

# Linear Optocoupler, High Gain Stability, Wide Bandwidth



1179026



## FEATURES

- Couples AC and DC signals
- 0.01 % servo linearity
- Wide bandwidth, > 200 kHz
- High gain stability,  $\pm 0.005 \%/^{\circ}\text{C}$  typically
- Low input-output capacitance
- Low power consumption, < 15 mW
- Isolation test voltage, 5300 V<sub>RMS</sub>, 1 s
- Internal insulation distance, > 0.4 mm
- Compliant to RoHS Directive 2002/95/EC and in accordance to WEEE 2002/96/EC



RoHS COMPLIANT

## DESCRIPTION

The IL300 linear optocoupler consists of an AlGaAs IRLED irradiating an isolated feedback and an output PIN photodiode in a bifurcated arrangement. The feedback photodiode captures a percentage of the LEDs flux and generates a control signal ( $I_{P1}$ ) that can be used to servo the LED drive current. This technique compensates for the LED's non-linear, time, and temperature characteristics. The output PIN photodiode produces an output signal ( $I_{P2}$ ) that is linearly related to the servo optical flux created by the LED.

The time and temperature stability of the input-output coupler gain ( $K3$ ) is insured by using matched PIN photodiodes that accurately track the output flux of the LED.

## APPLICATIONS

- Power supply feedback voltage/current
- Medical sensor isolation
- Audio signal interfacing
- Isolated process control transducers
- Digital telephone isolation

## AGENCY APPROVALS

- UL file no. E52744, system code H
- DIN EN 60747-5-2 (VDE 0884)
- DIN EN 60747-5-5 (pending) available with option 1
- BSI
- FIMKO

| ORDERING INFORMATION  |                            |                                 |  |                |                               |  |                |                              |   |  |
|---|----------------------------|---------------------------------|--|----------------|-------------------------------|--|----------------|------------------------------|---|--|
| <div style="display: flex; justify-content: space-around; border: 1px solid black; padding: 2px;"> <span>I</span><span>L</span><span>3</span><span>0</span><span>0</span> </div> <p>PART NUMBER</p> |                            |                                 | <div style="display: flex; justify-content: space-around; border: 1px solid black; padding: 2px;"> <span>D</span><span>E</span><span>F</span><span>G</span> </div> <p>K3 BIN</p> |                |                               | <div style="display: flex; justify-content: space-around; border: 1px solid black; padding: 2px;"> <span>X</span><span>0</span><span>#</span><span>#</span> </div> <p>PACKAGE OPTION</p> |                |                              | <div style="display: flex; justify-content: space-around; border: 1px solid black; padding: 2px;"> <span>T</span> </div> <p>TAPE AND REEL</p> |  |
| AGENCY CERTIFIED/PACKAGE  |                            | K3 BIN                          |  |                |                               |  |                |                              |   |  |
| UL, cUL, BSI, FIMKO   | 0.557 to 1.618             | 0.765 to 1.181                  | 0.851 to 1.181   | 0.765 to 0.955 | 0.851 to 1.061                | 0.945 to 1.181   | 0.851 to 0.955 | 0.945 to 1.061               |   |  |
| DIP-8   | IL300                      | IL300-DEFG                      | -  | -              | IL300-EF                      | -  | IL300-E        | IL300-F                      |   |  |
| DIP-8, 400 mil, option 6  | IL300-X006                 | IL300-DEFG-X006                 | -  | -              | IL300-EF-X006                 | IL300-FG-X006  | IL300-E-X006   | IL300-F-X006                 |   |  |
| SMD-8, option 7   | IL300-X007T <sup>(1)</sup> | IL300-DEFG-X007T <sup>(1)</sup> | IL300-EFG-X007   | IL300-DE-X007T | IL300-EF-X007T <sup>(1)</sup> | -  | IL300-E-X007T  | IL300-F-X007                 |   |  |
| SMD-8, option 9   | IL300-X009T <sup>(1)</sup> | IL300-DEFG-X009T <sup>(1)</sup> | -  | -              | IL300-EF-X009T <sup>(1)</sup> | -  | -              | IL300-F-X009T <sup>(1)</sup> |   |  |
| VDE, UL   | 0.557 to 1.618             | 0.765 to 1.181                  | 0.851 to 1.181   | 0.765 to 0.955 | 0.851 to 1.061                | 0.945 to 1.181   | 0.851 to 0.955 | 0.945 to 1.061               |   |  |
| DIP-8   | IL300-X001                 | IL300-DEFG-X001                 | -  | -              | IL300-EF-X001                 | -  | IL300-E-X001   | IL300-F-X001                 |   |  |
| DIP-8, 400 mil, option 6  | IL300-X016                 | IL300-DEFG-X016                 | -  | -              | IL300-EF-X016                 | -  | -              | IL300-F-X016                 |   |  |
| SMD-8, option 7   | IL300-X017                 | IL300-DEFG-X017T <sup>(1)</sup> | -  | -              | IL300-EF-X017T <sup>(1)</sup> | -  | IL300-E-X017T  | IL300-F-X017T <sup>(1)</sup> |   |  |
| SMD-8, option 9   | -                          | -                               | -  | -              | -                             | -  | -              | IL300-F-X019T <sup>(1)</sup> |   |  |



### Note

<sup>(1)</sup> Also available in tubes, do not put "T" on the end.





| <b>ABSOLUTE MAXIMUM RATINGS</b> ( $T_{amb} = 25\text{ }^{\circ}\text{C}$ , unless otherwise specified) |  |            |               |           |
|--|--|------------|---------------|-----------|
| PARAMETER  | TEST CONDITION   | SYMBOL     | VALUE         | UNIT      |
| <b>INPUT</b>   |  |            |               |           |
| Power dissipation  |  | $P_{diss}$ | 160           | mW        |
| Derate linearly from 25 °C   |  |            | 2.13          | mW/°C     |
| Forward current  |  | $I_F$      | 60            | mA        |
| Surge current (pulse width < 10 μs)  |  | $I_{PK}$   | 250           | mA        |
| Reverse voltage  |  | $V_R$      | 5             | V         |
| Thermal resistance   |  | $R_{th}$   | 470           | K/W       |
| Junction temperature   |  | $T_j$      | 100           | °C        |
| <b>OUTPUT</b>  |  |            |               |           |
| Power dissipation  |  | $P_{diss}$ | 50            | mW        |
| Derate linearly from 25 °C   |  |            | 0.65          | mW/°C     |
| Reverse voltage  |  | $V_R$      | 50            | V         |
| Thermal resistance   |  | $R_{th}$   | 1500          | K/W       |
| Junction temperature   |  | $T_j$      | 100           | °C        |
| <b>COUPLER</b>   |  |            |               |           |
| Total package dissipation at 25 °C   |  | $P_{tot}$  | 210           | mW        |
| Derate linearly from 25 °C   |  |            | 2.8           | mW/°C     |
| Storage temperature  |  | $T_{stg}$  | - 55 to + 150 | °C        |
| Operating temperature  |  | $T_{amb}$  | - 55 to + 100 | °C        |
| Isolation test voltage   |  | $V_{ISO}$  | > 5300        | $V_{RMS}$ |
| Isolation resistance   | $V_{IO} = 500\text{ V}, T_{amb} = 25\text{ }^{\circ}\text{C}$  | $R_{IO}$   | > $10^{12}$   | $\Omega$  |
|  | $V_{IO} = 500\text{ V}, T_{amb} = 100\text{ }^{\circ}\text{C}$ | $R_{IO}$   | > $10^{11}$   | $\Omega$  |

**Note**

- Stresses in excess of the absolute maximum ratings can cause permanent damage to the device. Functional operation of the device is not implied at these or any other conditions in excess of those given in the operational sections of this document. Exposure to absolute maximum ratings for extended periods of the time can adversely affect reliability.

| <b>ELECTRICAL CHARACTERISTICS</b> ( $T_{amb} = 25\text{ }^{\circ}\text{C}$ , unless otherwise specified) |   |                                       |        |                     |       |          |
|--|---|---------------------------------------|--------|---------------------|-------|----------|
| PARAMETER  | TEST CONDITION                                | SYMBOL                                | MIN.   | TYP.                | MAX.  | UNIT     |
| <b>INPUT (LED EMITTER)</b>   |   |                                       |        |                     |       |          |
| Forward voltage  | $I_F = 10\text{ mA}$                          | $V_F$                                 |        | 1.25                | 1.50  | V        |
| $V_F$ temperature coefficient  |   | $\Delta V_F / \Delta^{\circ}\text{C}$ |        | - 2.2               |       | mV/°C    |
| Reverse current  | $V_R = 5\text{ V}$                            | $I_R$                                 |        | 1                   |       | μA       |
| Junction capacitance   | $V_F = 0\text{ V}, f = 1\text{ MHz}$          | $C_j$                                 |        | 15                  |       | pF       |
| Dynamic resistance   | $I_F = 10\text{ mA}$                          | $\Delta V_F / \Delta I_F$             |        | 6                   |       | $\Omega$ |
| <b>OUTPUT</b>  |   |                                       |        |                     |       |          |
| Dark current   | $V_{det} = - 15\text{ V}, I_F = 0\text{ A}$   | $I_D$                                 |        | 1                   | 25    | nA       |
| Open circuit voltage   | $I_F = 10\text{ mA}$                          | $V_D$                                 |        | 500                 |       | mV       |
| Short circuit current  | $I_F = 10\text{ mA}$                          | $I_{SC}$                              |        | 70                  |       | μA       |
| Junction capacitance   | $V_F = 0\text{ V}, f = 1\text{ MHz}$          | $C_j$                                 |        | 12                  |       | pF       |
| Noise equivalent power   | $V_{det} = 15\text{ V}$                       | NEP                                   |        | $4 \times 10^{-14}$ |       | W/√Hz    |
| <b>COUPLER</b>   |   |                                       |        |                     |       |          |
| Input-output capacitance   | $V_F = 0\text{ V}, f = 1\text{ MHz}$          |                                       |        | 1                   |       | pF       |
| K1, servo gain ( $I_{P1}/I_F$ )  | $I_F = 10\text{ mA}, V_{det} = - 15\text{ V}$ | K1                                    | 0.0050 | 0.007               | 0.011 |          |
| Servo current <sup>(1)(2)</sup>  | $I_F = 10\text{ mA}, V_{det} = - 15\text{ V}$ | $I_{P1}$                              |        | 70                  |       | μA       |
| K2, forward gain ( $I_{P2}/I_F$ )  | $I_F = 10\text{ mA}, V_{det} = - 15\text{ V}$ | K2                                    | 0.0036 | 0.007               | 0.011 |          |
| Forward current  | $I_F = 10\text{ mA}, V_{det} = - 15\text{ V}$ | $I_{P2}$                              |        | 70                  |       | μA       |
| K3, transfer gain ( $K2/K1$ ) <sup>(1)(2)</sup>  | $I_F = 10\text{ mA}, V_{det} = - 15\text{ V}$ | K3                                    | 0.56   | 1                   | 1.65  | K2/K1    |



| <b>ELECTRICAL CHARACTERISTICS</b> ( $T_{amb} = 25\text{ }^{\circ}\text{C}$ , unless otherwise specified) |  |                        |      |             |            |                       |
|--|--|------------------------|------|-------------|------------|-----------------------|
| PARAMETER  | TEST CONDITION   | SYMBOL                 | MIN. | TYP.        | MAX.       | UNIT                  |
| <b>COUPLER</b>   |  |                        |      |             |            |                       |
| Transfer gain stability  | $I_F = 10\text{ mA}$ , $V_{det} = -15\text{ V}$  | $\Delta K3/\Delta T_A$ |      | $\pm 0.005$ | $\pm 0.05$ | $\%/^{\circ}\text{C}$ |
| Transfer gain linearity  | $I_F = 1\text{ mA to }10\text{ mA}$  | $\Delta K3$            |      | $\pm 0.25$  |            | %                     |
|  | $I_F = 1\text{ mA to }10\text{ mA}$ ,<br>$T_{amb} = 0\text{ }^{\circ}\text{C to }75\text{ }^{\circ}\text{C}$ |                        |      | $\pm 0.5$   |            | %                     |
| <b>PHOTOCONDUCTIVE OPERATION</b>   |  |                        |      |             |            |                       |
| Frequency response   | $I_{Fq} = 10\text{ mA}$ , $MOD = \pm 4\text{ mA}$ ,<br>$R_L = 50\text{ }\Omega$                              | BW (-3 db)             |      | 200         |            | kHz                   |
| Phase response at 200 kHz  | $V_{det} = -15\text{ V}$   |                        |      | -45         |            | Deg.                  |

**Notes**

- Minimum and maximum values were tested requirements. Typical values are characteristics of the device and are the result of engineering evaluation. Typical values are for information only and are not part of the testing requirements.
- (1) Bin sorting:  
K3 (transfer gain) is sorted into bins that are  $\pm 6\%$ , as follows:  
Bin A = 0.557 to 0.626  
Bin B = 0.620 to 0.696  
Bin C = 0.690 to 0.773  
Bin D = 0.765 to 0.859  
Bin E = 0.851 to 0.955  
Bin F = 0.945 to 1.061  
Bin G = 1.051 to 1.181  
Bin H = 1.169 to 1.311  
Bin I = 1.297 to 1.456  
Bin J = 1.442 to 1.618  
K3 = K2/K1. K3 is tested at  $I_F = 10\text{ mA}$ ,  $V_{det} = -15\text{ V}$ .
- (2) Bin categories: All IL300s are sorted into a K3 bin, indicated by an alpha character that is marked on the part. The bins range from "A" through "J".  
The IL300 is shipped in tubes of 50 each. Each tube contains only one category of K3. The category of the parts in the tube is marked on the tube label as well as on each individual part.
- (3) Category options: standard IL300 orders will be shipped from the categories that are available at the time of the order. Any of the ten categories may be shipped. For customers requiring a narrower selection of bins, the bins can be grouped together as follows:  
IL300-DEFG: order this part number to receive categories D, E, F, G only.  
IL300-EF: order this part number to receive categories E, F only.  
IL300-E: order this part number to receive category E only.

| <b>SWITCHING CHARACTERISTICS</b> |  |        |      |      |      |               |
|----------------------------------|--|--------|------|------|------|---------------|
| PARAMETER                        | TEST CONDITION                                       | SYMBOL | MIN. | TYP. | MAX. | UNIT          |
| Switching time                   | $\Delta I_F = 2\text{ mA}$ , $I_{Fq} = 10\text{ mA}$ | $t_r$  |      | 1    |      | $\mu\text{s}$ |
|                                  |  | $t_f$  |      | 1    |      | $\mu\text{s}$ |
| Rise time                        |  | $t_r$  |      | 1.75 |      | $\mu\text{s}$ |
| Fall time                        |  | $t_f$  |      | 1.75 |      | $\mu\text{s}$ |

| <b>COMMON MODE TRANSIENT IMMUNITY</b> |   |          |      |      |      |      |
|---------------------------------------|---|----------|------|------|------|------|
| PARAMETER                             | TEST CONDITION                                  | SYMBOL   | MIN. | TYP. | MAX. | UNIT |
| Common mode capacitance               | $V_F = 0\text{ V}$ , $f = 1\text{ MHz}$         | $C_{CM}$ |      | 0.5  |      | pF   |
| Common mode rejection ratio           | $f = 60\text{ Hz}$ , $R_L = 2.2\text{ k}\Omega$ | CMRR     |      | 130  |      | dB   |

**TYPICAL CHARACTERISTICS** ( $T_{amb} = 25\text{ }^{\circ}\text{C}$ , unless otherwise specified)


Fig. 2 - LED Forward Current vs. Forward Voltage



Fig. 5 - Servo Gain vs. LED Current and Temperature



Fig. 3 - Servo Photocurrent vs. LED Current and Temperature



Fig. 6 - Normalized Transfer Gain vs. LED Current and Temperature



Fig. 4 - Normalized Servo Photocurrent vs. LED Current and Temperature



Fig. 7 - Amplitude Response vs. Frequency



Fig. 8 - Amplitude and Phase Response vs. Frequency



Fig. 9 - Common-Mode Rejection



Fig. 10 - Photodiode Junction Capacitance vs. Reverse Voltage

### APPLICATION CONSIDERATIONS

In applications such as monitoring the output voltage from a line powered switch mode power supply, measuring bioelectric signals, interfacing to industrial transducers, or making floating current measurements, a galvanically isolated, DC coupled interface is often essential. The IL300 can be used to construct an amplifier that will meet these needs.

The IL300 eliminates the problems of gain nonlinearity and drift induced by time and temperature, by monitoring LED output flux.

A pin photodiode on the input side is optically coupled to the LED and produces a current directly proportional to flux falling on it. This photocurrent, when coupled to an amplifier, provides the servo signal that controls the LED drive current.

The LED flux is also coupled to an output PIN photodiode. The output photodiode current can be directly or amplified to satisfy the needs of succeeding circuits.

### ISOLATED FEEDBACK AMPLIFIER

The IL300 was designed to be the central element of DC coupled isolation amplifiers. Designing the IL300 into an amplifier that provides a feedback control signal for a line powered switch mode power is quite simple, as the following example will illustrate.

See figure 12 for the basic structure of the switch mode supply using the Infineon TDA4918 push-pull switched power supply control cChip. Line isolation are provided by the high frequency transformer. The voltage monitor isolation will be provided by the IL300.

The isolated amplifier provides the PWM control signal which is derived from the output supply voltage. Figure 13 more closely shows the basic function of the amplifier.

The control amplifier consists of a voltage divider and a non-inverting unity gain stage. The TDA4918 data sheet indicates that an input to the control amplifier is a high quality operational amplifier that typically requires a + 3 V signal. Given this information, the amplifier circuit topology shown in figure 14 is selected.

The power supply voltage is scaled by R1 and R2 so that there is + 3 V at the non-inverting input ( $V_a$ ) of U1. This voltage is offset by the voltage developed by photocurrent flowing through R3. This photocurrent is developed by the optical flux created by current flowing through the LED. Thus as the scaled monitor voltage ( $V_a$ ) varies it will cause a change in the LED current necessary to satisfy the differential voltage needed across R3 at the inverting input. The first step in the design procedure is to select the value of R3 given the LED quiescent current ( $I_{Fq}$ ) and the servo gain (K1). For this design,  $I_{Fq} = 12$  mA. Figure 4 shows the servo photocurrent at  $I_{Fq}$  is found to be 100  $\mu$ A. With this data R3 can be calculated.

$$R3 = \frac{V_b}{I_{p1}} = \frac{3 \text{ V}}{100 \mu\text{A}} = 30 \text{ k}\Omega$$



iii300\_16

Fig. 11 - Isolated Control Amplifier

For best input offset compensation at U1, R2 will equal R3. The value of R1 can easily be calculated from the following.

$$R1 = R2 \times \left( \frac{V_{MONITOR}}{V_a} - 1 \right)$$

The value of R5 depends upon the IL300 Transfer Gain (K3). K3 is targeted to be a unit gain device, however to minimize the part to part Transfer Gain variation, Infineon offers K3 graded into  $\pm 5\%$  bins. R5 can be determined using the following equation,

$$R5 = \frac{V_{OUT}}{V_{MONITOR}} \times \frac{R3 \times (R1 + R2)}{R2 \times K3}$$

or if a unity gain amplifier is being designed ( $V_{MONITOR} = V_{OUT}$ ,  $R1 = 0$ ), the equation simplifies to:

$$R5 = \frac{R3}{K3}$$



iii300\_17

Fig. 12 - Switching Mode Power Supply



iii300\_18

Fig. 13 - DC Coupled Power Supply Feedback Amplifier

Table 1. Gives the value of R5 given the production K3 bin.

| TABLE 1 - R5 SELECTION |       |       |      |             |
|------------------------|-------|-------|------|-------------|
| BIN                    | K3    |       |      | R5 RESISTOR |
|                        | MIN.  | MAX.  | TYP. | 1 % kΩ      |
| A                      | 0.560 | 0.623 | 0.59 | 51.1        |
| B                      | 0.623 | 0.693 | 0.66 | 45.3        |
| C                      | 0.693 | 0.769 | 0.73 | 41.2        |
| D                      | 0.769 | 0.855 | 0.81 | 37.4        |
| E                      | 0.855 | 0.950 | 0.93 | 32.4        |
| F                      | 0.950 | 1.056 | 1    | 30          |
| G                      | 1.056 | 1.175 | 1.11 | 27          |
| H                      | 1.175 | 1.304 | 1.24 | 24          |
| I                      | 1.304 | 1.449 | 1.37 | 22          |
| J                      | 1.449 | 1.610 | 1.53 | 19.4        |

The last step in the design is selecting the LED current limiting resistor (R4). The output of the operational amplifier is targeted to be 50 % of the  $V_{CC}$ , or 2.5 V. With an LED quiescent current of 12 mA the typical LED ( $V_F$ ) is 1.3 V. Given this and the operational output voltage, R4 can be calculated.

$$R4 = \frac{V_{opamp} - V_F}{I_{Fq}} = \frac{2.5 \text{ V} - 1.3 \text{ V}}{12 \text{ mA}} = 100 \Omega$$

The circuit was constructed with an LM201 differential operational amplifier using the resistors selected. The amplifier was compensated with a 100 pF capacitor connected between pins 1 and 8.

The DC transfer characteristics are shown in figure 17. The amplifier was designed to have a gain of 0.6 and was measured to be 0.6036. Greater accuracy can be achieved by adding a balancing circuit, and potentiometer in the input divider, or at R5. The circuit shows exceptionally good gain linearity with an RMS error of only 0.0133 % over the input voltage range of 4 V to 6 V in a servo mode; see figure 15.



Fig. 14 - Transfer Gain



Fig. 15 - Linearity Error vs. Input Voltage

The AC characteristics are also quite impressive offering a - 3 dB bandwidth of 100 kHz, with a - 45° phase shift at 80 kHz as shown in figure 16.





Fig. 16 - Amplitude and Phase Power Supply Control

The same procedure can be used to design isolation amplifiers that accept bipolar signals referenced to ground. These amplifiers circuit configurations are shown in figure 17. In order for the amplifier to respond to a signal that swings above and below ground, the LED must be pre biased from a separate source by using a voltage reference source ( $V_{ref1}$ ). In these designs, R3 can be determined by the following equation.

$$R3 = \frac{V_{ref1}}{I_{P1}} = \frac{V_{ref1}}{K1I_{Fq}}$$



Fig. 17 - Non-inverting and Inverting Amplifiers

| TABLE 2 - OPTOLINEAR AMPLIFIERS |               |               |   |  |
|---------------------------------|---------------|---------------|---|--|
| AMPLIFIER                       | INPUT         | OUTPUT        | GAIN  | OFFSET   |
| Non-inverting                   | Inverting     | Inverting     | $\frac{V_{OUT}}{V_{IN}} = \frac{K3 \times R4 \times R2}{R3 \times (R1 \times R2)}$                            | $V_{ref2} = \frac{V_{ref1} \times R4 \times K3}{R3}$                             |
|                                 | Non-inverting | Non-inverting | $\frac{V_{OUT}}{V_{IN}} = \frac{K3 \times R4 \times R2 \times (R5 + R6)}{R3 \times R5 \times (R1 \times R2)}$ | $V_{ref2} = \frac{-V_{ref1} \times R4 \times (R5 + R6) \times K3}{R3 \times R6}$ |
| Inverting                       | Inverting     | Non-inverting | $\frac{V_{OUT}}{V_{IN}} = \frac{-K3 \times R4 \times R2 \times (R5 + R6)}{R3 \times (R1 \times R2)}$          | $V_{ref2} = \frac{V_{ref1} \times R4 \times (R5 + R6) \times K3}{R3 \times R6}$  |
|                                 | Non-inverting | Inverting     | $\frac{V_{OUT}}{V_{IN}} = \frac{-K3 \times R4 \times R2}{R3 \times (R1 \times R2)}$                           | $V_{ref2} = \frac{-V_{ref1} \times R4 \times K3}{R3}$                            |

These amplifiers provide either an inverting or non-inverting transfer gain based upon the type of input and output amplifier. Table 2 shows the various configurations along with the specific transfer gain equations. The offset column refers to the calculation of the output offset or  $V_{ref2}$  necessary to provide a zero voltage output for a zero voltage input. The non-inverting input amplifier requires the use of a bipolar supply, while the inverting input stage can be implemented with single supply operational amplifiers that permit operation close to ground.

For best results, place a buffer transistor between the LED and output of the operational amplifier when a CMOS opamp is used or the LED  $I_{Fq}$  drive is targeted to operate beyond 15 mA. Finally the bandwidth is influenced by the magnitude of the closed loop gain of the input and output amplifiers. Best bandwidths result when the amplifier gain is designed for unity.

**PACKAGE DIMENSIONS** in millimeters



**PACKAGE MARKING** (this is an example of the IL300-E-X001)





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**Please note that some Vishay documentation may still make reference to RoHS Directive 2002/95/EC. We confirm that all the products identified as being compliant to Directive 2002/95/EC conform to Directive 2011/65/EU.**

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Компания «ЭлектроПласт» предлагает заключение долгосрочных отношений при поставках импортных электронных компонентов на взаимовыгодных условиях!

Наши преимущества:

- Оперативные поставки широкого спектра электронных компонентов отечественного и импортного производства напрямую от производителей и с крупнейших мировых складов;
- Поставка более 17-ти миллионов наименований электронных компонентов;
- Поставка сложных, дефицитных, либо снятых с производства позиций;
- Оперативные сроки поставки под заказ (от 5 рабочих дней);
- Экспресс доставка в любую точку России;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- Лицензия ФСБ на осуществление работ с использованием сведений, составляющих государственную тайну;
- Поставка специализированных компонентов (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Aeroflex, Peregrine, Syfer, Eurofarad, Texas Instrument, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits, General Dynamics и др.);

Помимо этого, одним из направлений компании «ЭлектроПласт» является направление «Источники питания». Мы предлагаем Вам помощь Конструкторского отдела:

- Подбор оптимального решения, техническое обоснование при выборе компонента;
- Подбор аналогов;
- Консультации по применению компонента;
- Поставка образцов и прототипов;
- Техническая поддержка проекта;
- Защита от снятия компонента с производства.



#### Как с нами связаться

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