

Switched Capacitor Voltage Converter

FEATURES

- Charge Pump in 5-Pin SOT-23A Package
- >95% Voltage Conversion Efficiency
- Voltage Inversion and/or Doubling
- Low 38µA Quiescent Current
- Operates from +1.8V to +5.5V
- Up to 25mA Output Current
- Only Two External Capacitors Required
- Lower Power Version of TCM828

APPLICATIONS

- LCD Panel Bias
- Cellular Phones
- Pagers
- PDAs, Portable Dataloggers
- Battery-Powered Devices

PIN CONFIGURATION



TYPICAL OPERATING CIRCUIT



GENERAL DESCRIPTION

The TC828A is a CMOS "charge-pump" voltage converter in an ultra-small 5-Pin SOT-23A package. It can invert and/or double an input voltage that can range from +1.8V to +5.5V. Conversion efficiency is typically >95%, and switching frequency is 12KHz.

The external component requirement is only two capacitors (10μ F nominal) for standard voltage inverter applications. With a few additional components a positive doubler can also be built. All other circuitry, including control, oscillator, power MOSFETs are integrated on-chip. Supply current is 38μ A typically.

The TC828A is available in a 5-Pin SOT-23A surface mount package.

ORDERING INFORMATION

Part No.	Package	Temp. Range
TC828AECT	5-Pin SOT-23A	- 40°C to +85°C
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NOTE: 5-Pin SOT-23A is equivalent to EIAJ-SC74A.

ABSOLUTE MAXIMUM RATINGS*

Input Voltage (V _{IN} to GND)	+6.0V, - 0.3V
Output Voltage (OUT to GND)	6.0V, + 0.3V
Current at OUT Pin	50mA
Short-Circuit Duration - OUT to GND.	Indefinite
Operating Temperature Range	– 40°C to +85°C

Power Dissipation ($T_A \le 70^{\circ}C$)

ELECTRICAL CHARACTERISTICS: $T_A = -40^{\circ}C$ to $+85^{\circ}C$, $V_{IN} = +5V$, $C1 = C2 = 10 \ \mu$ F, unless otherwise noted. Typical values are at $T_A = +25^{\circ}C$.

Symbol	Parameter	Test Conditions	Min	Тур	Max	Unit
I _{DD}	Supply Current			38	80	μA
V ⁺	Minimum Supply Voltage	$R_{LOAD} = 1 \ K\Omega$	1.8	_	—	V
V ⁺	Maximum Supply Voltage	$R_{LOAD} = 1 \ K\Omega$	_	_	5.5	V
Fosc	Oscillator Frequency		6	12	20	KHz
P _{EFF}	Power Efficiency	$R_{LOAD} = 1 \text{ K}\Omega, T_A = +25^{\circ}\text{C}$	_	96		%
V _{EFF}	Voltage Conversion Efficiency	$R_{LOAD} = \infty$	95	99.9	-	%
R _{OUT}	Output Resistance	$I_{OUT} = 5 \text{ mA}, T_A = +25^{\circ}\text{C}$ $T_A = -40^{\circ}\text{C} \text{ to } +85^{\circ}\text{C}$	_	25 —	50 65	Ω

NOTE: 1. Capacitor contribution is approximately 20% of the output impedance [ESR = 1 / pump frequency x capacitance)]. 2. All – 40°C to +85°C specifications above are guaranteed by design.

PIN DESCRIPTION

Pin No. (5-Pin SOT-23A)	Symbol	Description	
1	OUT	Inverting charge pump output.	
2	V _{IN}	Positive power supply input.	
3	C ₁	Commutation capacitor negative terminal.	
4	GND	Ground.	
5	C ₁ ⁺	Commutation capacitor positive terminal.	

DETAILED DESCRIPTION

The TC828A charge pump converter inverts the voltage applied to the V_{IN} pin. Conversion consists of a two-phase operation (Figure 1). During the first phase, switches S2 and S4 are open and S1 and S3 are closed. During this time, C1 charges to the voltage on V_{IN} and load current is supplied from C2. During the second phase, S2 and S4 are closed, and S1 and S3 are open. This action connects C1 across C2, restoring charge to C2.



Figure 1. Ideal Switched Capacitor Charge Pump

APPLICATIONS INFORMATION

Output Voltage Considerations

The TC828A performs voltage conversion but does not provide *regulation*. The output voltage will droop in a linear manner with respect to load current. The value of this equivalent output resistance is approximately 25Ω nominal at +25°C and V_{IN} = +5V. V_{OUT} is approximately – 5V at light loads, and droops according to the equation below:

$$V_{DROOP} = I_{OUT} \times R_{OUT}$$

 $V_{OUT} = - (V_{IN} - V_{DROOP})$

Charge Pump Efficiency

The overall power efficiency of the charge pump is affected by four factors:

- (1) Losses from power consumed by the internal oscillator, switch drive, etc. (which vary with input voltage, temperature and oscillator frequency).
- (2) I²R losses due to the on-resistance of the MOSFET switches on-board the charge pump.
- (3) Charge pump capacitor losses due to effective series resistance (ESR).

(4) Losses that occur during charge transfer (from the commutation capacitor to the output capacitor) when a voltage difference between the two capacitors exists.

Most of the conversion losses are due to factors (2), (3) and (4) above. These losses are given by Equation 1.

$$P_{\text{LOSS}(2, 3, 4)} = I_{\text{OUT}}^{2} \times R_{\text{OUT}}$$
$$\cong I_{\text{OUT}}^{2} \times \left[\frac{1}{(f_{\text{OSC}}) \text{ C1}} + 8R_{\text{SWITCH}} + 4\text{ESR}_{\text{C1}} + \text{ESR}_{\text{C2}} \right]$$

Equation 1.

The $1/(f_{OSC})(C1)$ term in Equation 1 is the effective output resistance of an ideal switched capacitor circuit (Figures 2a, 2b).

The losses in the circuit due to factor (4) above are also shown in Equation 2. The output voltage ripple is given by Equation 3.

$$P_{\text{LOSS (4)}} = \left[(0.5)(\text{C1})(\text{V}_{\text{IN}}^2 - \text{V}_{\text{OUT}}^2) + (0.5)(\text{C2})(\text{V}_{\text{RIPPLE}}^2 - 2\text{V}_{\text{OUT}}\text{V}_{\text{RIPPLE}}) \right]_{\text{X}} \text{f}_{\text{OSC}}$$

Equation 2.

$$V_{\mathsf{RIPPLE}} = \frac{I_{\mathsf{OUT}}}{(f_{\mathsf{OSC}})(\mathsf{C2})} + 2(I_{\mathsf{OUT}})(\mathsf{ESR}_{\mathsf{C2}})$$





Figure 2a. Ideal Switched Capacitor Model



Figure 2b. Equivalent Output Resistance

Capacitor Selection

In order to maintain the lowest output resistance and output ripple voltage, it is recommended that low ESR capacitors be used. Additionally, larger values of C1 will lower the output resistance and larger values of C2 will reduce output ripple. (See Equation 1(b)).

Table 1 shows various values of C1 and the corresponding output resistance values @ +25°C. It assumes a 0.1 Ω ESR_{C1} and 2 Ω R_{SW}. Table 2 shows the output voltage ripple for various values of C2. The V_{RIPPLE} values assume 10mA output load current and 0.1 Ω ESR_{C2}.

Table 1. Output Resistance vs	. C1	(ESR =	= 0.1 Ω)
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R _{ουτ} (Ω)
850
100
42
25
18.3
17.3

Table 2. Output Voltage Ripple vs. C2 (ESR = 0.1Ω) I_{OUT} 10mA

C2(μF)	V _{RIPPLE} (mV)	
1	835	
3.3	254	
10	85	
47	19.7	
100	10.3	

Input Supply Bypassing

The V_{IN} input should be capacitively bypassed to reduce AC impedance and minimize noise effects due to the switching internal to the device. The recommended capacitor depends on the configuration of the TC828A.

If the device is loaded from OUT to GND it is recommended that a large value capacitor (at least equal to C1) be connected from the input to GND. If the device is loaded from IN to OUT a small (0.1 μF) capacitor from IN to OUT is sufficient.

Voltage Inverter

The most common application for charge pump devices is the inverter (Figure 3). This application uses two external capacitors – C1 and C2 (plus a power supply bypass capacitor, if necessary). The output is equal to $V_{\overline{IN}}$ plus any voltage drops due to loading. Refer to Table 1 and Table 2 for capacitor selection.



Figure 3. Test Circuit

Cascading Devices

Two or more TC828As can be cascaded to increase output voltage (Figure 4). If the output is lightly loaded, it will be close to $(-2 \times V_{IN})$ but will droop at least by R_{OUT} of the first device multiplied by the I_Q of the second. It can be seen that the output resistance rises rapidly for multiple cascaded devices. For large negative voltage requirements see the TC682 or TCM680 data sheets.



Figure 4. Cascading TC828As to Increase Output Voltage

Paralleling Devices

To reduce the value of R_{OUT} , multiple TC828As can be connected in parallel (Figure 5). The output resistance will be reduced by a factor of N where N is the number of TC828As. Each device will require it's own pump capacitor (C1), but all devices may share one reservoir capacitor (C2). However, to preserve ripple performance the value of C2 should be scaled according to the number of paralleled TC828As.



Figure 5. Paralleling TC828As to Reduce Output Resistance

Voltage Doubler/Inverter

Another common application of the TC828A is shown in Figure 6. This circuit performs two functions in combination. C1 and C2 form the standard inverter circuit described above. C3 and C4 plus the two diodes form the voltage doubler circuit. C1 and C3 are the pump capacitors and C2 and C4 are the reservoir capacitors. Because both subcircuits rely on the same switches if either output is loaded, both will droop toward GND. Make sure that the total current drawn from both the outputs does not total more than 40 mA.



Figure 6. Combined Doubler and Inverter

Diode Protection for Heavy Loads

When heavy loads require the OUT pin to sink large currents being delivered by a positive source, diode protection may be needed. The OUT pin should not be allowed to be pulled above ground. This is accomplished by connecting a Schottky diode (1N5817) as shown in Figure 7.

TC828A



Figure 7. High V⁻ Load Current

Layout Considerations

As with any switching power supply circuit good layout practice is recommended. Mount components as close together as possible to minimize stray inductance and capacitance. Also use a large ground plane to minimize noise leakage into other circuitry.

TYPICAL CHARACTERISTICS

Circuit of Figure 3, V_{IN} = +5V, C1 = C2 = C3, T_A = +25°C, unless otherwise noted.



TYPICAL CHARACTERISTICS (Cont.)

Circuit of Figure 3, V_{IN} = +5V, C1 = C2 = C3, T_A = +25°C, unless otherwise noted.





TAPING FORM



Switched Capacitor Voltage Converters

TC828A



Part Numbers and Part Marking

 & 2 = part number code + temperature range (two-digit code).

TC828A	Code		
TC828AECT	CC		

ex: 828ECT = ©©))

PACKAGE DIMENSIONS



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