

SLVSBI1A –OCTOBER 2013–REVISED SEPTEMBER 2014

TPS6128x Low-, Wide- Voltage Battery Front-End DC/DC Converter Single-Cell Li-Ion, Ni-Rich, Si-Anode Applications

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-
-
- **Output Voltage**
-
- True Pass-Through Mode During Shutdown
-
-
- In-Situ Customization with On-Chip E^2 PROM
- - $-$ I²C Compatible I/F up to 3.4Mbps (TPS61280)
	- Simple I/O Logic Control Interface (TPS6128x) boost mode to utilize the full battery capacity.
- Thermal Shutdown and Overload Protection **Device Information[\(1\)](#page-0-0)**
-

- Single-Cell Ni-Rich, Si-Anode, Li-Ion, LiFePO4 Smart-Phones or Tablet PCs
- 2.5G/3G/4G Mini-Module Data Cards
- Current Limited Applications Featuring High Peak Power Loads

4 Simplified Schematic

1 Features 3 Description

Tools & **[Software](#page-47-0)**

95% Efficiency at 2.3MHz Operation **195% CODEN 14 TRS6128x** device provides a power supply solution for products powered by either by a Li-Ion, 2μ A Quiescent Current in Low I_Q Pass-Through Nickel-Rich, Silicon Anode, Li-Ion or LiFePO4 battery.

Node, Life veltical scription Anode, Life battery. Mode
Wide V_{IN} Range From 2.3V to 4.8V **The voltage range is optimized for single-cell portable**
applications like in smart-phones or tablet PCs. applications like in smart-phones or tablet PCs.

 I_{OUT} ≥ 4A (Peak) at V_{OUT} = 3.35V, V_{IN} ≥ 2.65V Used as a high-power pre-regulator, the TPS6128x
Integrated Pass-Through Mode (35mΩ) extends the battery run-time and overcomes input extends the battery run-time and overcomes input current- and voltage limitations of the powered • Programmable Valley Inductor Current Limit and

• Programmable Average Input Current Limit and While in shutdown, the TPS6128x operates in a true Output Voltage pass-through mode with only 2µA quiescent consumption for longest battery shelf life.

During operation, when the battery is at a good state- • *Best-in-Class* Line and Load Transient of-charge, a low-ohmic, high-efficient integrated pass- Low-Ripple Light-Load PFM Mode
through path connects the battery to the powered system.

(Write Protect)

If the battery gets to a lower state of charge and its

Voltage becomes lower than the desired minimum voltage becomes lower than the desired minimum system voltage, the device seamlessly transits into

(1) For all available packages, see the orderable addendum at

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5 Revision History

Changes from Original (October 2013) to Revision A Page

6 Description (continued)

TPS6128x device supports more than 4A pulsed load current even from a deeply discharged battery. In this mode of operation, the TPS6128x enables the utilization of the full battery capacity: A high battery-cut-off voltage originated by powered components with a high minimum input voltage is overcome; new battery chemistries can be fully discharged; high current pulses forcing the system into shutdown are buffered by the device seamlessly transitioning between boost and by-pass mode back and forth.

This has significant impact on the battery on-time and translates into either a longer use-time and better userexperience at an equal battery capacity or into reduced battery costs at similar use-times.

The TPS6128x operates in synchronous, 2.3MHz boost mode and enters power-save mode operation (PFM) at light load currents to maintain high efficiency over the entire load current range.

The TPS6128x offers a small solution size (<20mm²) due to minimum amount of external components, enabling the use of small inductors and input capacitors, available as a 16-pin chip-scale package (CSP).

7 Device Comparison Table

8 Pin Configuration and Functions

TOP VIEW

Pin Functions - TPS61280

TPS6128x

TOP VIEW

Pin Functions - TPS6128x

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EXAS **STRUMENTS**

9 Specifications

9.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

(1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods my affect device reliability.

(2) All voltages are with respect to network ground terminal.

(3) Limit the junction temperature to 105°C for continuous operation at maximum output power.

(4) Limit the junction temperature to 105°C for 15% duty cycle operation.

(5) In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature $(T_{A(max)}$ is dependent on the maximum operating junction temperature $(T_{J(max)})$, the maximum power dissipation of the device in the application $(P_{D(max)})$, and the junction-to-ambient thermal resistance of the part/package in the application (θ_{JA}), as given by the following equation: $T_{A(max)} = T_{J(max)} - (θ_A \times P_{D(max)})$. To achieve optimum performance, it is recommended to operate the device with a maximum junction temperature of 105°C.

9.2 Handling Ratings

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

9.3 Recommended Operating Conditions

9.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](http://www.ti.com/lit/pdf/spra953).

9.5 Electrical Characteristics

Minimum and maximum values are at V_{IN} = 2.3V to 4.85V, V_{OUT} = 3.4V (or V_{IN}, whichever is higher), EN = 1.8V, VSEL = 1.8V, nBYP = 1.8V, -40° C ≤ T_J ≤ 125°C; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are at $V_{IN} = 3.2V$, $V_{OUT} = 3.4V$, $EN = 1.8V$, $T_J = 25^{\circ}C$ (unless otherwise noted).

Electrical Characteristics (continued)

Minimum and maximum values are at $V_{IN} = 2.3V$ to 4.85V, $V_{OUT} = 3.4V$ (or V_{IN} , whichever is higher), EN = 1.8V, VSEL = 1.8V, nBYP = 1.8V, $-40^{\circ}C \le T_J \le 125^{\circ}C$; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are at $V_{IN} = 3.2V$, $V_{OUT} = 3.4V$, $EN = 1.8V$, $T_J = 25°C$ (unless otherwise noted).

(1) Verified by characterization. Not tested in production.

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9.6 Timing Requirements

(1) Specified by characterization. Not tested in production.

9.7 I ²C Interface Timing Characteristics(1)

(1) Specified by design. Not tested in production.

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ISTRUMENTS

Texas

I ²C Interface Timing Characteristics[\(1\)](#page-9-0) (continued)

Figure 1. Serial Interface Timing Diagram for Standard-, Fast-, Fast-Mode Plus

Note A: First rising edge of the SCLH signal after Sr and after each acknowledge bit.

Figure 2. Serial Interface Timing Diagram for H/S-Mode

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9.8 Typical Characteristics

Typical Characteristics (continued)

Texas **NSTRUMENTS**

10 Detailed Description

10.1 Overview

The TPS6128x is a high-efficiency step-up converter featuring pass-through mode optimized to provide low-noise voltage supply for 2G RF power amplifiers (PAs) in mobile phones and/or to pre-regulate voltage for supplying subsystem like eMMC memory, audio codec, LCD bias, antenna switches, RF engine PMIC etc. It is designed to allow the system to operate at maximum efficiency for a wide range of power consumption levels from a low-, wide- voltage battery cell.

The capability of the TPS6128x to step-up the voltage as well as to pass-through the input battery voltage when its level is high enough allow systems to operate at maximum performance over a wide range of battery voltages, thereby extending the battery life between charging. The device also addresses brownouts caused by the peak currents drawn by the APU and GPU which can cause the battery rail to droop momentarily. Using the TPS6128x device as a pre-regulator eliminates system brownout condition while maintaining a stable supply rail for critical sub-system to function properly.

The TPS6128x synchronous step-up converter typically operates at a quasi-constant 2.3-MHz frequency pulse width modulation (PWM) at moderate to heavy load currents. At light load currents, the TPS6128x converter operates in power-save mode with pulse frequency modulation (PFM).

In general, a dc/dc step-up converter can only operate in "true" boost mode, i.e. the output "boosted" by a certain amount above the input voltage. The TPS6128x device operates differently as it can smoothly transition in and out of zero duty cycle operation. Depending upon the input voltage, output voltage threshold and load current, the integrated bypass switch automatically transitions the converter into pass-through mode to maintain lowdropout and high-efficiency. The device exits pass-through mode (0% duty cycle operation) if the total dropout resistance in bypass mode is insufficient to maintain the output voltage at it's nominal level. Refer to the typical characteristics section (DC Output Voltage vs. Input Voltage) for further details.

During PWM operation, the converter uses a novel quasi-constant on-time valley current mode control scheme to achieve excellent line/load regulation and allows the use of a small ceramic inductor and capacitors. Based on the $V_{\text{IN}}/V_{\text{OUT}}$ ratio, a simple circuit predicts the required on-time. At the beginning of the switching cycle, the lowside N-MOS switch is turned-on and the inductor current ramps up to a peak current that is defined by the ontime and the inductance. In the second phase, once the on-timer has expired, the rectifier is turned-on and the inductor current decays to a preset valley current threshold. Finally, the switching cycle repeats by setting the on timer again and activating the low-side N-MOS switch.

The current mode architecture provides excellent transient load response, requiring minimal output filtering. Internal soft-start and loop compensation simplifies the design process while minimizing the number of external components.

The TPS6128x directly and accurately controls the average input current through intelligent adjustment of the valley current limit, allowing an accuracy of ±17.5%. Together with an external bulk capacitor, the TPS6268x allows an application to be interfaced directly to its load, without overloading the input source due to appropriate set average input current limit. An open-drain output (PG or GPIO/nFAULT) provides a signal to issue an interrupt to the system if any fault is detected on the device (thermal shutdown, output voltage out-of limits etc ...).

The output voltage can be dynamically adjusted between two values (floor and roof voltages) by toggling a logic control input (VSEL) without the need for external feedback resistors. This features can either be used to raise the output voltage in anticipation of a positive load transient or to dynamically change the PA supply voltage depending on its mode of operation and/or transmitting power.

The TPS61280 integrates an I²C compatible interface allowing transfers up to 3.4Mbps. This communication interface can be used to set the output voltage threshold at which the converter transitions between boost and pass-through mode, for reprogramming the mode of operation (PFM/PWM or forced PWM), for settings the average input current limit or resetting the output voltage for instance.

Configuration parameters can be changed by writing the desired values to the appropriate $I²C$ register(s). The ¹²C registers are volatile and their contents are lost when power is removed from the device. By writing to the *[E2PROMCTRL](#page-32-0) Register*, it is possible to store the active configuration in non-volatile E ²PROM; during power-up, the contents of the E^2 PROM are copied into the I^2C registers and used to configure the device.

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10.2 Functional Block Diagram

10.3 Feature Description

10.3.1 Voltage Scaling Management (VSEL)

In order to maintain a certain minimum output voltage under heavy load transients, the output voltage set point can be dynamically increased by asserting the VSEL input. The functionality also helps to mitigate undershoot during severe line transients, while minimizing the output voltage during more benign operating conditions to save power.

The output voltage ramps up (floor to roof transition) at pre-defined rate defined by the average input current limit setting. The required time to ramp down the voltage (roof to floor transition) largely depends on the amount of capacitance present at the converter's output as well as on the load current. [Table](#page-15-1) 1 shows the ramp rate control when transitioning to a lower voltage.

Table 1. Ramp Down Rate vs. Target Mode

10.3.2 Spread Spectrum, PWM Frequency dithering

The goal is to spread out the emitted RF energy over a larger frequency range so that the resulting EMI is similar to white noise. The end result is a spectrum that is continuous and lower in peak amplitude, making it easier to comply with electromagnetic interference (EMI) standards and with the power supply ripple requirements in cellular and non-cellular wireless applications. Radio receivers are typically susceptible to narrowband noise that is focused on specific frequencies.

Switching regulators can be particularly troublesome in applications where electromagnetic interference (EMI) is a concern. Switching regulators operate on a cycle-by-cycle basis to transfer power to an output. In most cases, the frequency of operation is either fixed or regulated, based on the output load. This method of conversion creates large components of noise at the frequency of operation (fundamental) and multiples of the operating frequency (harmonics).

The spread spectrum architecture varies the switching frequency by ca. ±15% of the nominal switching frequency thereby significantly reducing the peak radiated and conducting noise on both the input and output supplies. The frequency dithering scheme is modulated with a triangle profile and a modulation frequency f_m .

The above figures show that after modulation the sideband harmonic is attenuated compared to the nonmodulated harmonic, and the harmonic energy is spread into a certain frequency band. The higher the modulation index (*mf*) the larger the attenuation.

(1) Spectrum illustrations and formulae ([Figure](#page-15-2) 15 and [Figure](#page-15-2) 16) copyright IEEE TRANSACTIONS ON ELECTROMAGNETIC COMPATIBILITY, VOL. 47, NO.3, AUGUST 2005.

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$$
m_f = \frac{\delta \times f_c}{f_m}
$$

where

- *f^c* is the carrier frequency (approx. 2.3MHz)
- *f^m* is the modulating frequency (approx. 40kHz)
- *δ* is the modulation ratio (approx 0.15) (1)

$$
\delta = \frac{\Delta f_{\rm c}}{f_{\rm c}}\tag{2}
$$

The maximum switching frequency *f^c* is limited by the process and finally the parameter modulation ratio (δ), together with *f^m* , which is the side-band harmonics bandwidth around the carrier frequency *f^c* . The bandwidth of a frequency modulated waveform is approximately given by the Carson's rule and can be summarized as:

$$
B = 2 \times f_m \times (1 + m_f) = 2 \times (\Delta f_c + f_m)
$$
\n(3)

f^m < RBW: The receiver is not able to distinguish individual side-band harmonics, so, several harmonics are added in the input filter and the measured value is higher than expected in theoretical calculations.

f^m > RBW: The receiver is able to properly measure each individual side-band harmonic separately, so the measurements match with the theoretical calculations.

Output Voltage

10.4 Device Functional Modes

10.4.1 Power-Save Mode

The TPS6128x integrates a power-save mode to improve efficiency at light load. In power save mode the converter only operates when the output voltage trips below a set threshold voltage. It ramps up the output voltage with several pulses and goes into power save mode once the output voltage exceeds the set threshold voltage. The PFM mode is left and PWM mode entered in case the output current can not longer be supported in PFM mode.

PFM mode at light load

PFM ripple

1.006 x VOUT NOM.

AAAAA- ^Vout nom.

Figure 17. Power-Save Mode Ripple

10.4.2 Pass-Through Mode

The TPS6128xA contains an internal switch for bypassing the dc/dc boost converter during pass-through mode. When the input voltage is larger than the preset output voltage, the converter seamlessly transitions into 0% duty cycle operation and the bypass FET is fully enhanced. Entry in pass-through mode is triggered by condition where VOUT > VOUT_NORM and no switching has occurred during past 16μs.

In this mode of operation, the load (2G RF PA for instance) is directly supplied from the battery for maximum RF output power, highest efficiency and lowest possible input-to-output voltage difference. The device consumes only a standby current of 15µA (typ). In pass-through mode, the device is short-circuit protected by a very fast current limit detection scheme.

During this operation, the output voltage follows the input voltage and will not fall below the programmed output voltage threshold as the input voltage decreases. The output voltage drop during pass-through mode depends on the load current and input voltage, the resulting output voltage is calculated as:

$$
V_{OUT} = V_{IN} - (R_{DSON(BP)} \times I_{OUT})
$$

Conversely, the efficiency in pass-through mode is defined as:

$$
\eta = 1 - R_{\text{DSON(BP)}} \frac{I_{\text{OUT}}}{V_{\text{IN}}}
$$

in which $R_{DSON(BP)}$ is the typical on-resistance of the bypass FET

(4)

Device Functional Modes (continued)

Figure 18. DC Output Voltage vs. Input Voltage

Pass-through mode exit is triggered when the output voltage reaches the pre-defined threshold (e.g. 3.4V).

During pass-through mode, the TPS6128x device is short-circuit protected by a very fast current limit detection scheme. If the current in the pass-through FET exceeds approximately 7.3Amps a fault is declared and the device cycles through a start-up procedure.

10.4.3 Mode Selection

Depending on the settings of *[CONFIG](#page-27-0) Register* the device can be operated at a quasi-constant 2.3-MHz frequency PWM mode or in automatic PFM/PWM mode. In this mode, the converter operates in pseudo-fixed frequency PWM mode at moderate to heavy loads and in the PFM mode during light loads, which maintains high efficiency over a wide load current range. For more details, see the *[CONFIG](#page-27-0) Register* description.

The quasi-constant frequency PWM mode has the tightest regulation and the best line/load transient performance. In forced PWM mode, the device features a unique $R_{DS(ON)}$ management function to maintain high broadband efficiency as well as low resistance in pass-through mode.

In the TPS61280 device, the GPIO pin can be configured (via the *[CONFIG](#page-27-0) Register*) to select the operating mode of the device. In the other TPS6128x devices, the MODE pin is used to select the operating mode. Pulling this pin high forces the converter to operate in the PWM mode even at light load currents. The advantage is that the converter modulates its switching frequency according to a spread spectrum PWM modulation technique allowing simple filtering of the switching harmonics in noise-sensitive applications.

For additional flexibility, it is possible to switch from power-save mode (GPIO or MODE input = L) to PWM mode (GPIO or MODE input = H) during operation. This allows efficient power management by adjusting the operation of the converter to the specific system requirements (e.g. 2G RF PA Rx/Tx operation).

NOTE

During start-up (conventionally or when recovering from thermal shutdown) the device must be set to operate with auto PFM/PWM mode. Consequently, the device determines automatically PFM or PWM mode depending on the output's load. Once the output voltage settled and PG pin indicates that the converter's output voltage is within its regulation limits, the device can be forced in PWM mode operation, if desired.

Entry to forced pass-through mode ($nBYP = L$) initiates with a current limited transition followed by a true bypass state. To prevent reverse current to the battery, the devices waits until the output discharges below the input voltage level before entering forced pass-through mode. Care should be taken to prohibit the output voltage from collapsing whilst transitioning into forced pass-through mode under heavy load conditions and/or limited output capacitance. This can be easily done by adding capacitance to the output of the converter. In forced passthrough mode, the output follows the input below the preset output threshold voltage (VOUT_TH).

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Device Functional Modes (continued)

10.4.4 Current Limit Operation

The TPS6128x device features a valley inductor current limit scheme.

In dc/dc boost mode, the TPS6128x device employs a current limit detection scheme in which the voltage drop across the synchronous rectifier is sensed during the off-time. In the TPS61280 the current limit threshold can be set via an I ²C register. TPS6128x devices have a fixed current limit threshold. See the *Device [Comparison](#page-2-1) Table* for detailed information.

The output voltage is reduced as the power stage of the device operates in a constant current mode. The maximum continuous output current (I_{OUTIMAX}), before entering current limit (CL) operation, can be defined by [Equation](#page-19-0) 6.

$$
I_{\text{OUT}(MAX_DC)} = I_{LIMIT} \times \frac{V_{IN}}{V_{OUT}} \times \eta
$$
\n(6)

Where η is the efficiency

The inductor peak-to-peak current ripple ($Δl_L$) is calculated by [Equation](#page-19-1) 7

$$
\Delta I_{L} = \frac{V_{N}}{L} \times \frac{D}{f}
$$
 (7)

The output current, $I_{\text{OUT(DC)}}$, is the average of the rectifier ripple current waveform. When the load current is increased such that the trough is above the current limit threshold, the off-time is increased to allow the current to decrease to this threshold before the next on-time begins (so called frequency fold-back mechanism). When the current limit is reached the output voltage decreases during further load increase.

[Figure](#page-19-2) 19 illustrates the inductor and rectifier current waveforms during current limit operation.

During pass-through mode, the TPS6128x device is short-circuit protected by a very fast current limit detection scheme. If the current in the bypass FET exceeds approximately 7.5Amps a fault is declared and the device cycles through a start-up procedure.

10.4.5 Start-Up and Shutdown Mode

The TPS6128x automatically powers-up as soon as the input voltage is applied. The device has an internal softstart circuit that limits the inrush current during start-up. The first phase in the start-up procedure is to bias the output node close to the input level (so called pre-charge phase).

Device Functional Modes (continued)

In this operating mode, the device limits its output current to ca. 500mA. Should the output voltage not have reached the input level within a maximum duration of 750µs, the device automatically increases its pre-charge current to ca. 2000mA. If the output voltage still fails to reach its target after 1.5ms, a fault condition is declared. After waiting 1ms, a restart is attempted.

During start-up, it is recommended to keep DC load current draw below 250mA.

The TPS6128x device contains a thermal regulation loop that monitors the die temperature during the pre-charge phase. If the die temperature rises to high values of about 110°C, the device automatically reduces the current to prevent the die temperature from increasing further. Once the die temperature drops about 10°C below the threshold, the device will automatically increase the current to the target value. This function also reduces the current during a short-circuit condition.

When the EN and nBYP pins are set high, the device enters normal operation (i.e. automatic dc/dc boost, passthrough mode) and ensures that the output voltage remains above a pre-defined threshold (e.g. 3.3V).

Setting the EN pin low (nBYP = 1) forces the TPS6128x device in shutdown mode with a current consumption of <8.5µA typ. In this mode, the output of the converter is regulated to a minimum level so as to limit the input-tooutput voltage difference to less than 3.6V (typ). The device is capable of sinking up to 10mA output current and prohibits reverse current flow from the output to the input. For proper operation, the EN pin must be terminated and must not be left floating.

Changing operating mode from auto mode (EN = $nBYP = 1$) to low I_0 Pass-through mode (EN = $nBYP = 0$) with device pins EN and nBYP can either be done controlling EN and nBYP pins from same control signal (delay between signal < 60ns) or first switching in forced pass-through mode (EN = 1, nBYP = 0) followed by switching to low I_{Ω} Pass-through mode (EN = nBYP = 0).

The TPS6128x device also features the possibility of shutting the converter's output for a short period of time, either via the nRST/nFAULT (GPIO). Pulling this input low initiates a reset of the converter's output. The sequence is falling edge-triggered and consists of a discharge phase (down to ca. 600mV or lower) of the capacitance located at the converter's output followed by a start-up phase.

Table 2. Mode of Operation

10.4.6 Undervoltage Lockout

The under voltage lockout circuit prevents the device from malfunctioning at low input voltages and the battery from excessive discharge. The I2C control interface and the output stage of the converter are disabled once the falling V_{IN} trips the under-voltage lockout threshold V_{UVLO} (2.0V typ). The device starts operation once the rising V_{IN} trips V_{UNLO} threshold plus its hysteresis of 100 mV at typ. 2.1V.

10.4.7 Thermal Shutdown

As soon as the junction temperature, T_{J} , exceeds 150°C (typ.) the device goes into thermal shutdown. In this mode the bypass, high-side and low-side MOSFETs are turned-off. When the junction temperature falls below the thermal shutdown minus its hysteresis, the device continuous the operation.

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10.4.8 Fault State and Power-Good

The TPS6128x enters the fault state under any of the followings conditions:

- The output voltage fails to achieve the required level during a start-up phase.
- The output voltage falls out of regulation (in pre-charge mode).
- The device has entered thermal shutdown.

Once a fault is triggered, the regulator stops operating and disconnects the load. After waiting 1ms, the device attempts to restart. The TPS61280 device can be configured to signal a fault condition by pulling the open-drain GPIO pin (nFAULT) low for a short period of time. The nFAULT output provides a falling edge triggered interrupt signal to the host. To ensure proper operation, the GPIO port needs to be pull high quick enough, i.e. faster than ca. 200ns. To do so, it is recommended to use a GPIO pull-up resistor in the range of 1kΩ to 10kΩ.

The TPS6128x (simple logic I/F version) device only provide a power-good output (PG) for signaling the system when the regulator has successfully completed start-up and no faults have occurred. Power-good also functions as an early warning flag for excessive die temperature and overload conditions.

- PG is asserted high when the start-up sequence is successfully completed.
- PG is pulled low when the output voltage falls approx. 10% below its regulation level or the die temperature exceeds 115°C. PG is re-asserted high when the device cools below ca. 100°C.
- Any fault condition causes PG to be de-asserted.
- PG is pulled high when the device is operating in forced pass-through mode (i.e. $nBYP = L$).
- PG is pulled high when the device is in shutdown mode.

10.5 Programming

10.5.1 Serial Interface Description (TPS61280)

I²C[™] is a 2-wire serial interface developed by Philips Semiconductor, now NXP Semiconductors (see I2C-Bus Specification, Version 2.1, January 2000). The bus consists of a data line (SDA) and a clock line (SCL) with pullup structures. When the bus is *idle*, both SDA and SCL lines are pulled high. All the I ²C compatible devices connect to the I ²C bus through open drain I/O pins, SDA and SCL. A *master* device, usually a microcontroller or a digital signal processor, controls the bus. The master is responsible for generating the SCL signal and device addresses. The master also generates specific conditions that indicate the START and STOP of data transfer. A *slave* device receives and/or transmits data on the bus under control of the master device.

The TPS6128x device works as a *slave* and supports the following data transfer *modes*, as defined in the I ²C-Bus Specification: standard mode (100 kbps) and fast mode (400 kbps), fast mode plus (1 Mbps) and high-speed mode (3.4 Mbps). The interface adds flexibility to the power supply solution, enabling most functions to be programmed to new values depending on the instantaneous application requirements. Register contents remain intact as long as supply voltage remains above 2.1V.

The data transfer protocol for standard and fast modes is exactly the same; therefore, they are referred to as F/S-mode in this document. The protocol for high-speed mode is different from F/S-mode, and it is referred to as HS-mode. The TPS6128xA device supports 7-bit addressing; 10-bit addressing and general call address are not supported. The device 7bit address is defined as '111 0101'.

It is recommended that the I2C masters initiates a STOP condition on the I2C bus after the initial power up of SDA and SCL pull-up voltages to ensure reset of the TPS6128x I2C engine.

10.5.2 Standard-, Fast-, Fast-Mode Plus Protocol

The master initiates data transfer by generating a start condition. The start condition is when a high-to-low transition occurs on the SDA line while SCL is high, as shown in [Figure](#page-22-1) 20. All I²C-compatible devices should recognize a start condition.

Figure 20. START and STOP Conditions

The master then generates the SCL pulses, and transmits the 7-bit address and the read/write direction bit R/W on the SDA line. During all transmissions, the master ensures that data is valid. A valid data condition requires the SDA line to be stable during the entire high period of the clock pulse (see [Figure](#page-22-2) 21). All devices recognize the address sent by the master and compare it to their internal fixed addresses. Only the slave device with a matching address generates an acknowledge (see [Figure](#page-23-0) 22) by pulling the SDA line low during the entire high period of the ninth SCL cycle. Upon detecting this acknowledge, the master knows that communication link with a slave has been established.

Figure 21. Bit Transfer on the Serial Interface

Programming (continued)

The master generates further SCL cycles to either transmit data to the slave (R/W bit 1) or receive data from the slave (R/W bit 0). In either case, the receiver needs to acknowledge the data sent by the transmitter. So an acknowledge signal can either be generated by the master or by the slave, depending on which one is the receiver. 9-bit valid data sequences consisting of 8-bit data and 1-bit acknowledge can continue as long as necessary.

To signal the end of the data transfer, the master generates a stop condition by pulling the SDA line from low to high while the SCL line is high (see [Figure](#page-22-1) 20). This releases the bus and stops the communication link with the addressed slave. All I²C compatible devices must recognize the stop condition. Upon the receipt of a stop condition, all devices know that the bus is released, and they wait for a start condition followed by a matching address.

Attempting to read data from register addresses not listed in this section will result in 00h being read out.

Figure 22. Acknowledge on the I ²C Bus

Figure 23. Bus Protocol

Programming (continued)

10.5.3 HS-Mode Protocol

The master generates a start condition followed by a valid serial byte containing HS master code 00001XXX. This transmission is made in F/S-mode at no more than 400 Kbps. No device is allowed to acknowledge the HS master code, but all devices must recognize it and switch their internal setting to support 3.4 Mbps operation.

The master then generates a *repeated start condition* (a repeated start condition has the same timing as the start condition). After this repeated start condition, the protocol is the same as F/S-mode, except that transmission speeds up to 3.4 Mbps are allowed. A stop condition ends the HS-mode and switches all the internal settings of the slave devices to support the F/S-mode. Instead of using a stop condition, repeated start conditions should be used to secure the bus in HS-mode.

Attempting to read data from register addresses not listed in this section will result in 00h being read out.

10.5.4 TPS6128x I ²C Update Sequence

The TPS6128xA requires a start condition, a valid I²C address, a register address byte, and a data byte for a single update. After the receipt of each byte, TPS6128x device acknowledges by pulling the SDA line low during the high period of a single clock pulse. A valid I²C address selects the TPS6128x. TPS6128x performs an update on the falling edge of the acknowledge signal that follows the LSB byte.

EXAS **ISTRUMENTS**

10.6 Register Maps

10.6.1 Slave Address Byte

The slave address byte is the first byte received following the START condition from the master device.

10.6.2 Register Address Byte

Following the successful acknowledgment of the slave address, the bus master will send a byte to the TPS6128xA, which will contain the address of the register to be accessed.

10.6.3 I ²C Registers, E ²PROM, Write Protect

Configuration parameters can be changed by writing the desired values to the appropriate $I²C$ register(s). The ²C registers are volatile and their contents are lost when power is removed from the device. By writing to the *[E2PROMCTRL](#page-32-0) Register*, it is possible to store the active configuration in non-volatile E ²PROM; during power-up, the contents of the E^2 PROM are copied into the I^2C registers and used to configure the device.

NOTE

An active high Write Protect (WP) bit prevents the configuration parameters from being changed by accident. Once the E²PROM memory has been programmed with Write Protect (WP) bit set, its content will be locked and can not be reprogrammed any more.

Configuration parameters can be read from the I^2C register(s) or E^2 PROM registers at any time (the WP bit has no effect on read operations).

10.6.4 E ²PROM Configuration Parameters

[Table](#page-25-1) 3 shows the memory map of the configuration parameters.

Table 3. Configuration Memory Map

The following procedure details how to save the content of all I²C registers to the E²PROM non-volatile configuration memory.

- 1. Bus master sends START condition
- 2. Bus master sends 7-bit slave address plus low R/W bit (for example EAh)
- 3. TPS6128x acknowledges (SDA low)
- 4. Bus master sends address of *[E2PROMCTRL](#page-32-0) Register* (FFh)
- 5. TPS6128x acknowledges (SDA low)
- 6. Bus master sends data to be written to the Control Register (C0h)
- 7. TPS6128x acknowledges (SDA low)
- 8. Bus master sends STOP condition

Figure 27. Saving Contents of all I ²C Registers to E ²PROM

10.6.5 CONFIG Register

Memory location: 0x01

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10.6.6 VOUTFLOORSET Register

Memory location: 0x02

10.6.7 VOUTROOFSET Register

Memory location: 0x03

10.6.8 ILIMSET Register

Memory location: 0x04

(1) Refer to the *Start-Up and [Shutdown](#page-19-3) Mode* section for additional information.

10.6.9 Status Register

Memory location: 0x05

10.6.10 E2PROMCTRL Register

Memory location: 0xFF

FXAS NSTRUMENTS

11 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

11.1 Application Information

The devices are step up dc/dc converters with true bypass function integrated. They are typically used as preregulators with input voltage ranges from 2.3V to 4.8V, extend the battery run time and overcome input current and input voltage limitations of the system being powered.

While in input voltage higher than boost/bypass threshold, the high-efficient integrated pass-through path connects the battery to the powered system directly.

If the input voltage becomes lower than boost/bypass threshold, the device seamlessly transitions into boost mode operation with a maximum available output current of 3 A.

The following design procedure can be used to select component values for the TPS61280, TPS61281 and TPS61282.

11.2 Typical Application

11.2.1 TPS61281 with 2.5V-4.35 VIN, 1500 mA Output Current (TPS61280 with I ²C Programmable)

Figure 28. TPS61280 Typical Application

11.2.1.1 Design Requirement

Table 4. Design Parameters

11.2.1.2 Detailed Design Parameters

11.2.1.2.1 Inductor Selection

A boost converter normally requires two main passive components for storing energy during the conversion, an inductor and an output capacitor are required. It is advisable to select an inductor with a saturation current rating higher than the possible peak current flowing through the power switches.

The inductor peak current varies as a function of the load, the input and output voltages and can be estimated using [Equation](#page-34-0) 8.

$$
I_{L(PEAK)} = \frac{V_{IN} \times D}{2 \times f \times L} + \frac{I_{OUT}}{(1 - D) \times \eta} \quad \text{with} \quad D = 1 - \frac{V_{IN}}{V_{OUT}} \tag{8}
$$

Selecting an inductor with insufficient saturation performance can lead to excessive peak current in the converter. This could eventually harm the device and reduce it's reliability.

When selecting the inductor, as well as the inductance, parameters of importance are: maximum current rating, series resistance, and operating temperature. The inductor DC current rating should be greater than the maximum input average current, refer to [Equation](#page-34-1) 9 and the *Current Limit [Operation](#page-19-4)* section for more details.

$$
I_{L(DC)} = \frac{V_{OUT}}{V_{IN}} \times \frac{1}{\eta} \times I_{OUT}
$$
 (9)

The TPS6128xA series of step-up converters have been optimized to operate with a effective inductance in the range of 200nH to 800nH. Larger or smaller inductor values can be used to optimize the performance of the device for specific operating conditions. For more details, see the *[Checking](#page-36-0) Loop Stability* section.

In high-frequency converter applications, the efficiency is essentially affected by the inductor AC resistance (that is, quality factor) and to a smaller extent by the inductor DCR value. To achieve high efficiency operation, care should be taken in selecting inductors featuring a quality factor above 25 at the switching frequency. Increasing the inductor value produces lower RMS currents, but degrades transient response. For a given physical inductor size, increased inductance usually results in an inductor with lower saturation current.

The total losses of the coil consist of both the losses in the DC resistance, $R_{(DC)}$, and the following frequencydependent components:

- The losses in the core material (magnetic hysteresis loss, especially at high switching frequencies)
- Additional losses in the conductor from the skin effect (current displacement at high frequencies)
- Magnetic field losses of the neighboring windings (proximity effect)
- Radiation losses

For good efficiency, the inductor's DC resistance should be less than 30mΩ. The following inductor series from different suppliers have been used with the TPS6128xA converters.

Table 5. List of Inductors

11.2.1.2.2 Output Capacitor

For the output capacitor, it is recommended to use small ceramic capacitors placed as close as possible to the VOUT and GND pins of the IC. If, for any reason, the application requires the use of large capacitors which can not be placed close to the IC, using a smaller ceramic capacitor in parallel to the large one is highly recommended. This small capacitor should be placed as close as possible to the V_{OUT} and GND pins of the IC. To get an estimate of the recommended minimum output capacitance, [Equation](#page-35-0) 10 can be used.

$$
C_{\text{MIN}} = \frac{I_{\text{OUT}} \times (V_{\text{OUT}} - V_{\text{IN}})}{f \times \Delta V \times V_{\text{OUT}}}
$$
\n(10)

Where f is the switching frequency which is 2.3MHz (typ.) and ΔV is the maximum allowed output ripple.

With a chosen ripple voltage of 20mV, a minimum effective capacitance of 10µF is needed. The total ripple is larger due to the ESR and ESL of the output capacitor. This additional component of the ripple can be calculated using [Equation](#page-35-1) 11

$$
\Delta V_{\text{OUT(ESR)}} = \text{ESR x} \left(\frac{I_{\text{OUT}}}{1 - D} + \frac{\Delta I_{\text{L}}}{2} \right)
$$
\n(11)

$$
\Delta V_{\text{OUT(ESL)}} = \text{ESL x} \left(\frac{I_{\text{OUT}}}{1 - D} + \frac{\Delta I_{\text{L}}}{2} - I_{\text{OUT}} \right) x \frac{1}{t_{\text{SW(RISE)}}}
$$
(12)

$$
\Delta V_{\text{OUT(ESL)}} = \text{ESL x} \left(\frac{I_{\text{OUT}}}{1 - D} - \frac{\Delta I_{\text{L}}}{2} - I_{\text{OUT}} \right) x \frac{1}{t_{\text{SW(FALL)}}}
$$
\n(13)

with:

- I_{OUT} = output current of the application
- $D =$ duty cycle
- ΔI_{L} = inductor ripple current
- $t_{SW(RISE)}$ = switch node rise time
- $t_{SW(FALL)}$ = switch node fall time
- $ESR =$ equivalent series resistance of the used output capacitor
- $ESL =$ equivalent series inductance of the used output capacitor

An MLCC capacitor with twice the value of the calculated minimum should be used due to DC bias effects. This is required to maintain control loop stability. The output capacitor requires either an X7R or X5R dielectric. Y5V and Z5U dielectric capacitors, aside from their wide variation in capacitance over temperature, become resistive at high frequencies. There are no additional requirements regarding minimum ESR. Larger capacitors cause lower output voltage ripple as well as lower output voltage drop during load transients.

In applications featuring high (pulsed) load currents (e.g. ≥2Amps), it is recommended to run the converter with a reasonable amount of effective output capacitance and low-ESL device, for instance x2 22µF X5R 6.3V (0603) MLCC capacitors connected in parallel with a 1µF X5R 6.3V (0306-2T) MLCC LL capacitor.

DC bias effect: high cap. ceramic capacitors exhibit DC bias effects, which have a strong influence on the device's effective capacitance. Therefore the right capacitor value has to be chosen carefully. Package size and voltage rating in combination with material are responsible for differences between the rated capacitor value and it's effective capacitance. For instance, a 10µF X5R 6.3V (0603) MLCC capacitor would typically show an effective capacitance of less than 5µF (under 3.5V bias condition, high temperature).

For RF Power Amplifier applications, the output capacitor loading is combined between the dc/dc converter and the RF Power Amplifier (x2 10µF X5R 6.3V (0603) + PA input cap 4.7µF X5R 6.3V (0402)) are recommended.

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High values of output capacitance are mainly achieved by putting capacitors in parallel. This reduces the overall series resistance (ESR) to very low values. This results in almost no voltage ripple at the output and; therefore, the regulation circuit has no voltage drop on which it can react.

11.2.1.2.3 Input Capacitor

Multilayer ceramic capacitors are an excellent choice for input decoupling of the step-up converter as they have extremely low ESR and are available in small footprints. Input capacitors should be located as close as possible to the device. While a 4.7μF input capacitor is sufficient for most applications, larger values may be used to reduce input current ripple without limitations.

Take care when using only ceramic input capacitors. When a ceramic capacitor is used at the input and the power is being supplied through long wires, such as from a wall adapter, a load step at the output can induce ringing at the VIN pin. This ringing can couple to the output and be mistaken as loop instability or could even damage the part. Additional "bulk" capacitance (electrolytic or tantalum) should in this circumstance be placed between C_1 and the power source lead to reduce ringing than can occur between the inductance of the power source leads and $C₁$.

11.2.1.2.4 Checking Loop Stability

The first step of circuit and stability evaluation is to look from a steady-state perspective at the following signals:

- Switching node, SW
- Inductor current, I_L
- Output ripple voltage, $V_{\text{OUT}(AC)}$

These are the basic signals that need to be measured when evaluating a switching converter. When the switching waveform shows large duty cycle jitter or the output voltage or inductor current shows oscillations, the regulation loop may be unstable. This is often a result of board layout and/or L-C combination.

As a next step in the evaluation of the regulation loop, the load transient response is tested. The time between the application of the load transient and the turn on of the P-channel MOSFET, the output capacitor must supply all of the current required by the load. V_{OUT} immediately shifts by an amount equal to $\Delta I_{(LOAD)}$ x ESR, where ESR is the effective series resistance of C_{OUT} . $\Delta I_{(LOAD)}$ begins to charge or discharge C_{OUT} generating a feedback error signal used by the regulator to return V_{OUT} to its steady-state value. The results are most easily interpreted when the device operates in PWM mode.

During this recovery time, V_{OUT} can be monitored for settling time, overshoot or ringing that helps judge the converter's stability. Without any ringing, the loop has usually more than 45° of phase margin. Because the damping factor of the circuitry is directly related to several resistive parameters (that is, MOSFET $r_{DS(on)}$) that are temperature dependant, the loop stability analysis has to be done over the input voltage range, load current range, and temperature range.

The TPS6128xA series of step-up converters have been optimized to operate with a effective inductance in the range of 200nH to 800nH and with output capacitors in the range of 8uF to 100µF. The internal compensation is optimized for an output filter of $L = 0.5\mu H$ and $C_O = 15\mu F$.

Table 6. Component List

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11.2.1.3 Application Performance Curves

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11.2.2 TPS61282 with 2.5V-4.35 VIN, 2000 mA Output Current (TPS61280 with I2C Programmable)

Figure 48. TPS6128x, Device Overview

11.2.2.1 Design Requirements

Table 7. Design Parameters

Table 8. Component List

11.2.2.2 Detailed Design Procedures

See *TPS61281 with 2.5V-4.35 VIN, 1500 mA Output Current (TPS61280 with I ²C [Programmable\)](#page-33-3)* for all Detailed Design Procedures.

11.2.2.3 Application Performance Curves

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12 Power Supply Recommendations

The devices are designed to operate from an input voltage supply range between 2.3 V and 4.8 V. This input supply should be well regulated. If the input supply is located more than a few inches from the TPS61280, TPS61281 or TPS61282 converter additional bulk capacitance may be required in addition to the ceramic bypass capacitors. An electrolytic or tantalum capacitor with a value of $47 \mu F$ is a typical choice.

13 Layout

13.1 Layout Guidelines

- For all switching power supplies, the layout is an important step in the design, especially at high peak currents and high switching frequencies.
- If the layout is not carefully done, the regulator could show stability problems as well as EMI problems.
- Therefore, use wide and short traces for the main current path and for the power ground tracks.
- To minimize voltage spikes at the converter's output:
	- Place the output capacitor(s) as close as possible to GND and V_{OUT} , as shown in [Figure](#page-45-4) 65.
	- The input capacitor and inductor should also be placed as close as possible to the IC.
	- Use a common ground node for power ground and a different one for control ground to minimize the effects of ground noise.
	- Connect these ground nodes at any place close to the ground pins of the IC.
	- Junction-to-ambient thermal resistance is highly application and board-layout dependent.
	- It is suggested to maximize the pour area for all planes other than SW. Especially the ground pour should be set to fill available PWB surface area and tied to internal layers with a cluster of thermal vias.

13.2 Layout Example

Figure 65. Suggested Layout (Top)

13.3 Thermal Consideration

Implementation of integrated circuits in low-profile and fine-pitch surface-mount packages typically requires special attention to power dissipation. Many system-dependent issues such as thermal coupling, airflow, added heat sinks and convection surfaces, and the presence of other heat-generating components affect the powerdissipation limits of a given component.

Three basic approaches for enhancing thermal performance are listed below:

- Improving the power dissipation capability of the PCB design
- Improving the thermal coupling of the component to the PCB
- Introducing airflow in the system

As power demand in portable designs is more and more important, designers must figure the best trade-off between efficiency, power dissipation and solution size. Due to integration and miniaturization, junction temperature can increase significantly which could lead to bad application behaviors (i.e. premature thermal shutdown or worst case reduce device reliability).

Junction-to-ambient thermal resistance is highly application and board-layout dependent. In applications where high maximum power dissipation exists, special care must be paid to thermal dissipation issues in board design. The device operating junction temperature (T_{J}) should be kept below 125°C.

EXAS **ISTRUMENTS**

14 Device and Documentation Support

14.1 Device Support

14.1.1 Third-Party Products Disclaimer

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14.2 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

Table 9. Related Links

14.3 Trademarks

NanoFree is a trademark of Texas Instruments. I²C is a trademark of NXP Semiconductors.

14.4 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

14.5 Glossary

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

15 Mechanical, Packaging, and Orderable Information

The following pages include mechanical packaging and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

15.1 Package Summary

Code:

- YM Year Month date code
- LLLL Lot trace code
- S Assembly site code

15.1.1 Chip Scale Package Dimensions

The TPS6128x device is available in a 16-bump chip scale package (YFF, NanoFree™). The package dimensions are given as:

- $D = ca. 1666 \pm 30 \mu m$
- $E = ca. 1666 \pm 30 \mu m$

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent>for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

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Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

PACKAGE OPTION ADDENDUM

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⁽⁶⁾ Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

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PACKAGE MATERIALS INFORMATION

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*All dimensions are nominal

NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994. B. This drawing is subject to change without notice.

C. NanoFree™ package configuration.

NanoFree is a trademark of Texas Instruments

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- Экспресс доставка в любую точку России;
- Техническая поддержка проекта, помощь в подборе аналогов, поставка прототипов;
- Система менеджмента качества сертифицирована по Международному стандарту ISO 9001;
- Лицензия ФСБ на осуществление работ с использованием сведений, составляющих государственную тайну;
- Поставка специализированных компонентов (Xilinx, Altera, Analog Devices, Intersil, Interpoint, Microsemi, Aeroflex, Peregrine, Syfer, Eurofarad, Texas Instrument, Miteq, Cobham, E2V, MA-COM, Hittite, Mini-Circuits,General Dynamics и др.);

Помимо этого, одним из направлений компании «ЭлектроПласт» является направление «Источники питания». Мы предлагаем Вам помощь Конструкторского отдела:

- Подбор оптимального решения, техническое обоснование при выборе компонента;
- Подбор аналогов;
- Консультации по применению компонента;
- Поставка образцов и прототипов;
- Техническая поддержка проекта;
- Защита от снятия компонента с производства.

Как с нами связаться

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