## Introduction

This Application Note is intended to provide practical guidance in the selection of PIN Diodes for switch control circuit functions. Switches, Digital and Analog Attenuators, and Limiters each have unique functions that require proper device selection. The design difficulty lies within the parametric translation from Diode Specifications, to the circuit designers' Microwave Specifications. Diode parametric language such as $\mathrm{Vb}, \mathrm{Vf}, \mathrm{Ct}, \mathrm{Rs}, \tau_{\mathrm{L}}, \theta$, must convert into Insertion Loss, VSWR, Isolation, P1dB, Input IP3, RF Operating Power, RF Power Dissipation, and D.C. Power Consumption Specification Terminology.

In addition to actual diode parameters, package parasitics play a significant role in determining switch circuit performance. Package capacitance, package inductance, package electrical resistance, and package thermal impedance are extremely important considerations to determine the effective frequency bandwidth and maximum incident power for reliable switch operation.

The manufacturing methodology dictates the type of diode selection. Surface mount assembly will mandate the usage of either plastic, HMIC SURMOUNT, or MELF \& HiPAX ceramic devices. Chip and Wire ( Hybrid ) manufacturing will determine the usage of Cermachips, Flip Chips, or Beam Lead Devices. Schematics for the most common switch designs: Series-Exclusive, Shunt-Exclusive, and Series-Shunt are outlined below for consideration.

## The Decision Making Process for PIN Diode Selection for Microwave Switch Design

The following procedure outlines and Effective Process for PIN Diode Selection for Switch Design.

1. Determine the Preferred Type of Manufacturing for the PIN Diode in the Switch Design: Surface Mount or Chip and Wire (Hybrid) Manufacturing.
2. Determine the Frequency of Operation and RF Power Handling of the Switch Design.
3. Use Table 1, "Relative Switch Performance and Design Evaluation Matrix" to determine the Type of Switch Design that Best Satisfies the Particular Switch Specifications and Requirements.
4. Use Table 2, "Relative PIN Diode Performance Evaluation Matrix" to Determine the Type of PIN Diode that Best Satisfies the Switch Design Selected from Table 1.
5. Use Table 3, "PIN Diode P/N Series Matrix" to Determine the PIN Diode P/N Series that Best Satisfies the Type of PIN Diode Selected from Table 2.

Table 1: Relative Switch Performance and Design Evaluation Matrix

|  | Switch Design Configuration |  |  |
| :---: | :---: | :---: | :---: |
| Parameter | Series Diodes Exclusive | Shunt Diodes Exclusive | Series-Shunt Diodes |
| Insertion Loss | Worst | Moderate | Best |
| VSWR | Moderate | Worst | Best |
| Isolation | Worst | Moderate | Best |
| P1dB | Moderate | Moderate | Moderate |
| Input IP3 | Moderate | Moderate | Moderate |
| RF Incident Power | Worst | Best | Moderate |
| RF Power Dissipation | Worst | Best | Moderate |
| Switching Speed | Worst | Best | Moderate |
| D.C. Power Consumption | Best (Single +5V) | Moderate (+5V, -5 V) | Worst (+5 V, -5V) |
| PIN Diode Driver Design Simplicity | Best (+5 V Only) | Moderate (+5V, -5 V ) | Moderate (+5 V, -5 V) |
| RF Design Simplicity | Best | Worst | Moderate |
| Cost | Best | Moderate | Moderate |
| Overall Evaluation | 34 Points | 38 Points | 40 Points |

## Notes:

1. Evaluation based upon following grading : Best =5 Points, Moderate $=3$ Points, Worst $=1$ Point. The higher the score, the better the overall relative design advantage.
2. Where there is No significant relative advantage, a " Moderate " weighting can be used.

## Assumptions for SP2T Design:

1. Design is a Reflective SP2T.
2. (2) Diodes are used per RF port.
3. Frequency Bandwidth is $3.0: 1$ maximum.

## Conclusions:

The Series-Shunt Design is the Best in terms of Overall Switch Performance and value. Since each Design has a specific advantage, the decision for a Switch Design Selection is determined by the Specific Design Priorities for the requirement.

[^0]
## Table 2: Relative PIN Diode Performance Evaluation Matrix

|  | Surface Mount Assembly |  |  | Chip \& Wire Hybrid Assembly |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Key Parameter | Plastic | $\begin{gathered} \text { MELF or Hi- } \\ \text { Pax } \end{gathered}$ | SURMOUNT | Cerma Chip | Flip Chip | Beam Lead |
| $1 \mathrm{MHz}<\mathrm{F}<1 \mathrm{GHz}$ |  | Best Selection |  |  |  |  |
| $100 \mathrm{MHz}<\mathrm{F}<4 \mathrm{GHz}$ | Best Selection |  |  |  |  |  |
| $4 \mathrm{GHz}<\mathrm{F}<20 \mathrm{GHz}$ |  |  | Best Selection |  |  |  |
| $20 \mathrm{GHz}<\mathrm{F}<60 \mathrm{GHz}$ |  |  |  |  | Best Selection | Best Selection |
| 100 MHz < F $<20 \mathrm{GHz}$ |  |  |  | Best Selection |  |  |
| Pinc < 0.1 W |  |  |  |  |  | Best Selection |
| 0.1 W < Pinc < 1 W | Best Selection |  |  |  | Best Selection |  |
| 1 W < Pinc < 20 W |  |  | Best Selection |  |  |  |
| 20 W < Pinc < 200 W |  | Best Selection |  | Best Selection |  |  |
| Relative Cost Index | Lowest | Moderate/Highest | Moderate/Highest | Lowest | Moderate | Highest |

## Conclusions:

1. Plastic Devices are best suited where Cost is a decision driver, the Operating Frequency $<4 \mathrm{GHz}$, and the RF C.W. Incident Power < 1 W ( + 30 dBm ).
2. MELF or HIPAX Ceramic Devices are best utilized where Highest Average Power ( $>20 \mathrm{~W}$ C.W.) is the Primary Design Goal and the Operating Frequency $<1 \mathrm{GHz}$.
3. SURMOUNT Devices are probably the Best Overall Compromise in Device Selection. They can Operate ( In Various bands ) from $10 \mathrm{MHz}-20 \mathrm{GHz}$ and Perform well with RF Incident Power < 20 W C.W ( +43 dBm ).
4. Cermachip Devices provide the Best Overall Performance for Operating Frequeny ( $100 \mathrm{MHz}-20$ GHz ), and RF Incident Power < 200 W C.W (+ 53 dBm ).
5. Flip Chip Devices are best suited for mmwave Frequencies $<60 \mathrm{GHz}$, where the RF Incident C.W. < 1W ( +30 dBm ) and Conductive Epoxy or Soldering is Required.
6. Beam Lead Devices are best suited for mmwave Frequencies $<60 \mathrm{GHz}$, where the RF Incident C.W. < 0.1 W ( +20 dBm ) and Thermo Compression Bonding is Required.
[^1]Table 3: PIN Diode Part Number Series Matrix

| Plastic PIN <br> Diodes | MELF \& HiPax <br> PIN Diodes | SURMOUNT PIN <br> Diodes | Cermachip PIN <br> Diodes | Flip Chip PIN <br> Diodes |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Beam Lead PIN |  |  |  |  |  |
| Diodes |  |  |  |  |  |

## Notes:

1. The following M/A-COM PIN Diode Drivers Operating with +5 V \& -5 V D.C. Power Supplies are Practical with Many PIN Diode Switch Designs: DR65 Series, MADRMA0001 and MADRMA0002 Series.
2. M/A-COM Website Homepage Hyperlink Address: http://www.macom.com
[^2]PIN Diodes for Microwave Switch Designs
Rev. V2

Schematic 1: SP2T Series Exclusive PIN Diode Switch, 40 dB Isolation with +5 V Supply


Schematic 1: D.C. Bias to RF Truth Table

| RF State | B2 Bias | B3 Bias |
| :---: | :---: | :---: |
| Low Loss J1-J2 \& Isolation J1-J3 | $+0.5 \mathrm{~V} @ 10 \mathrm{~mA}$ | $+5 \mathrm{~V} @ 0 \mathrm{~mA}$ |
| Low Loss J1-J3 \& Isolation J1-J2 | $+5 \mathrm{~V} @ 0 \mathrm{~mA}$ | $+0.5 \mathrm{~V} @ 10 \mathrm{~mA}$ |

Schematic 2: SP2T All Shunt, 60 dB Isolation Design with $90^{\circ}$ Transformer using Distributed Transmission Line


Schematic 2: D.C. Bias to RF Truth Table

| RF State | B2 Bias | B3 Bias |
| :---: | :---: | :---: |
| Low Loss J1-J2 \& Isolation J1-J3 | $-\mathrm{V} @ 0 \mathrm{~mA}$ | $+1 \mathrm{~V} @(+20 \mathrm{~mA} \mathrm{per} \mathrm{Diode)}$ |
| Low Loss J1-J3 \& Isolation J1-J2 | $+1 \mathrm{~V} @(+20 \mathrm{~mA} \mathrm{per} \mathrm{Diode)}$ | $-\mathrm{V} @ 0 \mathrm{~mA}$ |

Schematic 3: SP2T All Shunt, 30 dB Isolation Design using $\boldsymbol{\pi}, \mathrm{C}-\mathrm{L}-\mathrm{C}$ Lumped Element $90^{\circ}$ Transformer


Schematic 3: D.C. Bias to RF Truth Table

| RF State | B2 Bias | B3 Bias |
| :---: | :---: | :---: |
| Low Loss J1-J2 \& Isolation J1-J3 | $-\mathrm{V} @ 0 \mathrm{~mA}$ | $+1 \mathrm{~V} @+20 \mathrm{~mA}$ |
| Low Loss J1-J3 \& Isolation J1-J2 | $+1 \mathrm{~V} @+20 \mathrm{~mA}$ | $-\mathrm{V} @ 0 \mathrm{~mA}$ |

Schematic 4: SP2T Series-Shunt, 40 dB Isolation Design with Positive \& Negative Bias Current


## Schematic 4: D.C. Bias to RF Truth Table

| RF State | B2 Bias | B3 Bias |
| :---: | :---: | :---: |
| Low Loss J1-J2 \& Isolation J1-J3 | $-4 \mathrm{~V} @ 10 \mathrm{~mA}$ | $+1 \mathrm{~V} @+10 \mathrm{~mA}$ |
| Low Loss J1-J3 \& Isolation J1-J2 | $+1 \mathrm{~V} @+10 \mathrm{~mA}$ | $-4 \mathrm{Q} @-10 \mathrm{~mA}$ |

Schematic 5: SP2T Series-Shunt, 40 dB Isolation Design with +5 V Supply


## Schematic 5: D.C. Bias to RF Truth Table

| RF State | B2 Series Bias | B2 Shunt Bias | B3 Series Bias | B3 Shunt Bias | B0 Voltage |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  <br> $\mathrm{J} 1-\mathrm{J} 3$ Isolation | $+0.5 \mathrm{~V} @ 11 \mathrm{~mA}$ | $+5 \mathrm{~V} @ 0 \mathrm{~mA}$ | $+1.4 \mathrm{~V} @+11 \mathrm{~mA}$ <br> $(T o \mathrm{~J} 3$ Shunt Diode) | $+0.5 \mathrm{~V} @+11 \mathrm{~mA}$ | +1.4 V |
|  <br> $\mathrm{J} 1-\mathrm{J} 2$ Isolation | $+1.4 \mathrm{~V} @+11 \mathrm{~mA}$ <br> (To J2 Shunt Diode) | $+0.5 \mathrm{~V} @+11 \mathrm{~mA}$ | $+0.5 \mathrm{~V} @+10 \mathrm{~mA}$ | $+5 \mathrm{~V} @ 0 \mathrm{~mA}$ | +1.4 V |

Notes:

1. Forward Bias Diode $\Delta \mathrm{Vf} @ 10 \mathrm{~mA} \sim+0.9 \mathrm{~V}$
2. Reverse Bias Series Diode $=(+1.4 \mathrm{~V}-+1.4 \mathrm{~V})=0 \mathrm{~V}$
3. Reverse Bias Shunt Diode $=(+0.5 \mathrm{~V}-+5.0 \mathrm{~V})=-4.5 \mathrm{~V}$

PIN Diodes for Microwave Switch Designs

Schematic 6: TR Switch Schematic with 25 dB Isolation Design with +3 V Supply


## Schematic 6: TR Switch D.C. Bias to RF Truth Table

| RF State | B1 Bias |
| :---: | :---: |
| Low Loss Tx - Ant \& Isolation $\mathrm{Rx}-\mathrm{Tx}$ | $+2 \mathrm{~V} @+10 \mathrm{~mA}$ |
| Low Loss Ant $-\mathrm{Rx} \&$ Isolation $\mathrm{Tx}-\mathrm{Rx}$ | $0 \vee @ 0 \mathrm{~mA}$ |

For Lumped Electrical Transmission Line Length, $\theta$, between Junction and Rx Shunt Diode :
$L=Z o /(2 \pi F o), C=1 /(2 \pi F o Z o)$, Where $F o$ is the Resonant Frequency $=\left(F_{1}{ }^{*} F_{2}\right)^{1 / 2} \& F_{1} \& F_{2}$ are Band Edge Frequencies.


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