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Dim | Min | Max | Typ |  |
| A | 0.35 | 0.50 | 0.38 |  |
| B | 1.50 | 1.70 | 1.60 |  |
| C | 2.70 | 3.00 | 2.80 |  |
| D | - | - | 0.95 |  |
| H | 2.90 | 3.10 | 3.00 |  |
| J | 0.013 | 0.10 | 0.05 |  |
| K | 1.00 | 1.30 | 1.10 |  |
| L | 0.35 | 0.55 | 0.40 |  |
| M | 0.10 | 0.20 | 0.15 |  |
| $\mathbf{N}$ | 0.70 | 0.80 | 0.75 |  |
| $\mathbf{\alpha}$ | $0^{\circ}$ | $8^{\circ}$ | - |  |
| All Dimensions in | $\mathbf{~ m m}$ |  |  |  |
|  |  |  |  |  |

(2) MSOP-8EP


## Suggested Pad Layout

Please see AP02001 at http://www.diodes.com/datasheets/ap02001.pdf for latest version.
(1) SOT25


| Dimensions | Value (in mm) |
| :---: | :---: |
| $\mathbf{Z}$ | 3.20 |
| $\mathbf{G}$ | 1.60 |
| $\mathbf{X}$ | 0.55 |
| $\mathbf{Y}$ | 0.80 |
| $\mathbf{C 1}$ | 2.40 |
| $\mathbf{C 2}$ | 0.95 |

(2) MSOP-8EP


| Dimensions | Value <br> (in mm) |
| :---: | :---: |
| $\mathbf{C}$ | 0.650 |
| $\mathbf{G}$ | 0.450 |
| $\mathbf{X}$ | 0.450 |
| $\mathbf{X 1}$ | 2.000 |
| $\mathbf{Y}$ | 1.350 |
| Y1 | 1.700 |
| Y2 | 5.300 |

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