

# **Power Supply IC Series for TFT-LCD Panels**

# 5V Input Multi-channel System Power Supply IC





**BD8153EFV** No.09035JBT09

#### Description

The BD8153EFV is a system power supply IC for TFT panels.A 1-chip IC providing a total of four voltages required for TFT panels, i.e., logic voltage, sauce voltage, gate high-level, and gate low-level voltage, thus constructing a TFT panel power supply with minimal components required.

#### ● Features (BD8153EFV)

- 1) Operates in an operating voltage range as low as 2.1 V to 6. 0 V.
- 2) Incorporates a step-up DC/DC converter.
- 3) Incorporates a 3.3-V regulator.
- 4) Incorporates positive and negative-side charge pumps.
- 5) Switching frequency of 1100 kHz
- 6) DC/DC converter feedback voltage of 1.24 V  $\pm$  1%
- 7) Incorporates a gate shading function
- 8) Under-voltage lockout protection circuit
- 9) Thermal shutdown circuit
- 10) Overcurrent protection circuit
- 11) HTSSOP-B24 package

#### Applications

Liquid crystal TV, PC monitor, and TFT-LCD panel

Absolute maximum ratings (Ta = 25°C)

Parameter	Symbol	Limit	Unit
Power supply voltage	VCC	7	V
Vo1 voltage	Vo1	19	V
Vo2 voltage	Vo2	32	V
SW voltage	Vsw	19	V
Maximum junction temperature	Tjmax	150	°C
Power dissipation	Pd	1100*	mW
Operating temperature range	Topr	-40 to 125	°C
Storage temperature range	Tstg	-55 to 150	°C

<sup>\*</sup> Reduced by 4.7 mW/°C over 25°C, when mounted on a glass epoxy board. (70 mm × 70 mm × 1.6 mm).

# Recommended Operating Ranges

Doromotor	Cumbal	Lir	Unit	
Parameter	Symbol	MIN	MAX	Unit
Power supply voltage	VCC	2.1	6	V
Vo1 voltage	Vo1	8	18	V
SW voltage	Vsw	_	18	V
SW Current	Isw	_	1.8	Α
Vo2 voltage	Vo2	_	30	V

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# ●Electrical Characteristics (Unless otherwise specified, VCC = 5 V; Vo1 = 15 V; Vo2 = 25 V; Ta = 25°C)

# 1 DC/DC Converter Block

Doromotor	Cumbal		Limit		l loit	Conditions	
Parameter	Symbol	Min.	Тур.	Max.	Unit	Conditions	
[Soft start]				•			
Source current	Iso	6	10	14	μΑ	Vss = 0.5 V	
Sinking current	Isi	0.1	0.2	1.0	mΑ	Vss = 0.5 V,VDD = 1.65 V	
[Error amp]							
Input bias current 1	IFB1	_	0.1	0.5	μΑ		
Feedback voltage 1	VFB1	1.227	1.240	1.253	V	Buffer	
Voltage gain	AV	_	200	_	V/V	*	
Sinking current	lol	25	50	100	μΑ	VFB = 1.5 V VCOMP = 0.5 V	
Source current	loo	-100	-50	-25	μΑ	VFB = 1.0 V VCOMP = 0.5 V	
[SW]							
ON resistance N-channel	Ron_n	50	200	600	mΩ	*	
Leak current N-channel	ILEAKN	_	_	10	μA	Vsw = 18 V	
Maximum duty cycle	Dмах	75	85	95	%		
[Overcurrent protection]				<u> </u>			
Saw current limit	Insw	2	3	_	Α	*	

#### 2. Regulator controller

Parameter	Coursels al	Limit			1.1	O an alistia and		
	Symbol	Min.	Тур.	Max.	Unit	Conditions		
[Error amp]								
VDD voltage	VDD	3.2	3.3	3.4	V			
Maximum base current	Івмах	4	7	11	mA			
Line regulation	Regl	_	10	30	mV	VCC = 4.5 V to 5.5 V		
Load regulation	RegL	_	10	50	mV	Io = 10 mA to 100 mA		
[Under-voltage lockout protection]								
Off threshold voltage	VROFF	1.7	1.8	1.9	V			
On threshold voltage	VRON	1.6	1.7	1.8	V			

OThis product is not designed for protection against radio active rays.

\* Design guarantee (No total shipment inspection is made.)

# ●Electrical Characteristics (Unless otherwise specified, VCC = 5 V; Vo1 = 15 V; Vo2 = 25 V; Ta = 25°C)

3.Charge pump

Doromotor	Cumbal	Limit			l lait	O an alitica a
Parameter	Symbol	Min.	Тур.	Max.	Unit	Conditions
[Error amp]						
Input bias current 2	IFB2	_	0.1	0.5	μA	
Input bias current 3	IFB3	_	0.1	0.5	μA	
Feedback voltage 2	VFB2	1.183	1.240	1.307	V	
Feedback voltage 3	VFB3	0.15	0.2	0.25	V	
[Delay start block]						
Source current	IDSO	3	5	7	μA	VDLS = 0.5V
Sinking current	IDSI	0.1	0.5	1.0	mA	VDLS = 0.5V
Startup voltage	VsT	0.45	0.60	0.75	V	
[Switch]						
ON resistance N-channel	Ron_nc	0.5	2	4	Ω	Io = 10 mA *
ON resistance P-channel	Ron_pc	0.5	4	8	Ω	Io = -10 mA *
[Diode]						
Voltage of diode	Vf	600	710	800	mV	Io = 10 mA
[Gate shading block]						
ON resistance N-channel	Ron_ngs	2	10	20	Ω	Io = 10 mA *
ON resistance P-channel	Ron_pgs	2	10	20	Ω	Io = -10 mA *
Leak current N-channel	ILEAK_NGS	_	_	10	μA	
Leak current P-channel	ILEAK_PGS		_	10	μΑ	
High voltage	IGH	VDD × 0.7	VDD	_	V	
Low voltage	IGL	_	0	VDD × 0.3	V	
Input current	IIG	8	16.5	30	μA	IG = 3.3 V

#### 4.Overall

Parameter	Symbol	Limit			Unit	Conditions			
Farameter	Symbol	Min.	Тур.	Max.	Ullit	Conditions			
Reference block]									
Reference voltage	VREF	1.215	1.240	1.265	V				
Drive current	IREF	-	23	_	mA	VREF = 0 V			
Load regulation	$\Delta V$		1	10	mV	IREF = -1 mA			
[Oscillator]									
Oscillating frequency	Fosc	0.94	1.1	1.265	MHz				
[Oscillator]									
DET 1 On threshold voltage	VDON1	1.7	1.8	1.9	V				
DET 1 Off threshold voltage	VDOFF1	1.6	1.7	1.8	V				
DET 2 On threshold voltage	VDON2	1.02	1.12	1.22	V				
DET 2 Off threshold voltage	VDOFF2	0.90	1.00	1.10	V				
DET 3 On threshold voltage	VDON3	0.25	0.30	0.35	V				
DET 3 Off threshold voltage	VDOFF3	0.35	0.41	0.47	V				
DET 4 On threshold voltage	VDON4	1.02	1.12	1.22	V				
DET 4 Off threshold voltage	VDOFF4	0.90	1.00	1.10	V				
[Device]									
Average circuit current	Icc	0.5	2	5	mA	No switching			

OThis product is not designed for protection against radio active rays.

\* Design guarantee (No total shipment inspection is made.)

#### Reference Data (Unless otherwise specified, Ta = 25°C)

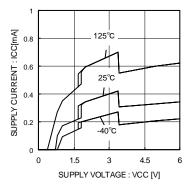


Fig. 1 Total Supply Current 1

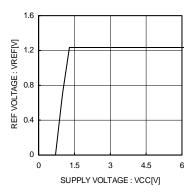


Fig. 4 Internal Reference Line Regulation

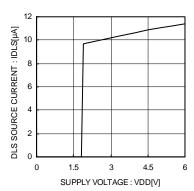


Fig. 7 DLS Source Current

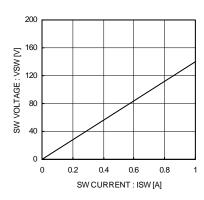


Fig. 10 SW On Resistance

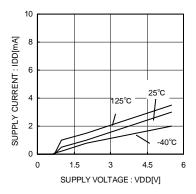


Fig. 2 Total Supply Current 2

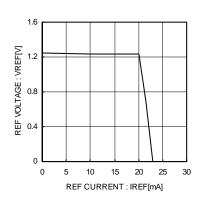


Fig. 5 Internal Reference Load Regulation

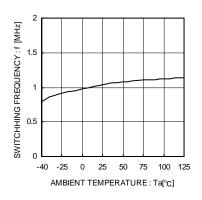


Fig. 8 Switching Frequency Temperature

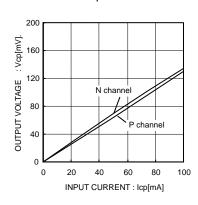


Fig. 11 Charge Pump On Voltage

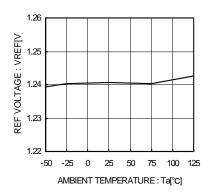


Fig. 3 Internal Reference Temperature

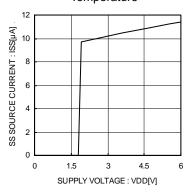


Fig. 6 SS Source Current

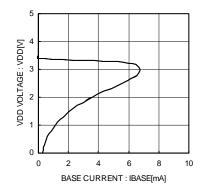


Fig. 9 REG Current Capacity

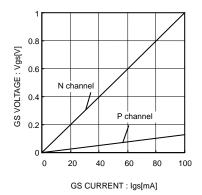


Fig. 12 Gate Shading On Voltage

#### ■Reference Data (Unless otherwise specified, Ta = 25°C)

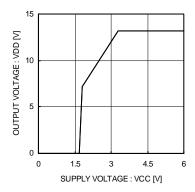


Fig. 13 Vo1 Line Regulation

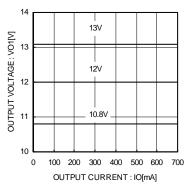


Fig. 16 Vo1 Load Regulation

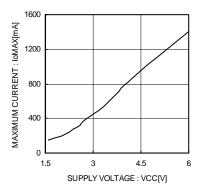


Fig. 19 Power Supply Voltage vs Max. Output Current Capacity

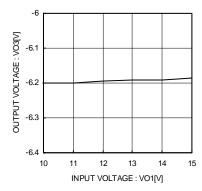


Fig. 22 Negative-side Charge Pump Line Regulation

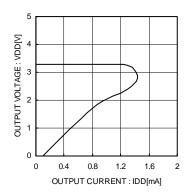


Fig. 14 VDD Load Regulation

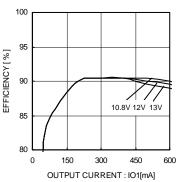


Fig. 17 Efficiency vs Output Current

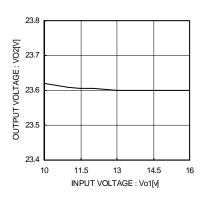


Fig. 20 Vo2 Line Regulation

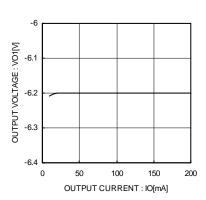


Fig. 23 Negative-side Charge Pump Load Regulation

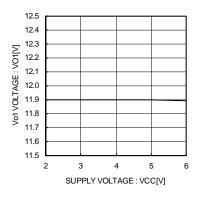


Fig. 15 Vo1 Line Regulation

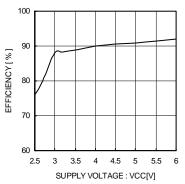


Fig. 18 Efficiency vs Power Supply Voltage

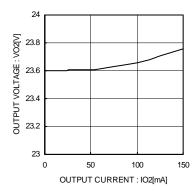


Fig. 21 Vo2 Load Regulation

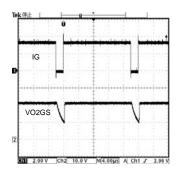
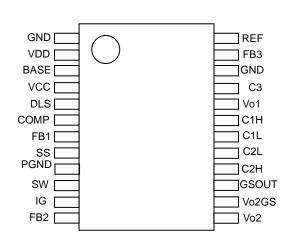


Fig. 24 Gate Shading Output Waveform

# ●Pin Assignments Diagram



# **●**Block Diagram

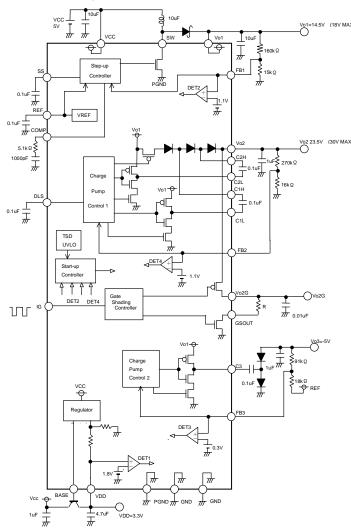


Fig. 25 Pin Arrangements and Block Diagram

●Pin Assignments and Function

PIN NO.	Pin name	Function	PIN NO.	Pin name	Function
1	GND	Ground pin	13	Vo2	Positive-side charge pump output
2	VDD	LDO feedback input pin	14	Vo2GS	Gate shading source output pin
3	BASE	LDO base drive output pin	15	GSOUT	Gate shading sink output pin
4	VCC	Power supply input pin	16	C2H	Flying capacitor connection pin
5	DLS	Capacity connection pin for delay start	17	C2L	Flying capacitor connection pin
6	COMP	DC/DC difference amplifier output	18	C1L	Flying capacitor connection pin
7	FB1	DC/DC feedback input	19	C1H	Flying capacitor connection pin
8	SS	Soft start capacitor connection pin	20	Vo1	Negative-side charge pump power supply input pin
9	PGND	Ground pin	21	C3	Negative-side charge pump driver output
10	SW	Switch output	22	GND	Ground pin
11	IG	Gate shading input	23	FB3	Negative-side charge pump feedback input
12	FB2	Positive-side charge pump feedback input	24	REF	Internal standard output pin

#### ●Block Function

• Step-up Controller

A controller circuit for DC/DC boosting.

The switching duty is controlled so that the feedback voltage FB1 is set to 1.24 V (typ.).

A soft start operates at the time of starting. Therefore, the switching duty is controlled by the SS pin voltage.

• Charge Pump Control 1

A controller circuit for the positive-side charge pump.

The switching amplitude is controlled so that the feedback voltage FB2 will be set to 1.24 V (typ.).

The start delay time can be set in the DLS terminal at the time of starting.

When the DLS voltage reaches 0.6 V (Typ.), switching waves will be output from the C1L and C2L pins.

• Charge Pump Control 2

A controller circuit for the negative-side charge pump.

The switching amplitude is controlled so that the feedback voltage FB2 will be set to 0.6 V (Typ.).

Gate Shading Controller

A controller circuit of gate shading.

The Vo2GS and GSOUT are in on/off control according to IG pin input.

Regulator Control

A regulator controller circuit for VDD voltage generation.

The base pin current is controlled so that VDD voltage will be set to 3.3 V (typ.).

• DET 1 to DET 4

A detection circuit of each output voltage. This detected signal is used for the starting sequential circuit.

Start-up Controller

A control circuit for the starting sequence.

Controls to start in order of Vcc  $\rightarrow$ VDD  $\rightarrow$ Vo1  $\rightarrow$ Vo3  $\rightarrow$ Vo2.

VRFF

A block that generates internal reference voltage. 1.24V (Typ.) is output.

• TSD/UVLO

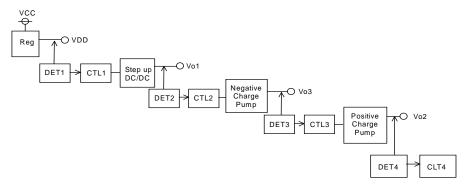
Thermal shutdown/Under-voltage lockout protection/circuit blocks.

The thermal shutdown circuit is shut down at an IC internal temperature of 175°C and reset at 160°C.

The under-voltage lockout protection circuit shuts down the IC when the VCC is 1.8 V (typ.) or below.

#### Starting sequence

For malfunction prevention, starting logic control operates so that each output will rise in order of Vcc  $\rightarrow$ VDD  $\rightarrow$ Vo1  $\rightarrow$ Vo3  $\rightarrow$ Vo2. As shown below, detectors DET1 to DET3 detect that the output on the detection side has reached 90% (typ.) of the set voltage, and starts the next block.



#### Starting sequence model

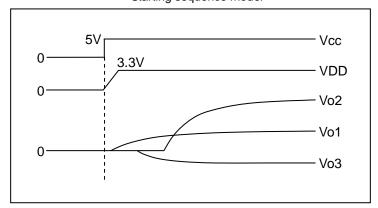


Fig. 26 Starting Timing Chart

#### Selecting Application Components

#### (1) Setting the Output L Constant

The coil to use for output is decided by the rating current ILR and input current maximum value IINMAX of the coil.

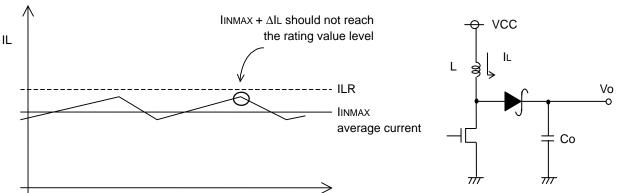


Fig. 27 Coil Current Waveform

Fig. 28 Output Application Circuit Diagram

Adjust so that Inmax +  $\Delta$ IL does not reach the rating current value ILR. At this time,  $\Delta$ IL can be obtained by the following equation.

$$\Delta IL = \frac{1}{L} VCC \times \frac{VO-VCC}{VCC} \times \frac{1}{f}$$
 [A] Here, f is the switching frequency.

Set with sufficient margin because the coil value may have the dispersion of  $\pm 30\%$ . If the coil current exceeds the rating current ILR of the coil, it may damage the IC internal element.

BD8153EFV uses the current mode DC/DC converter control and has the optimized design at the coil value. A coil inductance (L) of  $4.7 \mu H$  to  $15 \mu H$  is recommended from viewpoints of electric power efficiency, response, and stability.

#### (2) Output Capacity Settings

For the capacitor to use for the output, select the capacitor which has the larger value in the ripple voltage VPP allowance value and the drop voltage allowance value at the time of sudden load change. Output ripple voltage is decided by the following equation.

$$\Delta VPP = ILMAX \times RESR + \frac{1}{fCo} \times \frac{VCC}{Vo} \times (ILMAX - \frac{\Delta IL}{2})$$
 [V] Here, f is the switching frequency.

Perform setting so that the voltage is within the allowable ripple voltage range.

For the drop voltage during sudden load change; VDR, please perform the rough calculation by the following equation.

$$VDR = \frac{\Delta I}{Co} \times 10 \text{ us}$$
 [V]

However, 10 µs is the rough calculation value of the DC/DC response speed. Please set the capacitance considering the sufficient margin so that these two values are within the standard value range.

# (3) Selecting the Input Capacitor

Since the peak current flows between the input and output at the DC/DC converter, a capacitor is required to install at the input side. For the reason, the low ESR capacitor is recommended as an input capacitor which has the value more than 10  $\mu$ F and less than 100 m $\Omega$ . If a capacitor out of this range is selected, the excessive ripple voltage is superposed on the input voltage, accordingly it may cause the malfunction of IC.

However these conditions may vary according to the load current, input voltage, output voltage, inductance and switching frequency. Be sure to perform the margin check using the actual product.

# (4) Setting Rc, Cc of the Phase Compensation Circuit

In the current mode control, since the coil current is controlled, a pole (phase lag) made by the CR filter composed of the output capacitor and load resistor will be created in the low frequency range, and a zero (phase lead) by the output capacitor and ESR of capacitor will be created in the high frequency range. In this case, to cancel the pole of the power amplifier, it is easy to compensate by adding the zero point with Cc and Rc to the output from the error amp as shown in the illustration.

#### Open loop gain characteristics

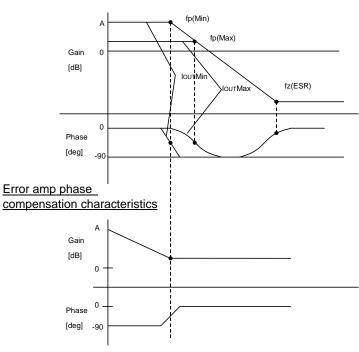
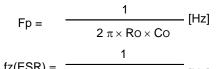


Fig. 29 Gain vs Phase



Pole at the power amplification stage

When the output current reduces, the load resistance Ro increases and the pole frequency lowers.

$$fp(Min) = \frac{1}{2 \pi \times ROMax \times CO}$$
 [Hz]  $\leftarrow$  at light load 
$$fz(Max) = \frac{1}{2 \pi \times ROMin \times CO}$$
 [Hz]  $\leftarrow$  at heavy load

Zero at the power amplification stage

When the output capacitor is set larger, the pole frequency lowers but the zero frequency will not change. (This is because the capacitor ESR becomes 1/2 when the capacitor becomes 2 times.)

$$fp(Amp.) = \frac{1}{2 \pi \times Rc \times Cc} [Hz]$$

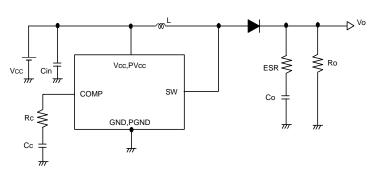


Fig. 30 Application Circuit Diagram

It is possible to realize the stable feedback loop by canceling the pole fp(Min.), which is created by the output capacitor and load resistor, with CR zero compensation of the error amp as shown below.

$$fz(Amp.) = fp(Min.)$$

$$\frac{1}{2 \pi \times Rc \times Cc} = \frac{1}{2 \pi \times Romax \times Co} [Hz]$$

# (5) Regulator Controller Settings

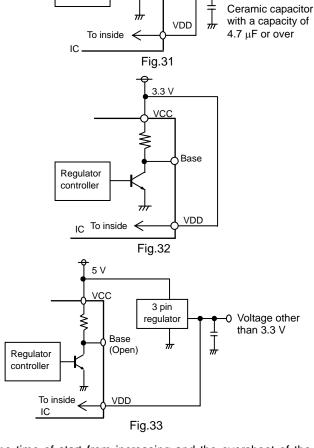
The IC incorporates a 3.3-V regulator controller, and a regulator can be formed by using an external PNP transistor. Design the current capability of the regulator with a margin according to the following formula.

 $IOMAX = 7mA \times hfe$  [A]

The hfe is the current gain of the external PNP transistor. 7 mA is the sinking current of the internal transistor.

It is not necessary to use the regulator if the input voltage is  $3.3~\rm V.$  In that case, input  $3.3~\rm V$  to both VCC and VDD.

When incorporating a regulator into the external transistor, input the output voltage into the regulator.



VCC

O VDD=3.3 V

Regulator

controller

#### (6) Setting the Soft Start Time

Soft start is required to prevent the coil current at the time of start from increasing and the overshoot of the output voltage at the starting time. The relation between the capacity and soft start time is shown in the following figure. Refer to the figure and set capacity C1.Soft start is required to prevent the coil current at the time of start from increasing and the overshoot of the output voltage at the starting time. Fig. 34 shows the relation between the capacitance and soft start time. Please refer to it to set the capacitance.

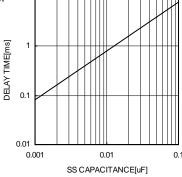


Fig. 34 SS Pin Capacitance vs Delay Time

As the capacitance,  $0.001\mu F$  to  $0.1\mu F$  is recommended. If the capacitance is set lower than  $0.001\mu F$ , the overshooting may occur on the output voltage. If the capacitance is set larger than  $0.1\mu F$ , the excessive back current flow may occur in the internal parasitic elements when the power is turned OFF and it may damage IC. When there is the activation relation (sequences) with other power supplies, be sure to use the high accuracy product (such as X5R).

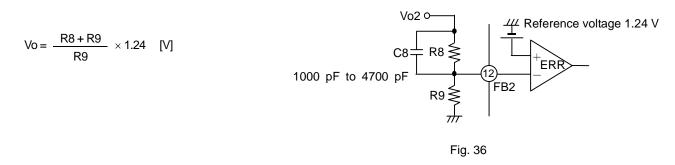
Soft start time may vary according to the input voltage, loads, coils and output capacity. Be sure to verify the operation using the actual product.

#### (7) Design of the Feedback Resistor Constant

Refer to the following equation to set the feedback resistor. As the setting range, 10 k $\Omega$  to 330 k $\Omega$  is recommended. If the resistor is set lower than a 10 k $\Omega$ , it causes the reduction of power efficiency. If it is set more than 330 k $\Omega$ , the offset voltage becomes larger by the input bias current 0.4  $\mu$ A(Typ.) in the internal error amplifier.

#### (8) Positive-side Charge Pump Settings

BU8513EFV incorporates a charge pump controller, thus making it possible to generate stable gate voltage. The output voltage is determined by the following formula. As the setting range,  $10~k\Omega$  to  $330~k\Omega$  is recommended. If the resistor is set lower than a  $10k\Omega$ , it causes the reduction of power efficiency. If it is set more than  $330~k\Omega$ , the offset voltage becomes larger by the input bias current  $0.4~\mu\text{A}$  (Typ.) in the internal error amp.



In order to prevent output voltage overshooting, add capacitor C8 in parallel with R8. The recommended capacitance is 1000 pF to 4700 pF. If a capacitor outside this range is inserted, the output voltage may oscillate. By connecting capacitance to the DLS, a rising delay time can be set for the positive-side charge pump. The delay time is determined by the following formula.

• Delay time of charge pump block t DELAY t DELAY = ( CDLS  $\times$  0.6 )/5  $\mu$ A [s6] where, CDLS is the external capacitance.

## (9) Negative-side Charge Pump Settings

BU8513EFV incorporates a charge pump controller for negative voltage, thus making it possible to generate stable gate voltage. The output voltage is determined by the following formula. As the setting range,  $10~\text{k}\Omega$  to  $330~\text{k}\Omega$  is recommended. If the resistor is set lower than a  $10~\text{k}\Omega$ , it causes the reduction of power efficiency. If it is set more than  $330~\text{k}\Omega$ , the offset voltage becomes larger by the input bias current  $0.4~\text{\mu}A$  (Typ.) in the internal error amp.

Vo3 = 
$$-\frac{R6}{R7} \times 1.04 + 0.2 \text{ V}$$
 [V] 1000 pF to 4700 pF  $\frac{\sqrt{03} \circ \sqrt{0.2} \circ \sqrt{$ 

The delay time is internally fixed at 200 us.

In order to prevent output voltage overshooting, insert capacitor C6 in parallel with R6. The recommended capacitance is 1000 pF to 4700 pF. If a capacitor outside this range is inserted, the output voltage may oscillate.

#### ● Gate Shading Setting Method

The IG input signal allows the high-level and low-level control of the positive-side gate voltage. The slope of output can be set by the external RC. The recommended resistance set value is  $200~\Omega$  to  $5.1~\text{k}\Omega$  and the recommended capacitor set value is  $0.001~\mu\text{F}$  to  $0.1~\mu\text{F}$ . The aggravation of efficiency may be caused if settings outside this range are made. Determine  $\Delta V$  by referring to the following value. The following calculation formula is used for  $\Delta V$ .

$$\Delta V = Vo2GS \quad (1 - exp( - \frac{tWL}{CR})) \quad [V]$$

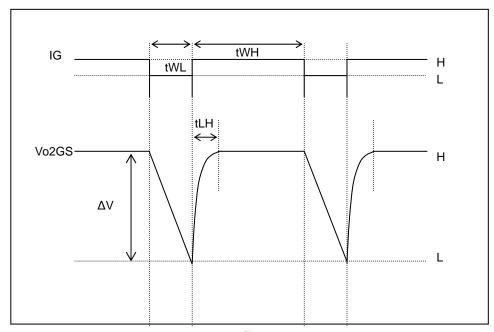
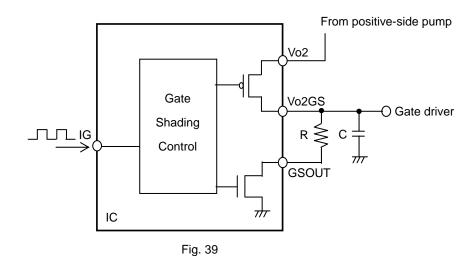


Fig. 38

PARAMETER	SYMBOL	LIMIT			UNIT	CONDITION	
PARAMETER	STIVIBUL	MIN	TYP	MAX	UNIT	CONDITION	
IG "L" Time	tWL	1	2	-	μs	-	
IG "H" Time	tWH	1	18	-	μs	-	
Vo2GS "H" to "L Voltage difference	ΔV		10	-	V	TWL = 2 $\mu s$ ,R = 500 $\Omega$ *	
Vo2GS "L" to "H" Time	tLH	-	0.1	-	μs	ΔV = 10 V *	

TIMING STANDARD VALUE

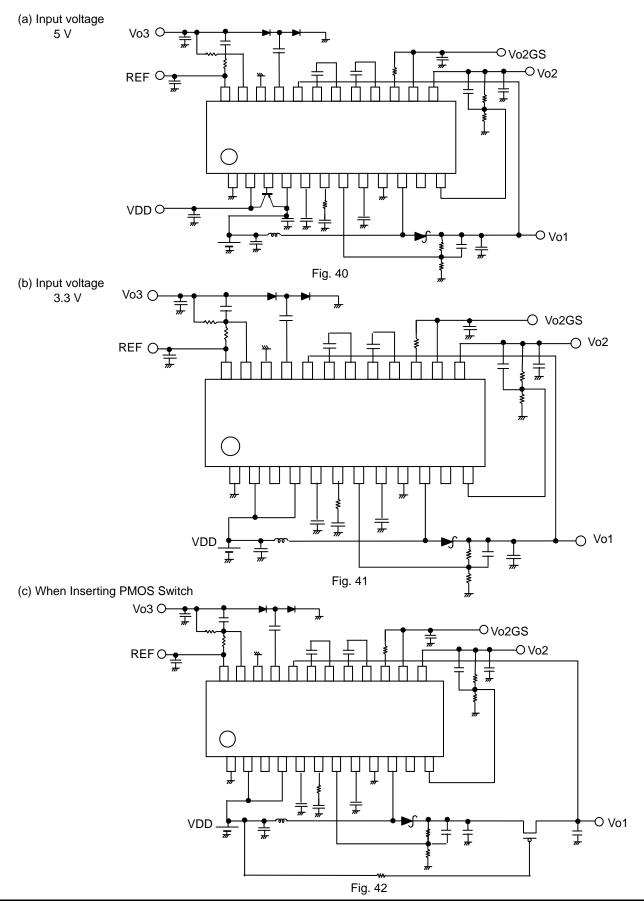


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#### Application Examples

\*Although we are confident that the application circuit diagram reflects the best possible recommendations, be sure to verify circuit characteristics for your particular application.

When a circuit is used modifying the externally connected circuit constant, be sure to decide allowing sufficient margins considering the dispersion of values by external parts as well as our IC including not only the static but also the transient characteristic. For the patent, we have not acquired the sufficient confirmation. Please acknowledge the status.



●I/O Equivalent Circuits

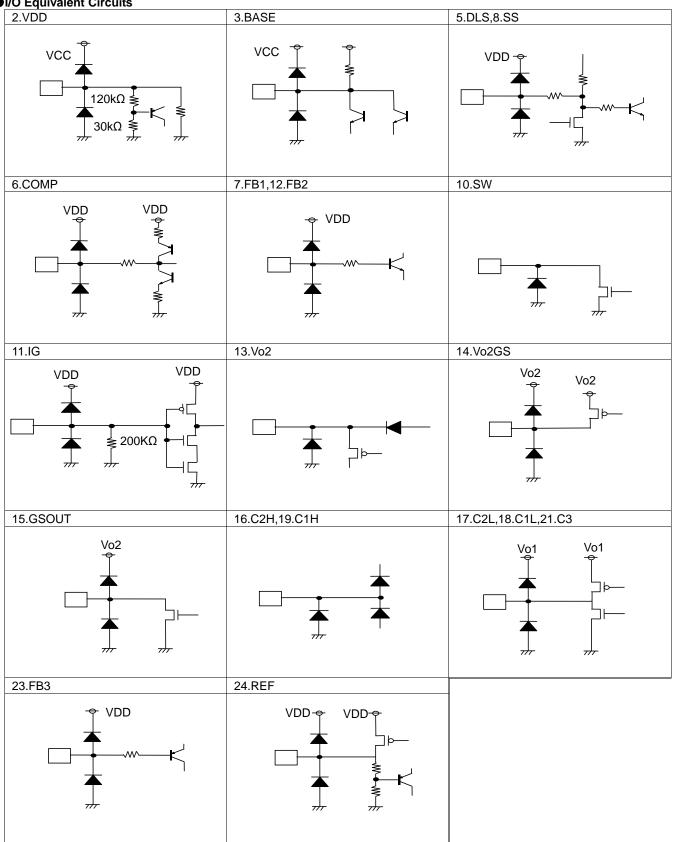


Fig.43

#### Operation Notes

#### 1) Absolute maximum ratings

Use of the IC in excess of absolute maximum ratings such as the applied voltage or operating temperature range may result in IC damage. Assumptions should not be made regarding the state of the IC (short mode or open mode) when such damage is suffered. A physical safety measure such as a fuse should be implemented when use of the IC in a special mode where the absolute maximum ratings may be exceeded is anticipated.

#### 2) GND potential

Ensure a minimum GND pin potential in all operating conditions.

#### 3) Setting of heat

Use a thermal design that allows for a sufficient margin in light of the power dissipation (Pd) in actual operating conditions.

#### 4) Pin short and mistake fitting

Use caution when orienting and positioning the IC for mounting on printed circuit boards. Improper mounting may result in damage to the IC. Shorts between output pins or between output pins and the power supply and GND pins caused by the presence of a foreign object may result in damage to the IC.

#### 5) Actions in strong magnetic field

Use caution when using the IC in the presence of a strong magnetic field as doing so may cause the IC to malfunction.

#### 6) Testing on application boards

When testing the IC on an application board, connecting a capacitor to a pin with low impedance subjects the IC to stress. Always discharge capacitors after each process or step. Ground the IC during assembly steps as an antistatic measure, and use similar caution when transporting or storing the IC. Always turn the IC's power supply off before connecting it to or removing it from a jig or fixture during the inspection process.

#### 7) Ground wiring patterns

When using both small signal and large current GND patterns, it is recommended to isolate the two ground patterns, placing a single ground point at the application's reference point so that the pattern wiring resistance and voltage variations caused by large currents do not cause variations in the small signal ground voltage. Be careful not to change the GND wiring patterns of any external components.

8) This monolithic IC contains P+ isolation and P substrate layers between adjacent elements in order to keep them isolated. P/N junctions are formed at the intersection of these P layers with the N layers of other elements to create a variety of parasitic elements.

For example, when the resistors and transistors are connected to the pins as shown in Fig. 44, a parasitic diode or a transistor operates by inversing the pin voltage and GND voltage.

The formation of parasitic elements as a result of the relationships of the potentials of different pins is an inevitable result of the IC's architecture. The operation of parasitic elements can cause interference with circuit operation as well as IC malfunction and damage. For these reasons, it is necessary to use caution so that the IC is not used in a way that will trigger the operation of parasitic elements, such as the application of voltages lower than the GND (P board) voltage to input and output pins.

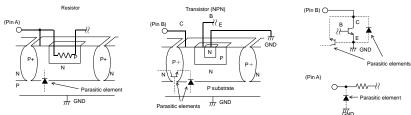


Fig.44 Example of a Simple Monolithic IC Architecture

#### 9) Overcurrent protection circuits

An over current protection circuit designed according to the output current is incorporated for the prevention of IC destruction that may result in the event of load shorting. This protection circuit is effective in preventing damage due to sudden and unexpected accidents. However, the IC should not be used in applications characterized by the continuous operation or transitioning of the protection circuits. At the time of thermal designing, keep in mind that the current capability has negative characteristics to temperatures.

#### 10) Thermal shutdown circuit

This IC incorporates a built-in thermal shutdown circuit for the protection from thermal destruction. The IC should be used within the specified power dissipation range. However, in the event that the IC continues to be operated in excess of its power dissipation limits, the attendant rise in the chip's temperature Tj will trigger the thermal shutdown circuit to turn off all output power elements. The circuit automatically resets once the chip's temperature Tj drops.

Operation of the thermal shutdown circuit presumes that the IC's absolute maximum ratings have been exceeded. Application designs should never make use of the thermal shutdown circuit.

#### 11) Testing on application boards

At the time of inspection of the installation boards, when the capacitor is connected to the pin with low impedance, be sure to discharge electricity per process because it may load stresses to the IC. Always turn the IC's power supply off before connecting it to or removing it from a jig or fixture during the inspection process. Ground the IC during assembly steps as an antistatic measure, and use similar caution when transporting or storing the IC.

#### Power Dissipation Reduction

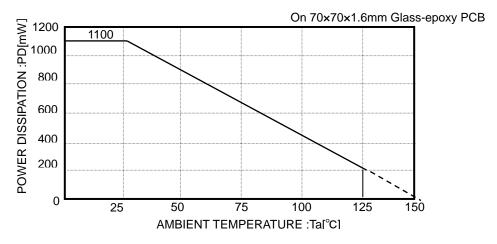
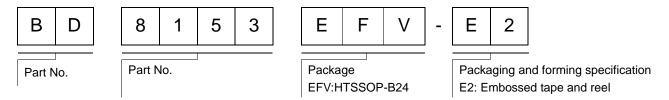
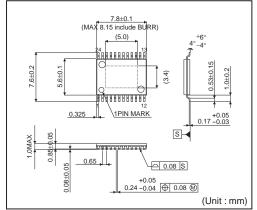


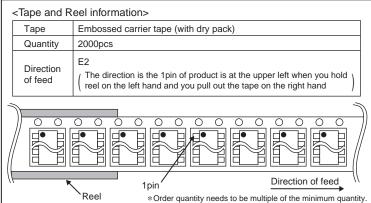
Fig.45

# Ordering part number



# HTSSOP-B24





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  - [d] Use of our Products in places where the Products are exposed to static electricity or electromagnetic waves
  - [e] Use of our Products in proximity to heat-producing components, plastic cords, or other flammable items
  - [f] Sealing or coating our Products with resin or other coating materials
  - [g] Use of our Products without cleaning residue of flux (even if you use no-clean type fluxes, cleaning residue of flux is recommended); or Washing our Products by using water or water-soluble cleaning agents for cleaning residue after soldering
  - [h] Use of the Products in places subject to dew condensation
- 4. The Products are not subject to radiation-proof design.
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- 6. In particular, if a transient load (a large amount of load applied in a short period of time, such as pulse. is applied, confirmation of performance characteristics after on-board mounting is strongly recommended. Avoid applying power exceeding normal rated power; exceeding the power rating under steady-state loading condition may negatively affect product performance and reliability.
- 7. De-rate Power Dissipation (Pd) depending on Ambient temperature (Ta). When used in sealed area, confirm the actual ambient temperature.
- 8. Confirm that operation temperature is within the specified range described in the product specification.
- 9. ROHM shall not be in any way responsible or liable for failure induced under deviant condition from what is defined in this document.

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- 2. In principle, the reflow soldering method must be used; if flow soldering method is preferred, please consult with the ROHM representative in advance.

For details, please refer to ROHM Mounting specification

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This Product is electrostatic sensitive product, which may be damaged due to electrostatic discharge. Please take proper caution in your manufacturing process and storage so that voltage exceeding the Products maximum rating will not be applied to Products. Please take special care under dry condition (e.g. Grounding of human body / equipment / solder iron, isolation from charged objects, setting of lonizer, friction prevention and temperature / humidity control).

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**Телефон:** 8 (812) 309 58 32 (многоканальный)

Факс: 8 (812) 320-02-42

Электронная почта: org@eplast1.ru

Адрес: 198099, г. Санкт-Петербург, ул. Калинина,

дом 2, корпус 4, литера А.