

## FEATURES

- **Very Wide, Over-the-Top<sup>®</sup>, Input Common Mode Range**
  - Extends 44V Above  $V^-$  (Independent of  $V^+$ )
  - Extends  $-0.3V$  Below  $V^-$
- **Wide Power Supply Range: 2.85V to 36V**
- **Input Offset Voltage: 300 $\mu$ V Maximum**
- **Gain Accuracy: 1% Max**
- Gain Configurable with External Resistors
- Operating Current: 150 $\mu$ A
- Slew Rate: 2V/ $\mu$ s
- Sense Input Current When Powered Down: 1nA
- Full-Scale Output Current: 1mA Minimum
- Operating Temperature Range  $-40^{\circ}C$  to  $125^{\circ}C$
- Available in 2mm  $\times$  3mm DFN and 8-Lead MSOP Packages

## APPLICATIONS

- High Side or Low Side Current Sensing
- Current Monitoring on Positive or Negative Supply Voltages
- Battery Monitoring
- Fuse/MOSFET Monitoring
- Automotive
- Power Management
- Portable Test/Measurement Systems

## DESCRIPTION

The LT<sup>®</sup>6105 is a micropower, precision current sense amplifier with a very wide input common mode range. The LT6105 monitors unidirectional current via the voltage across an external sense resistor. The input common mode range extends from  $-0.3V$  to  $44V$ , with respect to the negative supply voltage ( $V^-$ ). This allows the LT6105 to operate as a high side current sense monitor or a low side current sense monitor. It also allows the LT6105 to monitor current on a negative supply voltage, as well as continuously monitor a battery from full charge to depletion. The inputs of LT6105 can withstand differential voltages up to  $\pm 44V$ , which makes it ideal for monitoring a fuse or MOSFET switch.

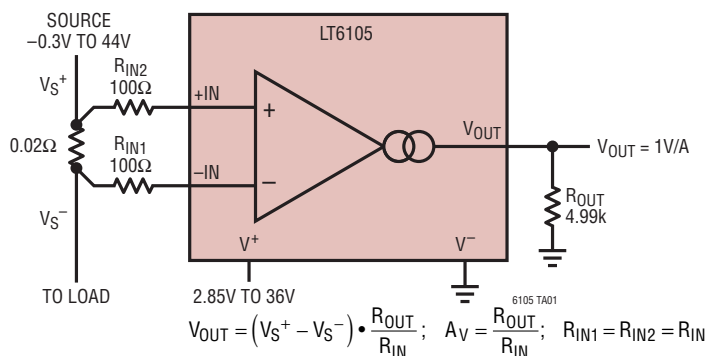
Gain is configured with external resistors from 1V/V to 100V/V. The input common mode rejection and power supply rejection are in excess of 100dB and the input offset voltage is less than 300 $\mu$ V. A typical slew rate of 2V/ $\mu$ s ensures fast response to unexpected current changes.

The LT6105 can operate from an independent power supply of 2.85V to 36V and draws only 150 $\mu$ A. When  $V^+$  is powered down, the sense pins are biased off. This prevents loading of the monitored circuit, irrespective of the sense voltage. The LT6105 is available in a 6-lead DFN and 8-lead MSOP package.

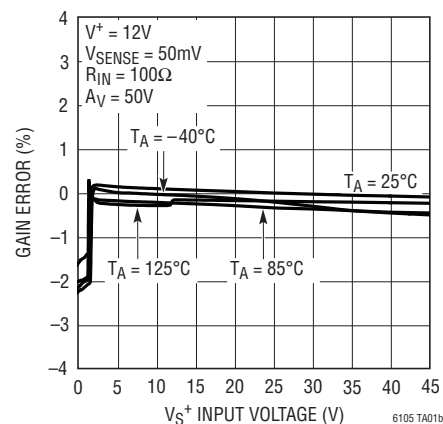
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## TYPICAL APPLICATION

Gain of 50 Current Sense Amplifier



Gain Error vs Input Voltage



# LT6105

## ABSOLUTE MAXIMUM RATINGS

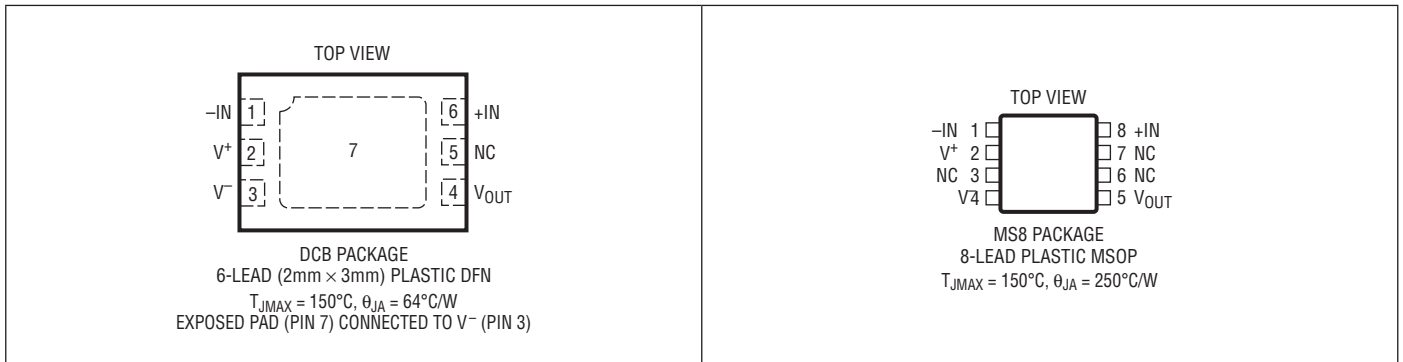
(Notes 1, 2)

Differential Input Voltage (+IN – –IN)	±44V
Input Voltage V(+IN, –IN) to V <sup>-</sup>	–9.5V to 44V
Total V <sup>+</sup> Supply Voltage from V <sup>-</sup>	36V
Output Voltage	V <sup>-</sup> to (V <sup>-</sup> + 36V)
Output Short-Circuit Duration (Note 3)	Indefinite
Operating Temperature Range (Note 4)	
LT6105C	–40°C to 85°C
LT6105I	–40°C to 85°C
LT6105H	–40°C to 125°C

Specified Temperature Range (Note 5)

LT6105C	0°C to 70°C
LT6105I	–40°C to 85°C
LT6105H	–40°C to 125°C
Maximum Junction Temperature	150°C
Storage Temperature Range	–65°C to 150°C
Lead Temperature (Soldering, 10 sec)	
MSOP	300°C

## PIN CONFIGURATION



## ORDER INFORMATION

LEAD FREE FINISH	TAPE AND REEL	PART MARKING*	PACKAGE DESCRIPTION	SPECIFIED TEMPERATURE RANGE
LT6105CDCB#TRMPBF	LT6105CDCB#TRPBF	LCTF	6-Lead (2mm × 3mm) Plastic DFN	0°C to 70°C
LT6105IDCB#TRMPBF	LT6105IDCB#TRPBF	LCTF	6-Lead (2mm × 3mm) Plastic DFN	–40°C to 85°C
LT6105HDCB#TRMPBF	LT6105HDCB#TRPBF	LCTF	6-Lead (2mm × 3mm) Plastic DFN	–40°C to 125°C
LT6105CMS8#PBF	LT6105CMS8#TRPBF	LTCTD	8-Lead Plastic MS8	0°C to 70°C
LT6105IMS8#PBF	LT6105IMS8#TRPBF	LTCTD	8-Lead Plastic MS8	–40°C to 85°C
LT6105HMS8#PBF	LT6105HMS8#TRPBF	LTCTD	8-Lead Plastic MS8	–40°C to 125°C

TRM = 500 pieces. \*Temperature grades are identified by a label on the shipping container.

Consult LTC Marketing for parts specified with wider operating temperature ranges.

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For more information on lead free part marking, go to: <http://www.linear.com/leadfree/>

For more information on tape and reel specifications, go to: <http://www.linear.com/tapeandree/>

**ELECTRICAL CHARACTERISTICS** The ● denotes the specifications which apply over the temperature range  $0^{\circ}\text{C} < T_A < 70^{\circ}\text{C}$  (LT6105C), otherwise specifications are at  $T_A = 25^{\circ}\text{C}$ .  $V^+ = 12\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{S^+} = 12\text{V}$  (see Figure 1),  $R_{IN1} = R_{IN2} = 100\Omega$ ,  $R_{OUT} = 5\text{k}$  ( $A_V = 50$ ),  $V_{SENSE} = V_{S^+} - V_{S^-}$ , unless otherwise specified. (Note 5)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS	
$V_{S^+}, V_{S^-}$	Input Voltage Range	Guaranteed by CMRR	●	-0.3	44	V	
				-0.1	44	V	
$A_V$ Error	Voltage Gain Error (Note 6)	$V_{SENSE} = 25\text{mV}$ to $75\text{mV}$ , $V_{S^+} = 12\text{V}$	●	-1	0.1	1	%
				-1.3	1.3	%	
		$V_{SENSE} = 25\text{mV}$ to $75\text{mV}$ , $V_{S^+} = 0\text{V}$	●	-2.5	2.5	%	
$V_{OS}$	Input Offset Voltage MS8 Package	$V_{SENSE} = 5\text{mV}$	●	-0.3	-0.1	0.3	mV
	Input Offset Voltage DCB Package	$V_{SENSE} = 5\text{mV}$	●	-0.4	-0.1	0.4	mV
	Input Offset Voltage	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 0\text{V}$	●	-0.7	0.7	mV	
			●	-1	-0.3	1	mV
			●	-1.3	1.3	mV	
$\Delta V_{OS}/\Delta T$	Temperature Coefficient of $V_{OS}$		●	0.5		$\mu\text{V}/^{\circ}\text{C}$	
CMRR	Input Common Mode Rejection Ratio	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 2.8\text{V}$ to $44\text{V}$	●	100	120	dB	
			●	95	dB		
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = -0.3\text{V}$ to $44\text{V}$	●	94	dB		
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = -0.1\text{V}$ to $44\text{V}$	●	90	dB		
$V^+$	Power Supply Voltage Range	Guaranteed by PSRR	●	2.85	36	V	
PSRR	Power Supply Rejection Ratio	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 12\text{V}$ , $V^+ = 2.85\text{V}$ to $36\text{V}$	●	98	120	dB	
			●	94	dB		
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 0\text{V}$ , $V^+ = 2.85\text{V}$ to $36\text{V}$	●	98	120	dB	
			●	94	dB		
$I_{(+IN)}, I_{(-IN)}$	Input Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$	●		15	25	$\mu\text{A}$
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 0\text{V}$	●		-0.05	$\mu\text{A}$	
$I_{(+IN)} - I_{(-IN)}$	Input Offset Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$	●		0.05	0.5	$\mu\text{A}$
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 0\text{V}$	●		0.005	$\mu\text{A}$	
$I_{(+IN)} + I_{(-IN)}$	Input Current (Power-Down)	$V^+ = 0\text{V}$ , $V_{S^+} = 44\text{V}$ , $V_{SENSE} = 0\text{V}$	●		0.03	1	$\mu\text{A}$
$I_S$	$V^+$ Supply Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$ , $V^+ = 2.85\text{V}$	●		200	300	$\mu\text{A}$
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$ , $V^+ = 36\text{V}$	●		240	350	$\mu\text{A}$
$V_{O(MIN)}$	Minimum Output Voltage	$V_{SENSE} = 0\text{mV}$ , $V_{S^+} = 44\text{V}$ , $V^+ = 36\text{V}$	●		35	mV	
$V_{O(MAX)}$	Output High (Referred to $V^+$ )	$V_{SENSE} = 120\text{mV}$ , $A_V = 100$ , $R_{OUT} = 10\text{k}$	●		1.25	1.5	V
$I_{OUT}$	Maximum Output Current	Guaranteed by $V_{O(MAX)}$	●	1		mA	
$I_{SC}$	Short-Circuit Output Current	$V_{S^+} = 44\text{V}$ , $V_{S^-} = 0\text{V}$ , $R_{OUT} = 0\Omega$	●	1.5		mA	
BW	-3dB Bandwidth	$V_{SENSE} = 50\text{mV}$ , $A_V = 10\text{V/V}$		100		kHz	
$t_S$	Output Settling to 1% of Final Value	$V_{SENSE} = 5\text{mV}$ to $100\text{mV}$		5		$\mu\text{s}$	
$t_r$	Input Step Response (Note 7)	$V_{SENSE} = 5\text{mV}$ to $100\text{mV}$		3		$\mu\text{s}$	
SR	Slew Rate (Note 8)	$V_{SENSE} = 5\text{mV}$ to $150\text{mV}$ , $A_V = 50\text{V/V}$ , $R_{IN} = 400\Omega$		1.75	2	$\text{V}/\mu\text{s}$	
$V_{REV}$	Reverse Input Voltage (Referred to $V^-$ )	$I_{(+IN)} + I_{(-IN)} = -5\text{mA}$	●	-9.5	-12	V	

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the temperature range  $-40^{\circ}\text{C} < T_A < 85^{\circ}\text{C}$  (LT6105I), otherwise specifications are at  $T_A = 25^{\circ}\text{C}$ .  $V^+ = 12\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{S^+} = 12\text{V}$  (see Figure 1),  $R_{IN1} = R_{IN2} = 100\Omega$ ,  $R_{OUT} = 5\text{k}$  ( $A_V = 50$ ),  $V_{SENSE} = V_{S^+} - V_{S^-}$ , unless otherwise specified. (Note 5)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS	
$V_{S^+}, V_{S^-}$	Input Voltage Range	Guaranteed by CMRR	●	-0.3	44	V	
				-0.3	44	V	
$A_V$ Error	Voltage Gain Error (Note 6)	$V_{SENSE} = 25\text{mV}$ to $75\text{mV}$ , $V_{S^+} = 12\text{V}$	●	-1	0.1	1	%
				-1.4	1.4	%	
		$V_{SENSE} = 25\text{mV}$ to $75\text{mV}$ , $V_{S^+} = 0\text{V}$	●	-3	3	%	
$V_{OS}$	Input Offset Voltage MS8 Package	$V_{SENSE} = 5\text{mV}$	●	-0.3	-0.1	0.3	mV
	Input Offset Voltage DCB Package	$V_{SENSE} = 5\text{mV}$	●	-0.65	0.65	mV	
	Input Offset Voltage	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 0\text{V}$	●	-0.4	-0.1	0.4	mV
			●	-0.75	0.75	mV	
			●	-1	-0.3	1	mV
			●	-1.4	1.4	mV	
$\Delta V_{OS}/\Delta T$	Temperature Coefficient of $V_{OS}$		●	0.5		$\mu\text{V}/^{\circ}\text{C}$	
CMRR	Input Common Mode Rejection Ratio	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 2.8\text{V}$ to $44\text{V}$	●	100	120	dB	
			●	95	dB		
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = -0.3\text{V}$ to $44\text{V}$ $V_{SENSE} = 5\text{mV}$ , $V_{S^+} = -0.1\text{V}$ to $44\text{V}$	●	94	90	dB	
		●	90	dB			
$V^+$	Power Supply Voltage Range	Guaranteed by PSRR	●	2.85	36	V	
PSRR	Power Supply Rejection Ratio	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 12\text{V}$ , $V^+ = 2.85\text{V}$ to $36\text{V}$	●	98	120	dB	
			●	94	dB		
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 0\text{V}$ , $V^+ = 2.85\text{V}$ to $36\text{V}$	●	98	120	dB	
		●	94	dB			
$I_{(+IN)}, I_{(-IN)}$	Input Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$	●		16	$\mu\text{A}$	
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 0\text{V}$	●		-0.05	$\mu\text{A}$	
$I_{(+IN)} - I_{(-IN)}$	Input Offset Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$	●		0.08	$\mu\text{A}$	
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 0\text{V}$	●		0.01	$\mu\text{A}$	
$I_{(+IN)} + I_{(-IN)}$	Input Current (Power-Down)	$V^+ = 0\text{V}$ , $V_{S^+} = 44\text{V}$ , $V_{SENSE} = 0\text{V}$	●		0.035	$\mu\text{A}$	
$I_S$	$V^+$ Supply Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$ , $V^+ = 2.85\text{V}$	●		200	$\mu\text{A}$	
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$ , $V^+ = 36\text{V}$	●		250	$\mu\text{A}$	
$V_{O(MIN)}$	Minimum Output Voltage	$V_{SENSE} = 0\text{mV}$ , $V_{S^+} = 44\text{V}$ , $V^+ = 36\text{V}$	●		40	mV	
$V_{O(MAX)}$	Output High (Referred to $V^+$ )	$V_{SENSE} = 120\text{mV}$ , $A_V = 100$ , $R_{OUT} = 10\text{k}$	●		1.27	V	
$I_{OUT}$	Maximum Output Current	Guaranteed by $V_{O(MAX)}$	●	1		mA	
$I_{SC}$	Short-Circuit Output Current	$V_{S^+} = 44\text{V}$ , $V_{S^-} = 0\text{V}$ , $R_{OUT} = 0\Omega$	●	1.5		mA	
BW	-3dB Bandwidth	$V_{SENSE} = 50\text{mV}$ , $A_V = 10\text{V}/\text{V}$		100		kHz	
$t_S$	Output Settling to 1% of Final Value	$V_{SENSE} = 5\text{mV}$ to $100\text{mV}$		5		$\mu\text{s}$	
$t_r$	Input Step Response (Note 7)	$V_{SENSE} = 5\text{mV}$ to $100\text{mV}$		3		$\mu\text{s}$	
SR	Slew Rate (Note 8)	$V_{SENSE} = 5\text{mV}$ to $150\text{mV}$ , $A_V = 50\text{V}/\text{V}$ , $R_{IN} = 400\Omega$		1.75	2	$\text{V}/\mu\text{s}$	
$V_{REV}$	Reverse Input Voltage (Referred to $V^-$ )	$I_{(+IN)} + I_{(-IN)} = -5\text{mA}$	●	-9.5	-12	V	

**ELECTRICAL CHARACTERISTICS** The ● denotes the specifications which apply over the temperature range  $-40^{\circ}\text{C} < T_A < 125^{\circ}\text{C}$  (LT6105H), otherwise specifications are at  $T_A = 25^{\circ}\text{C}$ .  $V^+ = 12\text{V}$ ,  $V^- = 0\text{V}$ ,  $V_{S^+} = 12\text{V}$  (see Figure 1),  $R_{IN1} = R_{IN2} = 100\Omega$ ,  $R_{OUT} = 5\text{k}$  ( $A_V = 50$ ),  $V_{SENSE} = V_{S^+} - V_{S^-}$ , unless otherwise specified. (Note 5)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS	
$V_{S^+}, V_{S^-}$	Input Voltage Range	Guaranteed by CMRR	●	-0.3	44	V	
			●	-0.1	44	V	
$A_V$ Error	Voltage Gain Error (Note 6)	$V_{SENSE} = 25\text{mV}$ to $75\text{mV}$ , $V_{S^+} = 12\text{V}$	●	-1	0.1	1	%
		$V_{SENSE} = 25\text{mV}$ to $75\text{mV}$ , $V_{S^+} = 0\text{V}$	●	-1.5		1.5	%
$V_{OS}$	Input Offset Voltage MS8 Package	$V_{SENSE} = 5\text{mV}$	●	-0.3	-0.1	0.3	mV
	Input Offset Voltage DCB Package	$V_{SENSE} = 5\text{mV}$	●	-0.8		0.8	mV
	Input Offset Voltage	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 0\text{V}$	●	-0.4	-0.1	0.4	mV
			●	-0.9		0.9	mV
			●	-1	-0.3	1	mV
			●	-1.6		1.6	mV
$\Delta V_{OS}/\Delta T$	Temperature Coefficient of $V_{OS}$		●	0.5		$\mu\text{V}/^{\circ}\text{C}$	
CMRR	Input Common Mode Rejection Ratio	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 2.8\text{V}$ to $44\text{V}$	●	100	120	dB	
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = -0.3\text{V}$ to $44\text{V}$ $V_{SENSE} = 5\text{mV}$ , $V_{S^+} = -0.1\text{V}$ to $44\text{V}$	●	95		dB	
			●	94		dB	
			●	80		dB	
$V^+$	Power Supply Voltage Range	Guaranteed by PSRR	●	2.85	36	V	
PSRR	Power Supply Rejection Ratio	$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 12\text{V}$ , $V^+ = 2.85\text{V}$ to $36\text{V}$	●	98	120	dB	
		$V_{SENSE} = 5\text{mV}$ , $V_{S^+} = 0\text{V}$ , $V^+ = 2.85\text{V}$ to $36\text{V}$	●	94		dB	
			●	98	120	dB	
			●	94		dB	
$I_{(+IN)}, I_{(-IN)}$	Input Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$	●		18	$\mu\text{A}$	
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 0\text{V}$	●		-0.05	$\mu\text{A}$	
$I_{(+IN)} - I_{(-IN)}$	Input Offset Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$	●	0.35	0.8	$\mu\text{A}$	
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 0\text{V}$	●	0.1		$\mu\text{A}$	
$I_{(+IN)} + I_{(-IN)}$	Input Current (Power-Down)	$V^+ = 0\text{V}$ , $V_{S^+} = 44\text{V}$ , $V_{SENSE} = 0\text{V}$	●	0.5	2.5	$\mu\text{A}$	
$I_S$	$V^+$ Supply Current	$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$ , $V^+ = 2.85\text{V}$	●	240	350	$\mu\text{A}$	
		$V_{SENSE} = 0\text{V}$ , $V_{S^+} = 3\text{V}$ , $V^+ = 36\text{V}$	●	300	450	$\mu\text{A}$	
$V_{O(MIN)}$	Minimum Output Voltage	$V_{SENSE} = 0\text{mV}$ , $V_{S^+} = 44\text{V}$ , $V^+ = 36\text{V}$	●		45	mV	
$V_{O(MAX)}$	Output High (Referred to $V^+$ )	$V_{SENSE} = 120\text{mV}$ , $A_V = 100$ , $R_{OUT} = 10\text{k}$	●	1.3	1.7	V	
$I_{OUT}$	Maximum Output Current	Guaranteed by $V_{O(MAX)}$	●	1		mA	
$I_{SC}$	Short-Circuit Output Current	$V_{S^+} = 44\text{V}$ , $V_{S^-} = 0\text{V}$ , $R_{OUT} = 0\Omega$	●	1.5		mA	
BW	-3dB Bandwidth	$V_{SENSE} = 50\text{mV}$ , $A_V = 10\text{V}/\text{V}$		100		kHz	
$t_S$	Output Settling to 1% of Final Value	$V_{SENSE} = 5\text{mV}$ to $100\text{mV}$		5		$\mu\text{s}$	
$t_r$	Input Step Response (Note 7)	$V_{SENSE} = 5\text{mV}$ to $100\text{mV}$		3		$\mu\text{s}$	
SR	Slew Rate (Note 8)	$V_{SENSE} = 5\text{mV}$ to $150\text{mV}$ , $A_V = 50\text{V}/\text{V}$ , $R_{IN} = 400\Omega$		1.75	2	$\text{V}/\mu\text{s}$	
$V_{REV}$	Reverse Input Voltage (Referred to $V^-$ )	$I_{(+IN)} + I_{(-IN)} = -5\text{mA}$	●	-9.5	-12	V	

## ELECTRICAL CHARACTERISTICS

**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** ESD (Electrostatic Discharge) sensitive devices. Extensive use of ESD protection devices are used internal to the LT6105, however, high electrostatic discharge can damage or degrade the device. Use proper ESD handling precautions.

**Note 3:** A heat sink may be required to keep the junction temperature below absolute maximum ratings.

**Note 4:** The LT6105C/LT6105I are guaranteed functional over the operating temperature range of  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ . The LT6105H is

guaranteed functional over the operating temperature range of  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ .

**Note 5:** The LT6105C is guaranteed to meet specified performance from  $0^{\circ}\text{C}$  to  $70^{\circ}\text{C}$ . The LT6105C is designed, characterized and expected to meet specified performance from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$  but is not tested or QA sampled at these temperatures. The LT6105I is guaranteed to meet specified performance from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ . The LT6105H is guaranteed to meet specified performance from  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ .

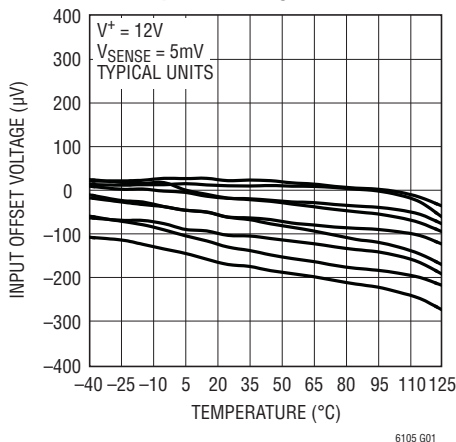
**Note 6:** 0.01% tolerance external resistors are used.

**Note 7:**  $t_r$  is measured from the input to the 2.5V point on the 5V output.

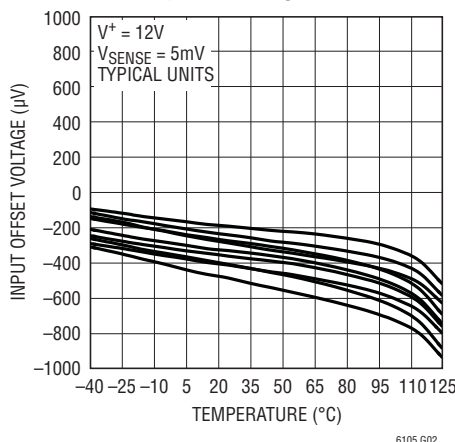
**Note 8:** Slew rate is measured on the output between 1V and 5V.

## TYPICAL PERFORMANCE CHARACTERISTICS

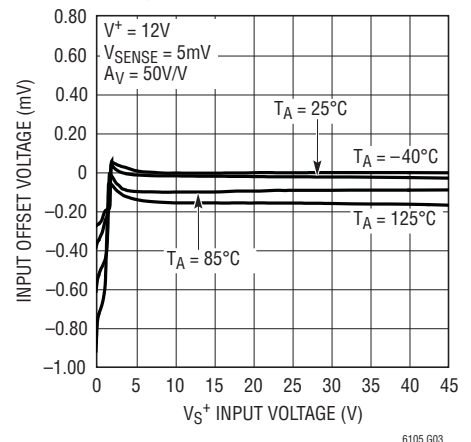
**Input Offset Voltage vs Temperature,  $V_S^+ = 12\text{V}$**



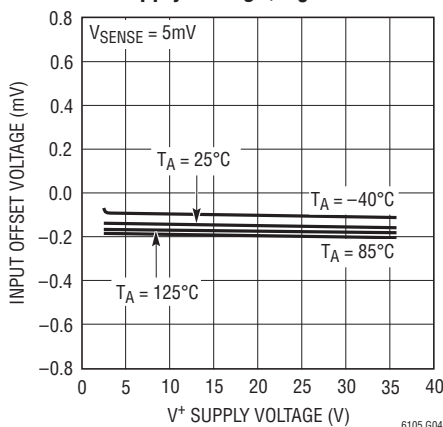
**Input Offset Voltage vs Temperature,  $V_S^+ = 0\text{V}$**



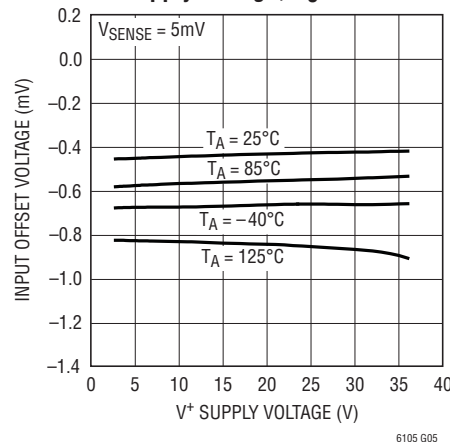
**Input Offset Voltage vs Input Voltage**



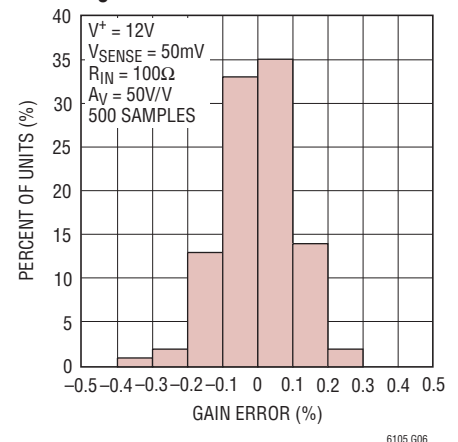
**Input Offset Voltage vs Supply Voltage,  $V_S^+ = 12\text{V}$**



**Input Offset Voltage vs Supply Voltage,  $V_S^+ = 0\text{V}$**

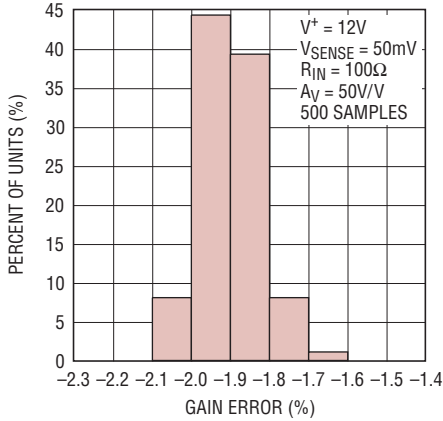


**Gain Error Distribution,  $V_S^+ = 12\text{V}$**



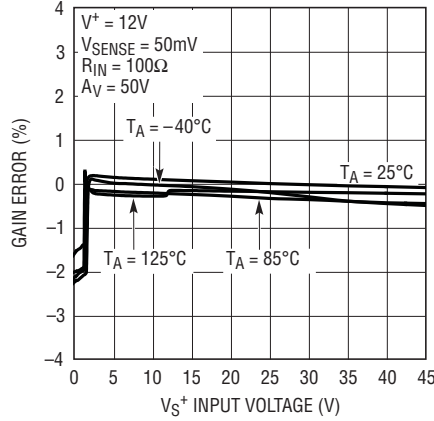
# TYPICAL PERFORMANCE CHARACTERISTICS

**Gain Error Distribution,  $V_S^+ = 0V$**



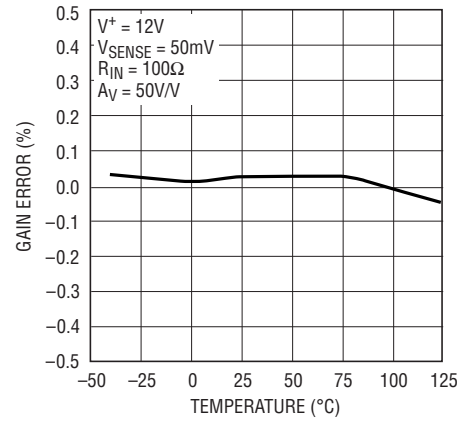
6105 G07

**Gain Error vs Input Voltage**



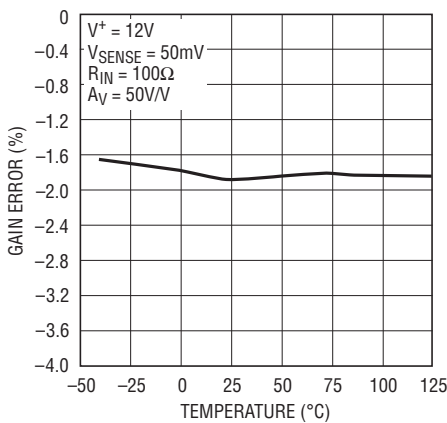
6105 G08

**Gain Error vs Temperature,  $V_S^+ = 12V$**



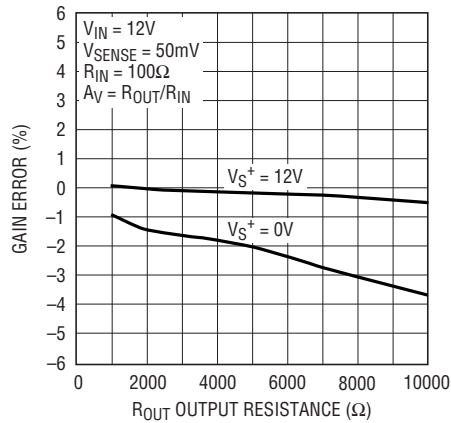
6105 G09

**Gain Error vs Temperature,  $V_S^+ = 0V$**



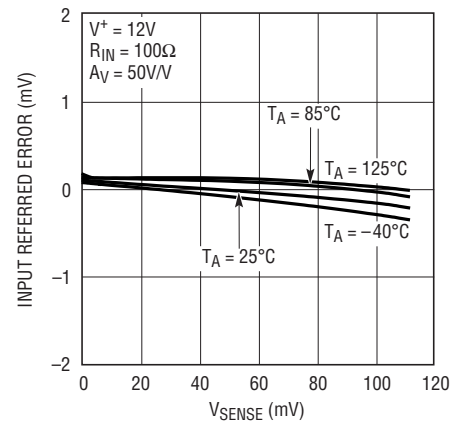
6105 G10

**Gain Error vs Output Resistance**



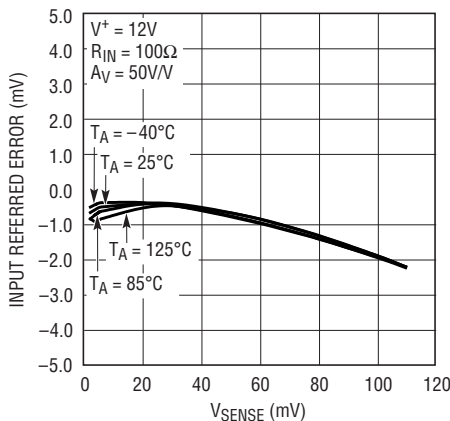
6105 G11

**Input Referred Voltage Error vs  $V_{SENSE}$ ,  $V_S^+ = 12V$**



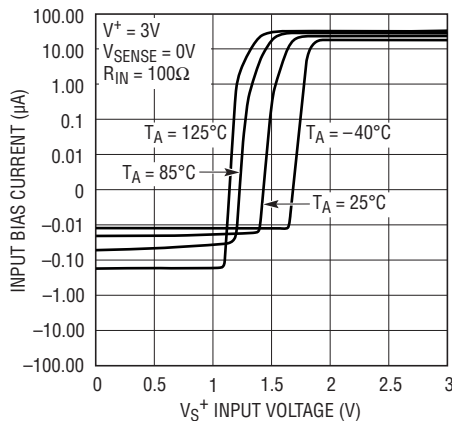
6105 G12

**Input Referred Voltage Error vs  $V_{SENSE}$ ,  $V_S^+ = 0V$**



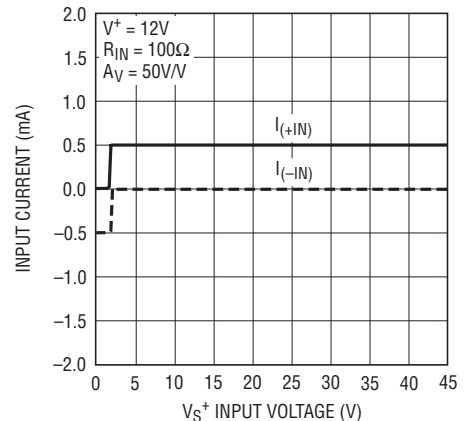
6105 G13

**Input Bias Current vs Input Voltage**



6105 G14

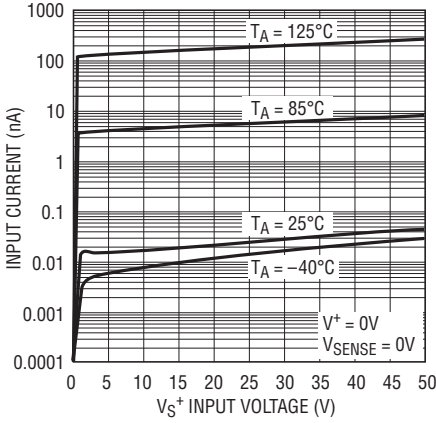
**Input Current vs Input Voltage,  $V_{SENSE} = 50mV$**



6105 G15

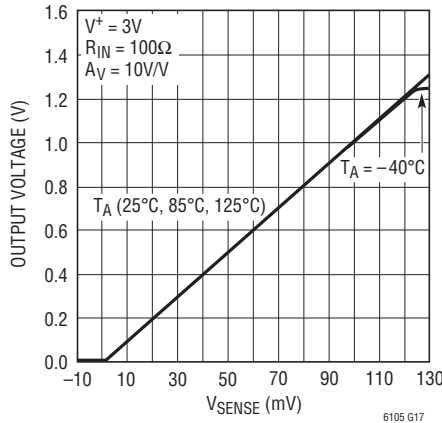
TYPICAL PERFORMANCE CHARACTERISTICS

Input Current ( $V^+$  Powered Down) vs Input Voltage



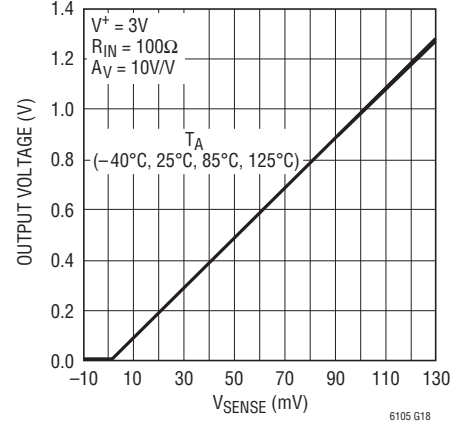
6105 G16

Output Voltage vs  $V_{SENSE}$  Voltage,  $V_{S^+} = 12V$



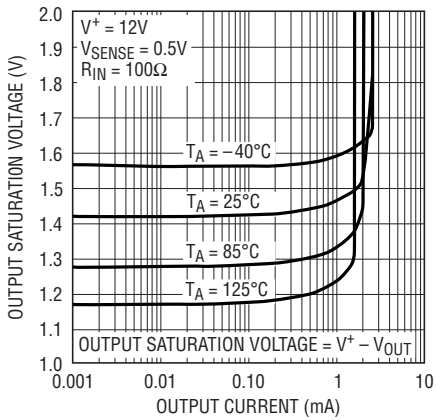
6105 G17

Output Voltage vs  $V_{SENSE}$  Voltage,  $V_{S^+} = 0V$



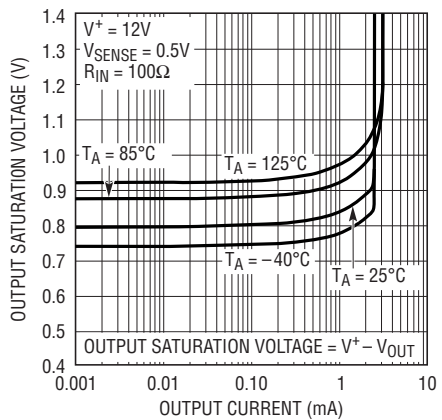
6105 G18

Output Saturation Voltage vs Output Current,  $V_{S^+} = 12V$



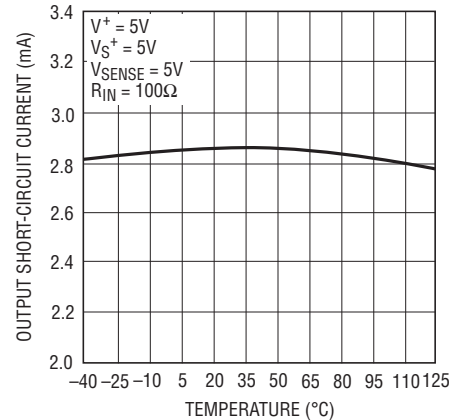
6105 G19

Output Saturation Voltage vs Output Current,  $V_{S^+} = 0.5V$



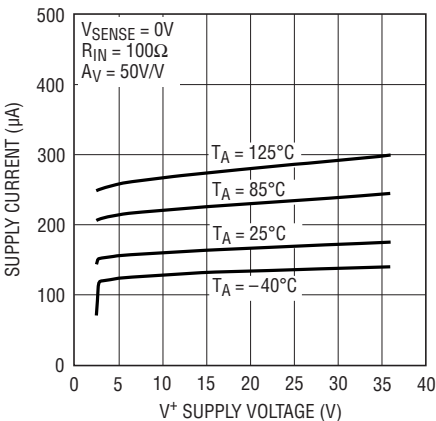
6105 G20

Output Short-Circuit Current vs Temperature



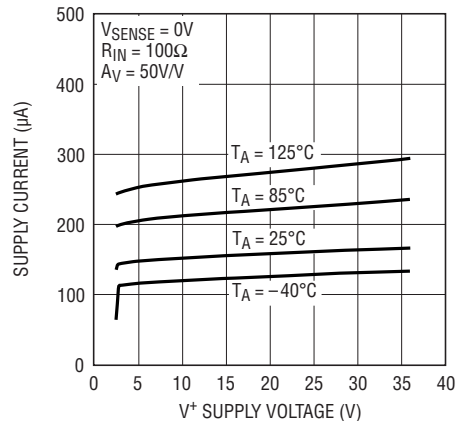
6105 G21

Supply Current vs Supply Voltage,  $V_{S^+} = 12V$



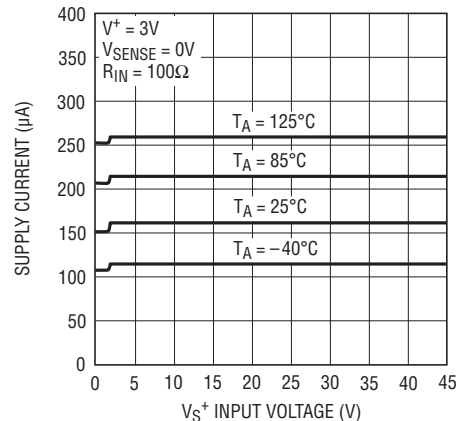
6105 G22

Supply Current vs Supply Voltage,  $V_{S^+} = 0V$



6105 G23

Supply Current vs Input Voltage

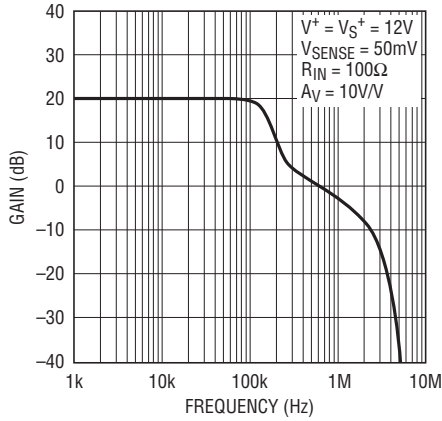


6105 G24



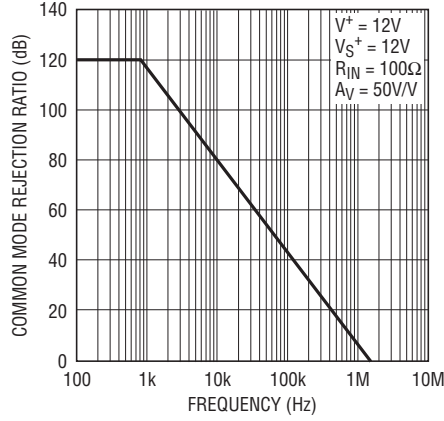
# TYPICAL PERFORMANCE CHARACTERISTICS

**Gain vs Frequency**



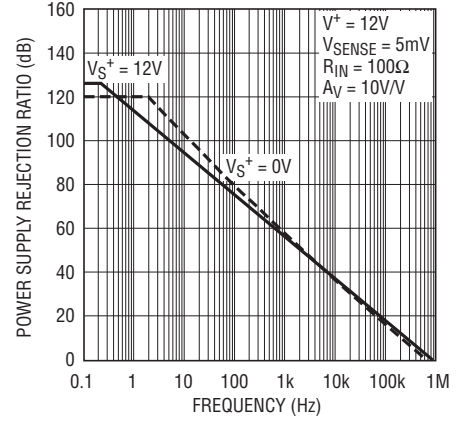
6105 G25

**Common Mode Rejection Ratio vs Frequency**



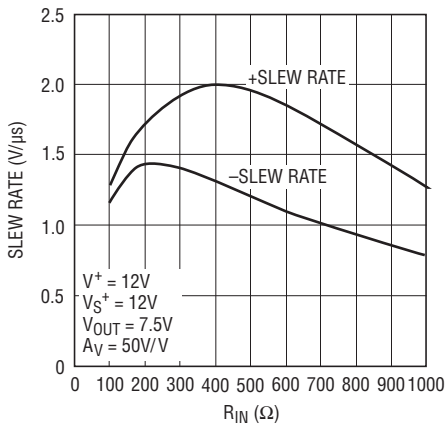
6105 G26

**Power Supply Rejection Ratio vs Frequency**



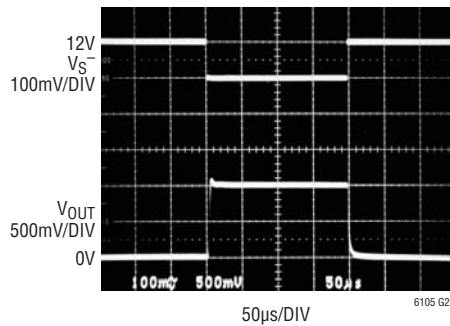
6105 G27

**Slew Rate vs  $R_{IN}$**



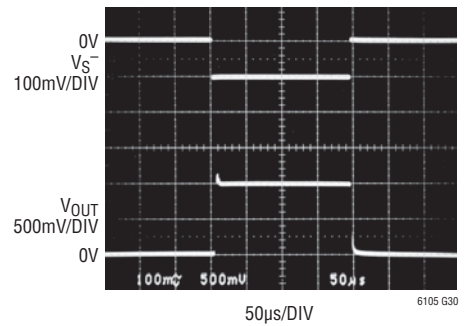
6105 G28

**Step Response**  
 $V_{SENSE} = 0V$  to  $100mV$ ,  $V_S^+ = 12V$



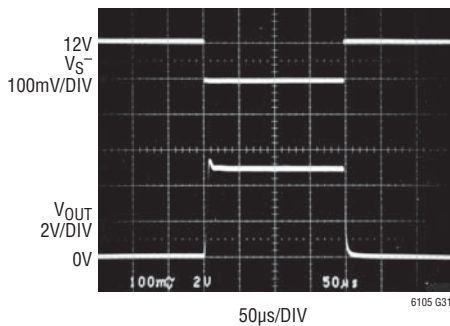
6105 G29

**Step Response**  
 $V_{SENSE} = 0V$  to  $100mV$ ,  $V_S^+ = 0V$



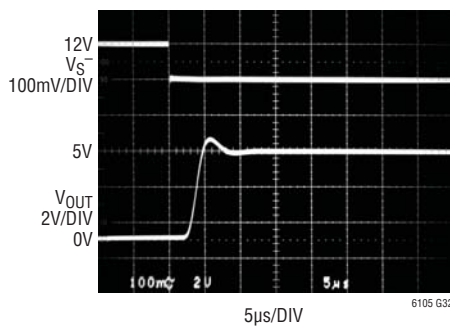
6105 G30

**Step Response**  
 $V_{SENSE} = 0V$  to  $100mV$ ,  $R_{IN} = 100\Omega$



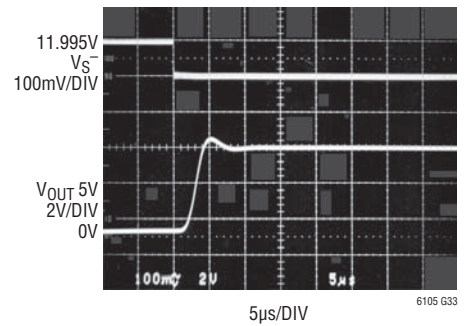
6105 G31

**Step Response**  
 $V_{SENSE} = 0V$  to  $100mV$



6105 G32

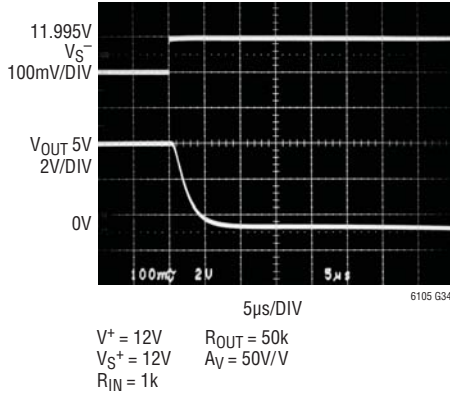
**Step Response**  
 $V_{SENSE} = 5mV$  to  $100mV$



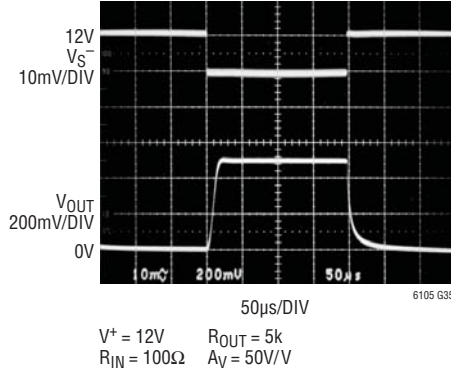
6105 G33

TYPICAL PERFORMANCE CHARACTERISTICS

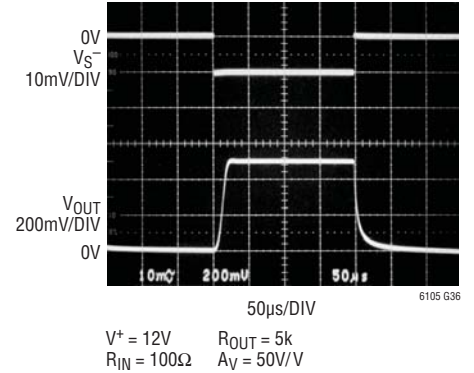
Step Response  
 $V_{SENSE} = 100mV \text{ to } 5mV$



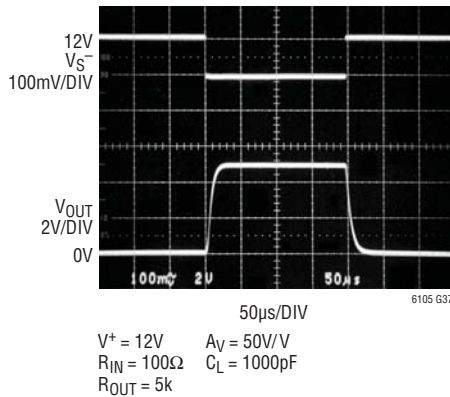
Step Response  
 $V_{SENSE} = 0V \text{ to } 10mV, V_{S^+} = 12V$



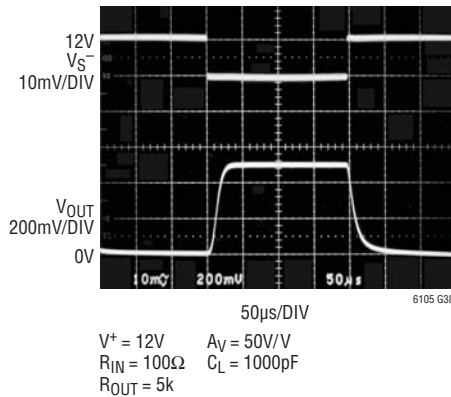
Step Response  
 $V_{SENSE} = 0V \text{ to } 10mV, V_{S^+} = 0V$



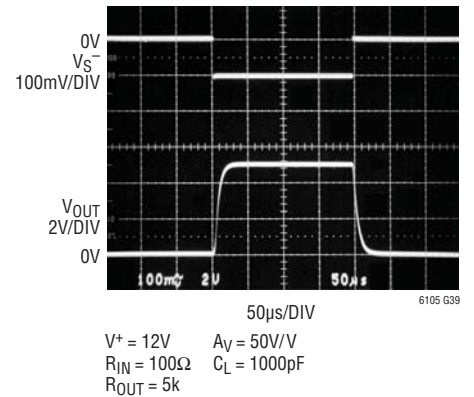
Step Response  
 $V_{SENSE} = 0V \text{ to } 100mV,$   
 $C_L = 1000pF, V_{S^+} = 12V$



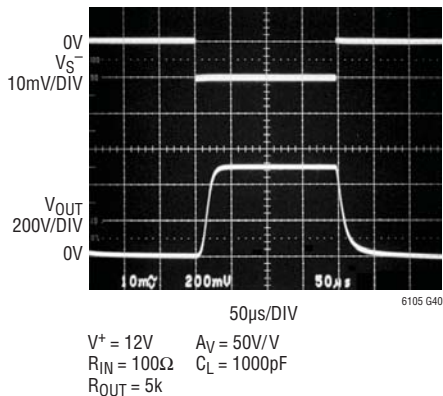
Step Response  
 $V_{SENSE} = 0V \text{ to } 10mV,$   
 $C_L = 1000pF, V_{S^+} = 12V$



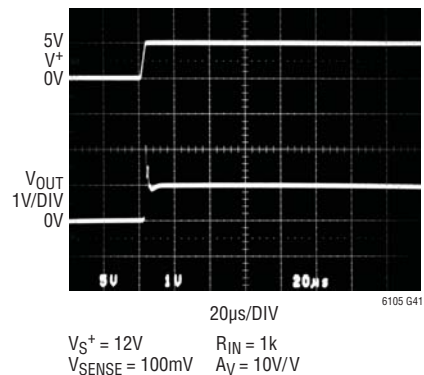
Step Response  
 $V_{SENSE} = 0V \text{ to } 100mV,$   
 $C_L = 1000pF, V_{S^+} = 0V$



Step Response  
 $V_{SENSE} = 0V \text{ to } 10mV,$   
 $C_L = 1000pF, V_{S^+} = 0V$



Power Supply Start-Up Response



## PIN FUNCTIONS (DCB/MS8)

**-IN (Pin 1/Pin 1):** Negative Sense Input Terminal. Negative sense voltage input will remain functional for voltages up to 44V, referred to  $V^-$ . Connect  $-IN$  to an external gain-setting resistor  $R_{IN1}$  ( $R_{IN1} = R_{IN2}$ ) to set the gain.

**$V^+$  (Pin 2/Pin 2):** Power Supply Voltage. This pin supplies current to the amplifier and can operate from 2.85V to 36V, independent of the voltages on the  $-IN$  or  $+IN$  pins.

**$V^-$  (Pin 3/Pin 4):** Negative Power Supply Voltage or Ground for Single Supply Operation.

**$V_{OUT}$  (Pin 4/Pin 5):** Voltage Output:

$$V_{OUT} = A_V \cdot (V_{SENSE} \pm V_{OS})$$

$V_{OS}$  is the input offset voltage.  $A_V$  is the gain set by external  $R_{IN1}$ ,  $R_{IN2}$ ,  $R_{OUT}$ .  $A_V = R_{OUT}/R_{IN1}$ , for  $R_{IN1} = R_{IN2}$ .

**NC (Pin 5/Pins 3, 6, 7):** Not Connected Internally.

**+IN (Pin 6/Pin 8):** Positive Sense Input Terminal. Connecting a source to  $V_{S^+}$  and a load to  $V_{S^-}$  will allow the LT6105 to monitor the current through  $R_{SENSE}$ , refer to Figure 1. Connect  $+IN$  to an external gain-setting resistor  $R_{IN2}$  to set the gain.  $+IN$  remains functional for voltages up to 44V, referred to  $V^-$ .

**Exposed Pad (Pin 7) DFN Only:**  $V^-$ . The Exposed Pad is connected to the  $V^-$  pin. It should be connected to the  $V^-$  trace of the PCB, or left floating.

## BLOCK DIAGRAM

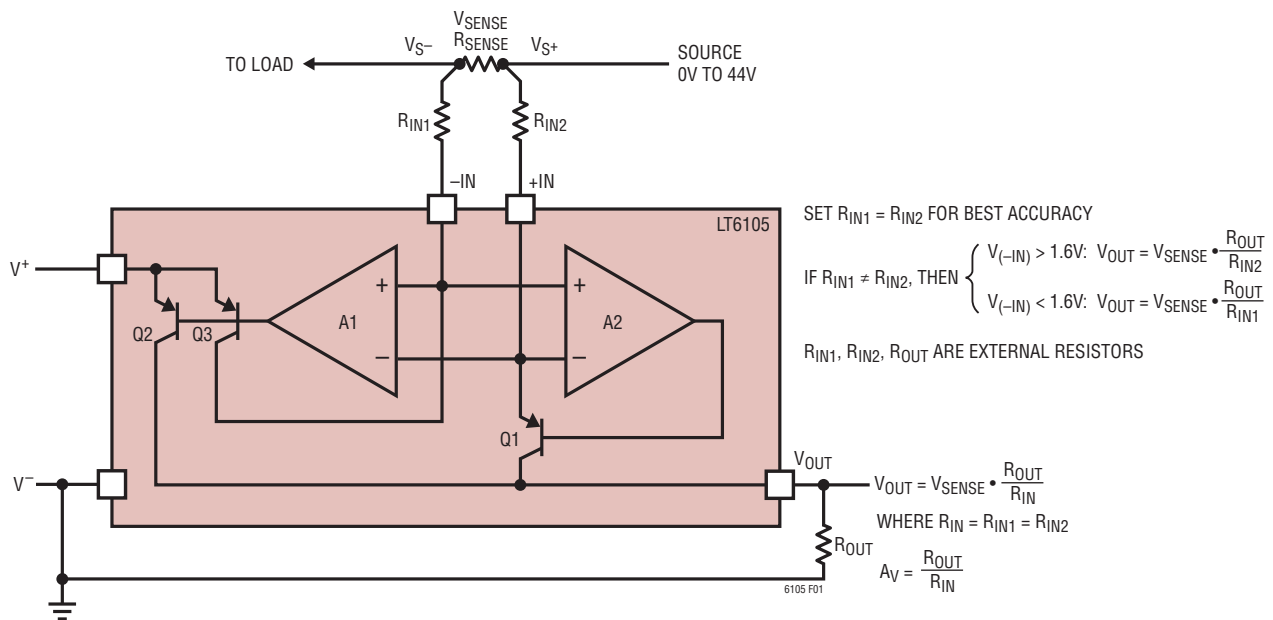


Figure 1. Simplified Block Diagram

## APPLICATIONS INFORMATION

The LT6105 extended input range current sense amplifier (see Figure 1) provides accurate unidirectional monitoring of current through a user-selected sense resistor. The LT6105 is fully specified over a  $-0.3\text{V}$  to  $44\text{V}$  input common mode range. A high PSRR  $V^+$  supply ( $2.85\text{V}$  to  $36\text{V}$ ) powers the current sense amplifier. The input sense voltage is level shifted from the sensed power supply to the ground reference and amplified by a user-selected gain to the output. The output voltage is directly proportional to the current flowing through the sense resistor.

### THEORY OF OPERATION (Refer to Figure 1)

#### Case 1: High Input Voltage ( $1.6\text{V} < V_{-IN} < 44\text{V}$ )

Current from the source at  $V_S^+$  flows through  $R_{SENSE}$  to the load at  $V_S^-$ , creating a sense voltage,  $V_{SENSE}$ . Inputs  $V_S^+$  and  $V_S^-$  apply the sense voltage to  $R_{IN2}$ . The opposite ends of resistors  $R_{IN1}$  and  $R_{IN2}$  are forced to be at equal potentials by the voltage gain of amplifier A2. Thus, the current through  $R_{IN2}$  is  $V_{SENSE}/R_{IN2}$ . The current through  $R_{IN2}$  is forced to flow through transistor Q1 and into  $R_{OUT}$ , creating an output voltage,  $V_{OUT}$ . Under this input operation range, amplifier A1 is kept off. The base current of Q1 has been compensated for and will not contribute to output error. The current from  $R_{IN2}$  flowing through resistor  $R_{OUT}$  gives an output voltage of  $V_{OUT} = V_{SENSE} \cdot R_{OUT}/R_{IN2}$ , producing a gain voltage of  $A_V = V_{OUT}/V_{SENSE} = R_{OUT}/R_{IN2}$ .

#### Case 2: Low Input Voltage ( $0\text{V} < V_{-IN} < 1.6\text{V}$ )

Current from the source at  $V_S^+$  flows through  $R_{SENSE}$  to the load at  $V_S^-$ , creating a sense voltage,  $V_{SENSE}$ . Inputs  $V_S^+$  and  $V_S^-$  apply the sense voltage to  $R_{IN1}$ . The opposite ends of resistors  $R_{IN1}$  and  $R_{IN2}$  are forced to be at equal potentials by the voltage gain of amplifier A1. Thus, the collector current of Q3 will flow out of the  $-IN$  pin through  $R_{IN1}$ . Q2 mirrors this current  $V_{SENSE}/R_{IN1}$  to  $R_{OUT}$ , creating an output voltage,  $V_{OUT}$ . Under this input operation range, amplifier A2 is kept off. This current  $V_{SENSE}/R_{IN1}$  flowing through resistor  $R_{OUT}$  gives an output voltage of  $V_{OUT} = V_{SENSE} \cdot R_{OUT}/R_{IN1}$ , producing a gain voltage of  $A_V = V_{OUT}/V_{SENSE} = R_{OUT}/R_{IN1}$ .

### Selection of External Current Sense Resistor

External  $R_{SENSE}$  resistor selection is a delicate trade-off between power dissipation in the resistor and current measurement accuracy. For high current applications, the user may want to minimize the sense voltage to minimize the power dissipation in the sense resistor.

The system load current will cause both heat and voltage loss in  $R_{SENSE}$ . As a result, the sense resistor should be as small as possible while still providing the input dynamic range required by the measurement. Note that input dynamic range is the difference between the maximum input signal and the minimum accurately reproduced signal, and is limited primarily by input DC offset voltage of the internal amplifier of the LT6105.

The sense resistor value will be set from the minimum signal current that can be accurately resolved by this sense amp. As an example, the LT6105 has a typical input offset of  $100\mu\text{V}$ . If the minimum current is  $20\text{mA}$ , a sense resistor of  $5\text{m}\Omega$  will set  $V_{SENSE}$  to  $100\mu\text{V}$ , which is the same value as the input offset. A larger sense resistor will reduce the error due to offset by increasing the sense voltage for a given load current, but it will limit the maximum peak current for a given application.

For a peak current of  $2\text{A}$  and a maximum  $V_{SENSE}$  of  $80\text{mV}$ ,  $R_{SENSE}$  should not be more than  $40\text{m}\Omega$ . The input offset causes an error equivalent to only  $2.5\text{mA}$  of load current. Peak dissipation is  $160\text{mW}$ . If a  $20\text{m}\Omega$  sense resistor is employed, then the effective current error is  $5\text{mA}$ , while the peak sense voltage is reduced to  $40\text{mV}$  at  $2\text{A}$ , dissipating only  $80\text{mW}$ .

The LT6105's low input offset voltage of  $100\mu\text{V}$  allows for high resolution while limiting the maximum sense voltages. Coupled with full scale sense voltage as large as  $1\text{V}$  for  $R_{IN} = 1\text{k}$ , it can achieve  $80\text{dB}$  of dynamic range.

### Sense Resistor Connection

Kelvin connection of the LT6105's input resistors to the sense resistor should be implemented to provide the highest accuracy in high current applications. Solder connections and PC board interconnect resistance (approximately  $0.5\text{m}\Omega$  per square for 1oz copper) can be a large error in high current systems. A  $5\text{A}$  application might choose

## APPLICATIONS INFORMATION

a 20mΩ sense resistor to give a 100mV full-scale input to the LT6105. Input offset voltage will limit resolution to 5mA. Neglecting contact resistance at solder joints, even one square of PC board copper at each resistor end will cause an error of 5%. This error will grow proportionately higher as monitored current levels rise.

### Gain Setting

The gain is set with three external resistors,  $R_{IN1}$ ,  $R_{IN2}$ ,  $R_{OUT}$ . The gain,  $R_{OUT}/R_{IN}$ , can be selected from 1V/V to 100V/V as long as the maximum current does not exceed 1mA. Select Gain =  $R_{OUT}/R_{IN2}$  for sense input voltage operation greater than 1.6V. Select gain =  $R_{OUT}/R_{IN1}$  for sense input voltage operation less than 1.6V. The overall system error will depend on the resistor tolerance chosen for the application. Set  $R_{IN1} = R_{IN2}$  for best accuracy across the entire input range. The total error will be gain error of the resistors plus the gain error of the LT6105 device.

### Output Signal Range

The LT6105's output signal is developed by current through  $R_{IN2}$  ( $44V > V_{-IN} > 1.6V$ ) or  $R_{IN1}$  ( $0V < V_{-IN} < 1.6V$ ) conducted to the output resistor,  $R_{OUT}$ . This current is  $V_{SENSE}/R_{IN2}$  or  $V_{SENSE}/R_{IN1}$ . The sense amplifier's maximum output current before gain error begins to increase

is 1mA. This allows low value output resistors to be used which helps preserve signal accuracy when the output pin is connected to other systems.

For zero  $V_{SENSE}$ , the internal circuitry gain will force  $V_{OUT}$  to  $V_{O(MIN)}$  referred to  $V^-$ . Depending on output currents,  $V_{OUT}$  may swing positive to within  $V_{O(MAX)}$  referred to  $V^+$  or a maximum of 36V, a limit set by internal junction breakdown. Within these constraints, an amplified, level shifted representation of  $R_{SENSE}$  voltage is developed at  $V_{OUT}$ . The output is well behaved driving capacitive loads.

### CM Input Signal Range

The LT6105 has high CMRR over the full input voltage range. The minimum operation voltage of the sense amplifier inputs is 0V whether  $V^+$  is at 2.7V or 36V. The output remains accurate even when the sense inputs are driven to 44V. The graph in Figure 2 shows that  $V_{OS}$  changes very slightly over a wide input range. Furthermore, either sense inputs  $V_S^+$  and  $V_S^-$  can collapse to 0V without incurring any damage to the device. The LT6105 can handle differential sense voltages up to 44V. For example,  $V_S^+ = 44V$  and  $V_S^- = 0V$  can be a valid condition in a current monitoring application (Figure 3) when an overload protection fuse is blown and  $V_S^-$  voltage collapses to ground. Under this condition, the output of the LT6105 goes to the positive rail,  $V_{O(MAX)}$ .

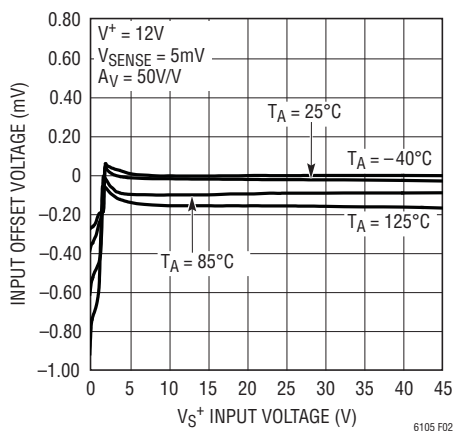


Figure 2. Input Offset Voltage vs  $V_S^+$  Input Voltage

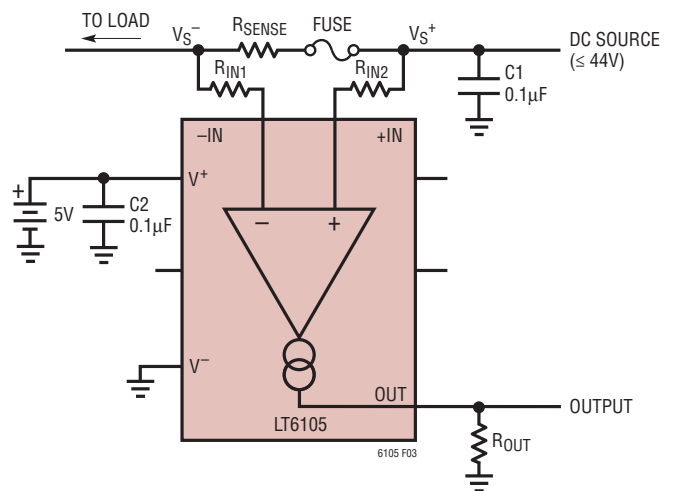


Figure 3. Current Monitoring of a Fuse Protected Circuit



## APPLICATIONS INFORMATION

There is no phase inversion. For the opposite case, when  $V_S^+$  collapses to ground with  $V_S^-$  held up at some higher voltage potential, the output will sit at  $V_{O(MIN)}$ .

### The Two Input Stages Crossover Region

The wide common mode input range is achieved with two input stages. These two input stages consist of a pair of matched common base PNP input transistors and a pair of common emitter PNP input transistors. As result of two input stages, there will be three distinct operating regions around the transition region as shown in the Input Bias Current vs Sense Input Voltage curve in the Typical Performance Characteristics section.

The crossover voltage, the voltage where the  $g_m$  of one input stage is transferred to the other, occurs at 1.6V above  $V^-$ . Near this region, one input stage is shutting off while the other is turning on. Increases in temperature will cause the crossover voltage to decrease. For input operation between 1.6V and 44V, the common base PNPs are active (Q2, Q3 of Figure 1). The typical current through each input at  $V_{SENSE} = 0V$  is 15 $\mu A$ . The input offset voltage is 300 $\mu V$  maximum at room temperature. For input operation between 1.6V to 0V, the other PNP is active. The current out of the inputs at  $V_{SENSE} = 0V$  is 100nA. The input offset voltage is untrimmed and is typically 300 $\mu V$ .

### Selection of External Output Resistor, $R_{OUT}$

The output resistor,  $R_{OUT}$ , determines how the output current is converted to voltage.  $V_{OUT}$  is simply  $I_{OUT} \cdot R_{OUT}$ .

In choosing an output resistor, the maximum output voltage must first be considered. If the following circuit is a buffer or ADC with limited input range, then  $R_{OUT}$  must be chosen so that  $I_{OUT(MAX)} \cdot R_{OUT}$  is less than the allowed maximum input range of this circuit. In addition, the output impedance is determined by  $R_{OUT}$ .

If the circuit to be driven has high input impedance, then almost any useful output impedance will be acceptable. However, if the driven circuit has relatively low input impedance, or draws spikes of current such as an ADC might do, then a lower  $R_{OUT}$  value may be required in order to preserve the accuracy of the output. As an example, if the input impedance of the driven circuit is 100 times  $R_{OUT}$ , then the accuracy of  $V_{OUT}$  will be reduced by 1% since:

$$\begin{aligned} V_{OUT} &= I_{OUT} \cdot \frac{R_{OUT} \cdot R_{IN(DRIVEN)}}{R_{OUT} + R_{IN(DRIVEN)}} \\ &= I_{OUT} \cdot R_{OUT} \cdot \frac{100}{101} = 0.99 \cdot I_{OUT} \cdot R_{OUT} \end{aligned}$$

### Full-Scale Sense Voltage, Selection of External Input Resistor, $R_{IN}$

The external input resistor,  $R_{IN}$ , controls the transconductance of the current sense circuit. Since  $I_{OUT} = V_{SENSE} / R_{IN}$ , transconductance  $g_m = 1 / R_{IN}$ . For example, if  $R_{IN} = 100$ , then  $I_{OUT} = V_{SENSE} / 100$  or  $I_{OUT} = 1mA$  for  $V_{SENSE} = 100mV$ .  $R_{IN}$  should be chosen to allow the required resolution while limiting the output current. The LT6105 can output more than 1mA into  $R_{OUT}$  without introducing a significant increase in gain error. By setting  $R_{IN}$  such that the largest expected sense voltage gives  $I_{OUT} = 1mA$ , then the maximum output dynamic range is available. Output dynamic range is limited by both the maximum allowed output current and the maximum allowed output voltage, as well as the minimum practical output signal. If less dynamic range is required, then  $R_{IN}$  can be increased accordingly, reducing the maximum output current and power dissipation. The LT6105's performance is optimized for values of  $R_{IN} = 100\Omega$  to 1k. Values outside this range may result in additional errors. The power dissipation across  $R_{IN}$  and  $R_{OUT}$  should not exceed the resistors' recommended ratings.

## APPLICATIONS INFORMATION

### Error Sources

The current sense system uses an amplifier, current mirrors and external resistors to apply gain and level shifting. The output is then dependent on the matching characteristics of the current mirrors, characteristics of the amplifier such as gain and input offset, as well as matching of external resistors. Ideally, the circuit output is:

$$V_{OUT} = V_{SENSE} \cdot \frac{R_{OUT}}{R_{IN}}; V_{SENSE} = I_{SENSE} \cdot R_{SENSE}$$

In this case, the only error is due to resistor mismatch, which provides an error in gain only. Mismatch in the internal current mirror adds to gain error but is trimmed to less than 0.3%. Offset voltage and sense input current are the main cause of any additional error.

### Error Due to Input Offset Voltage

Dynamic range is inversely proportional to the input offset voltage. Dynamic range can be thought of as the maximum  $V_{SENSE}$  divided by  $V_{OS}$ . The offset voltage of the LT6105 is typically only  $\pm 100\mu V$ .

### Error Due to Sense Input Offset Current

Input offset current or mismatches in input bias current will introduce an additional input offset voltage term. Typical input offset current is  $0.05\mu A$ . Lower values of  $R_{IN}$  will keep this error to a minimum. For example, if  $R_{IN} = 100\Omega$ , then the additional offset is  $5\mu V$ .

### Output Current Limitations Due to Power Dissipation

The LT6105 can deliver up to 1mA continuous current to the output pin. This output current,  $I_{OUT}$ , is the mirrored current which flows through  $R_{IN2}$  and enters the current sense amp via the +IN pin for  $V_{-IN} > 1.6V$ , and exits out of -IN through  $R_{IN1}$  for  $V_{-IN} < 1.6V$ . The total power dissipation due to input currents,  $P_{IN}$ , and the dissipation due to internal mirrored currents,  $P_Q$ :

$$P_{TOTAL} = P_{IN} + P_Q$$

$$P_{IN} = (V_{+IN}) \cdot I_{RIN2}; V_{-IN} > 1.6V$$

or

$$P_{IN} = (V^+ - (V_{-IN})) \cdot I_{RIN1}; V_{-IN} < 1.6V$$

Since the current exiting -IN is coming from  $V^+$ , the voltage is  $V^+ - V_{-IN}$ . Taking the worst case  $V_{-IN} = 0V$ , the above equation becomes:

$$P_{IN} \cong V^+ \cdot I_{RIN1}, \text{ for } V_{-IN} < 1.6V.$$

The power dissipated due to internal mirrored currents:

$$P_Q = 2 \cdot I_{OUT} \cdot V^+$$

The factor of 2 is the result of internal current shifting and 1:1 mirroring.

At maximum supply and maximum output current, the total power dissipation can exceed 100mW. This will cause significant heating of the LT6105 die. In order to prevent damage to the LT6105, the maximum expected dissipation in each application should be calculated. This number can be multiplied by the  $\theta_{JA}$  value listed in the Pin Configuration section to find the maximum expected die temperature. This must not be allowed to exceed  $150^\circ C$ , or performance may be degraded. As an example, if an LT6105 in the MSOP package is to be run at  $V_S^+ = 44V$  and  $V^+ = 36V$  with 1mA output current at  $80^\circ C$  ambient:

$$P_{Q(MAX)} = 2 \cdot I_{OUT(MAX)} \cdot V^+ = P_{Q(MAX)} = 72mW$$

$$P_{IN(MAX)} = I_{RIN2(MAX)} \cdot V_{+IN(MAX)} = 44mW$$

$$T_{RISE} = \theta_{JA} \cdot P_{TOTAL(MAX)}$$

$$T_{MAX} = T_{AMBIENT} + T_{RISE}$$

$T_{MAX}$  must be  $< 150^\circ C$

$P_{TOTAL(MAX)} = 116mW$  and the maximum die temperature will be  $109^\circ C$ . If this same circuit must run at  $125^\circ C$  ambient, the maximum die temperature will increase to  $150^\circ C$ . Note that supply current, and therefore  $P_Q$ , is proportional to temperature. Refer to the Typical Performance Characteristics section. In this condition, the maximum output current should be reduced to avoid device damage. The DCB package, on the other hand, has a lower  $\theta_{JA}$  and subsequently, a lower die temperature increase than the MSOP. With the same condition as above, the DCB will rise only  $7.5^\circ C$  to  $87.5^\circ C$  and  $132.5^\circ C$ , respectively.

It is important to note that the LT6105 has been designed to provide at least 1mA to the output when required, and can deliver more under large  $V_{SENSE}$  conditions. Care must be taken to limit the maximum output current by proper choice of sense resistor and input resistors.

## APPLICATIONS INFORMATION

### Output Filtering

The output voltage,  $V_{OUT}$  is simply  $I_{OUT} \cdot Z_{OUT}$ . This makes filtering straightforward. Any circuit may be used which generates the required  $Z_{OUT}$  to get the desired filter response. For example, a capacitor in parallel with  $R_{OUT}$  will give a low pass response. This will reduce unwanted noise from the output, and may also be useful as a charge reservoir to keep the output steady while driving a switching circuit such as a mux or an ADC. This output capacitor in parallel with an output resistor will create a pole in the output response at:

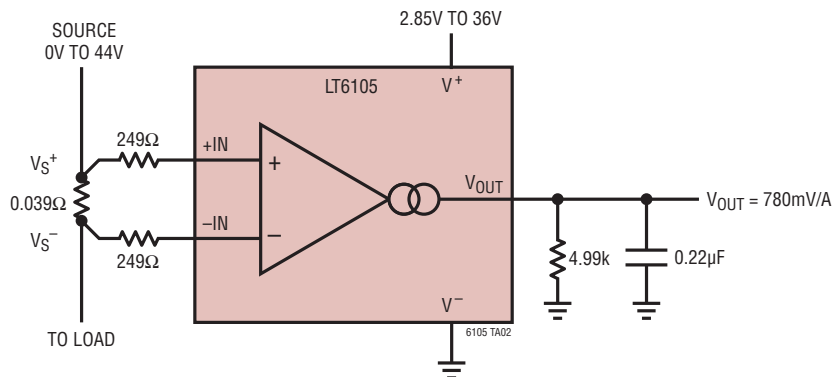
$$f_{-3db} = \frac{1}{2 \cdot \pi \cdot R_{OUT} \cdot C_{OUT}}$$

### Response Time

The LT6105 is designed to exhibit fast response to inputs for the purpose of circuit protection or signal transmission. This response time will be affected by the external circuit in two ways—delay and speed. If the output current is very low and an input transient occurs, there may be an increased delay before the output voltage begins changing. This can be improved by increasing the minimum output current, either by increasing  $R_{SENSE}$  or decreasing  $R_{IN}$ . The effect of increased output current is illustrated in the step response curves in the Typical Performance Characteristics section of this data sheet. Note that the curves are labeled with respect to the initial output currents. The speed is also affected by the external circuit. In this case, if the input changes very quickly, the internal amplifier will slew the base of the internal output PNP (Figure 1) in order to maintain the internal loop. This results in current flowing through  $R_{IN}$  and the internal PNP. This current slew rate will be determined by the amplifier and PNP characteristics as well as the input resistor,  $R_{IN}$ . See the Slew Rate vs  $R_{IN}$  curve in the Typical Performance Characteristics section. Using a smaller  $R_{IN}$  will allow the output current to increase more quickly, decreasing the response time at the output. This will also have the effect of increasing the maximum output current.

## TYPICAL APPLICATIONS

Gain of 20 Current Sense Amplifier with Output Filtering





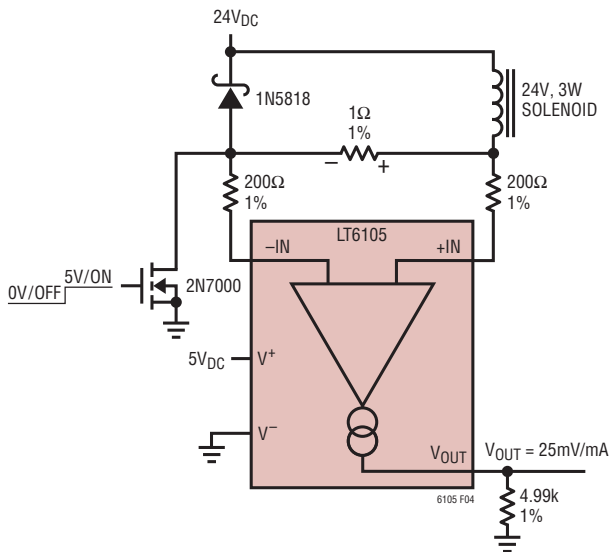
## TYPICAL APPLICATIONS

### Solenoid Monitor

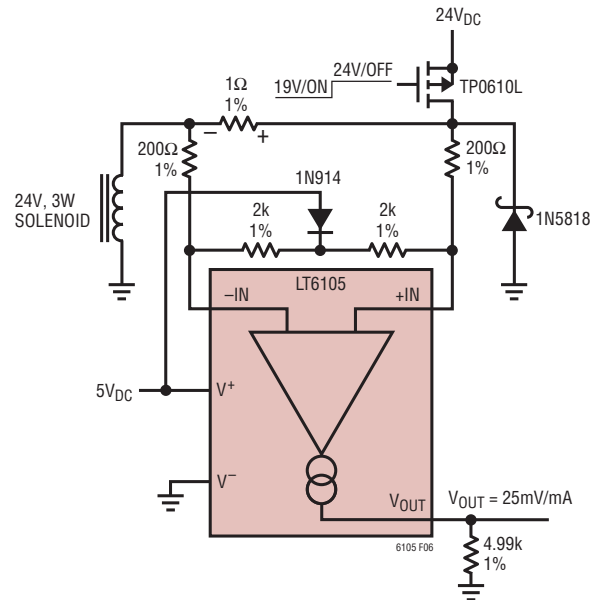
The large input common mode range of the LT6105 makes it suitable for monitoring currents in quarter, half and full bridge inductive load driving applications. Figure 4 shows an example of a quarter bridge. The MOSFET pulls down on the bottom of the solenoid to increase solenoid current. It lets go to decrease current, and the solenoid voltage freewheels around the Schottky diode. Current measurement waveforms are shown in Figure 5. The small glitches occur due to the action of the solenoid plunger, and this provides an opportunity for

mechanical system monitoring without an independent sensor or limit switch.

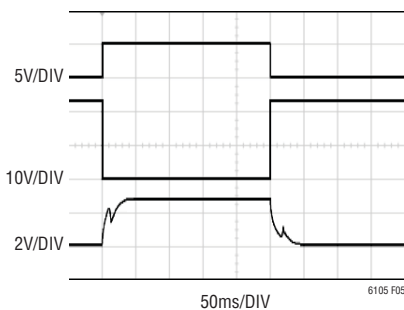
Figure 6 shows another solenoid driver circuit, this time with one end of the solenoid grounded and a P-channel MOSFET pulling up on the other end. In this case, the inductor freewheels around ground, imposing a negative input common mode voltage of one Schottky diode drop. This voltage may exceed the input range of the LT6105. This does not endanger the device, but it severely degrades its accuracy. In order to avoid violating the input range, pull-up resistors may be used as shown.



**Figure 4. Simplest Form of a Solenoid Driver. The LT6105 Monitors the Current in Both On and Freewheel States. The Lowest Common Mode Voltage Is 0V, While the Highest Is 24V Plus the Forward Voltage of the Schottky Diode**



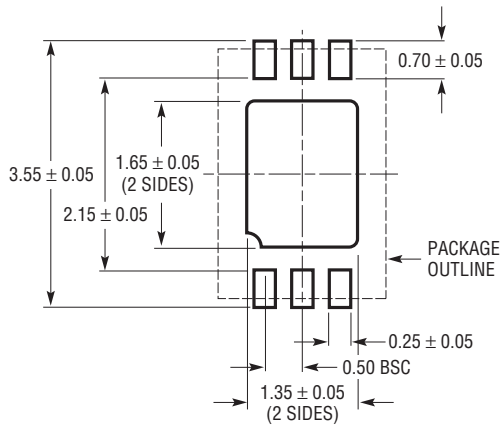
**Figure 6. A Similar Circuit to Figure 4, but with Solenoid Grounded, so Freewheeling Forces Inputs Negative. Providing Resistive Pull-Ups Keeps Amplifier Inputs From Falling Outside of Their Accurate Input Range**



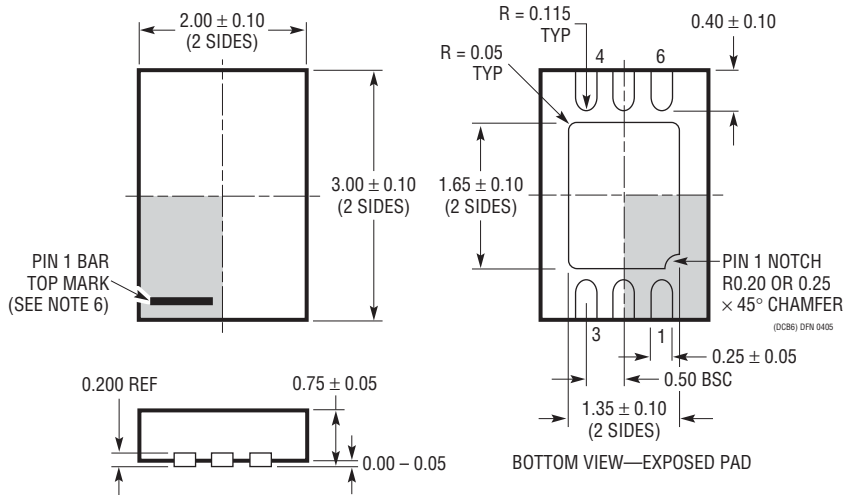
**Figure 5. Current Measurement Waveforms. The Top Trace Is the MOSFET Gate with High On. The Middle Trace Is the Bottom of the Solenoid/Inductor. The Bottom Trace Is the LT6105 Output, Representing Solenoid Current at 80mA/DIV. Glitches Are Useful Indicators of Solenoid Plunger Movement**

**PACKAGE DESCRIPTION**

**DCB Package**  
**6-Lead Plastic DFN (2mm × 3mm)**  
 (Reference LTC DWG # 05-08-1715)



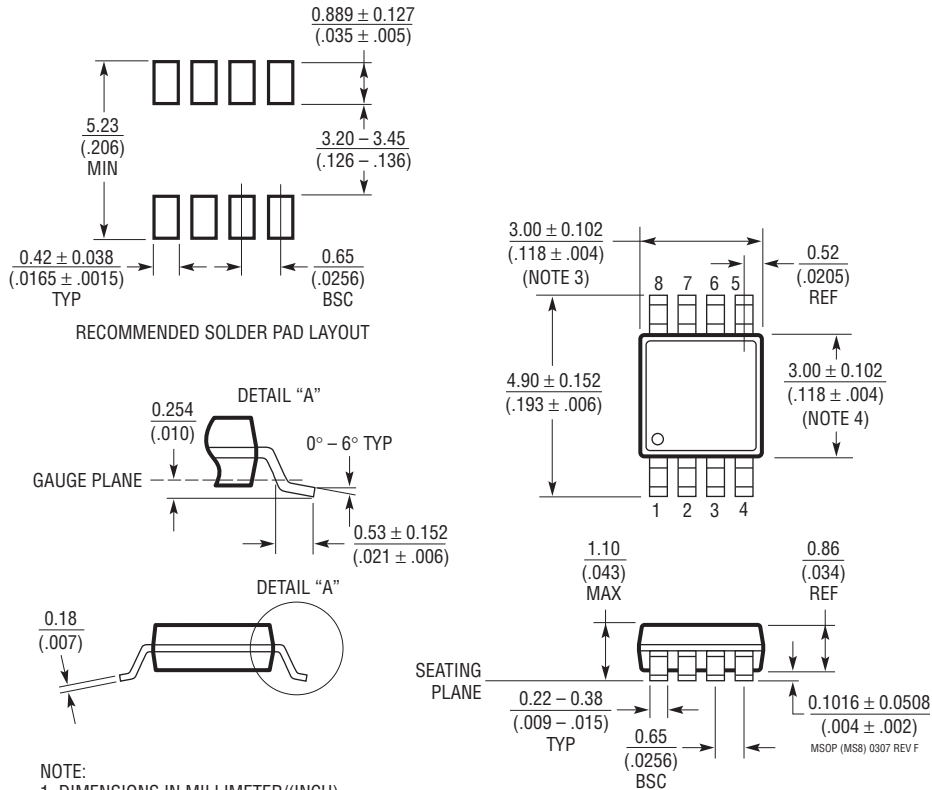
RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS



- NOTE:
1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE M0-229 VARIATION OF (TBD)
  2. DRAWING NOT TO SCALE
  3. ALL DIMENSIONS ARE IN MILLIMETERS
  4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
  5. EXPOSED PAD SHALL BE SOLDER PLATED
  6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

**PACKAGE DESCRIPTION**

**MS8 Package**  
**8-Lead Plastic MSOP**  
 (Reference LTC DWG # 05-08-1660)

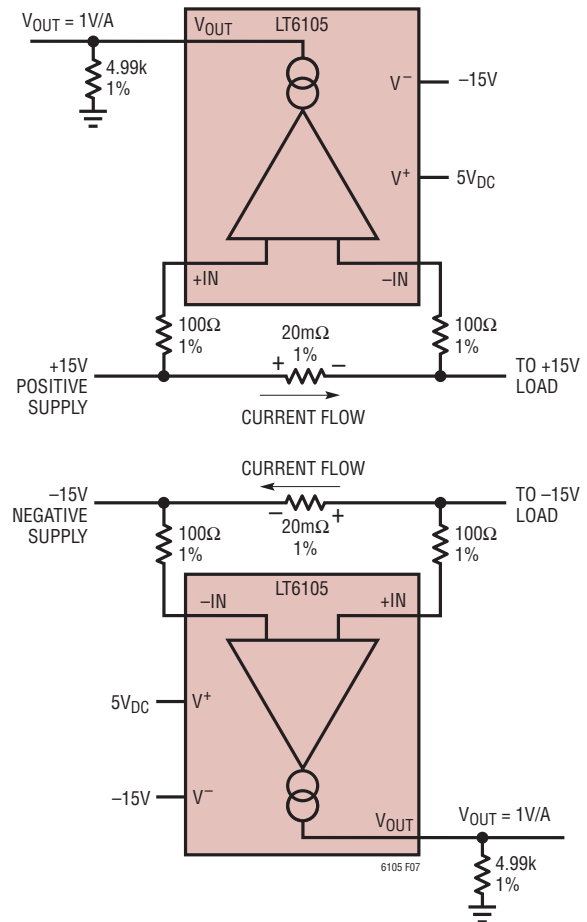


- NOTE:
1. DIMENSIONS IN MILLIMETER/(INCH)
  2. DRAWING NOT TO SCALE
  3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.  
MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
  4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.  
INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
  5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102mm (.004") MAX

## TYPICAL APPLICATION

### Supply Monitoring

The input common mode range of the LT6105 also makes it suitable for monitoring either positive or negative supplies. Figure 7 shows one LT6105 applied as a simple positive supply monitor, and another LT6105 as a simple negative supply monitor. Note that the schematics are practically identical and both have outputs conveniently referred to ground. The only requirement for negative supply monitoring, in addition to the usual constraints of the absolute maximum ratings, is that the negative supply to that LT6105 be at least as negative as the supply it is monitoring.



**Figure 7. The LT6105 Can Monitor the Current of Either Positive or Negative Supplies, Without a Schematic Change. Just Ensure That the Current Flow Is in the Correct Direction**

## RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1787/LT1787HV	Precision, Bidirectional, High Side Current Sense Amplifier	2.7V to 60V Operation, 75 $\mu$ V Offset, 60 $\mu$ A Current Draw
LTC4150	Coulomb Counter/Battery Gas Gauge	Indicates Charge Quantity and Polarity
LT6100	Gain-Selectable High Side Current Sense Amplifier	4.1V to 48V Operation, Pin-Selectable Gain: 10V/V, 12.5V/V, 20V/V, 25V/V, 40V/V, 50V/V
LTC6101/ LTC6101HV	High Voltage High Side Current Sense Amplifier	4V to 60V/5V to 100V Operation, External Resistor Set Gain, SOT23
LTC6102/ LTC6102HV	Zero Drift High Side Current Sense Amplifier	4V to 60V/5V to 100V Operation, $\pm$ 10 $\mu$ V Offset, 1 $\mu$ s Step Response, MSOP8 / DFN
LTC6103	Dual High Side Precision Current Sense Amplifier	4V to 60V, Gain Configurable, 8-Pin MSOP
LTC6104	Bidirectional High Side Precision Current Sense Amplifier	4V to 60V, Gain Configurable, 8-Pin MSOP
LT6106	Low Cost, High Side Precision Current Sense Amplifier	2.7V to 36V, Gain Configurable, SOT23

6105fa



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- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- Лицензия ФСБ на осуществление работ с использованием сведений, составляющих государственную тайну;
- Поставка специализированных компонентов (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Aeroflex, Peregrine, Syfer, Eurofarad, Texas Instrument, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

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- Подбор аналогов;
- Консультации по применению компонента;
- Поставка образцов и прототипов;
- Техническая поддержка проекта;
- Защита от снятия компонента с производства.



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