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## Datasheet

### **AS1364 1A Low Dropout Linear Voltage Regulator**

### **1 General Description**

The AS1364 is a low-dropout linear regulator (LDO) designed to operate from 2V to 5.5V input, that delivers a wide range of highly accurate (±0.75%) factory-trimmed output voltages as well as adjustable output voltages (using an external resistor-divider network).

The ultra-low dropout device requires only 140mV dropout voltage while delivering a guaranteed 1A load current and is therefore perfectly suited for battery-operated portable applications.

Additionally the AS1364 offers extremely low 10µVRMS (100Hz to 100kHz) or 45µVRMS (10Hz to 1MHz) output voltage noise.

*Table 1. Standard Products*



The device features an internal PMOS pass transistor (for a low supply current of only 35µA), reset output, a low-power shutdown mode, and protection from short-circuit and thermal-overload conditions.

When in shutdown, a  $5k\Omega$  (typ) discharge path is connected between the output pin and ground. The AS1364 is available in a 8-pin TDFN 3x3mm package.

### **2 Key Features**

- Guaranteed Output Current: 1A
- Low Dropout: 140mV @ 1A
- $\blacksquare$  Output Voltage Accuracy: Up to  $\pm 0.75\%$

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- 2.0V to 5.5V Input Voltage
- Fixed VOUT: 1.2V to 5.0V
- Adjustable VOUT: 1.2V to 5.3V
- Low Ground Current: 35µA
- Low Shutdown Current: 10nA
- Low Output Noise: 45µVRMS (from 10Hz to 1MHz)
- Thermal Overload Protection
- Output Current Limit
- Output discharge path during shutdown
- 8-pin TDFN 3x3mm Package

### **3 Applications**

The device is ideal for laptops, PDAs, portable audio devices, mobile phones, cordless phones, and any other battery-operated portable device.



<span id="page-1-1"></span><span id="page-1-0"></span>*Figure 1. AS1364 - Typical Application Diagram*

### **4 Pin Assignments**

*Figure 2. Pin Assignments (Top View)*



#### **4.1 Pin Descriptions**

#### *Table 2. Pin Descriptions*



### **5 Absolute Maximum Ratings**

Stresses beyond those listed in [Table 3](#page-3-0) may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in [Electrical Characteristics on page 4](#page-4-0) is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### <span id="page-3-0"></span>*Table 3. Absolute Maximum Ratings*



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### <span id="page-4-0"></span>**6 Electrical Characteristics**

**Note:** All limits are guaranteed. The parameters with min and max values are guaranteed by production tests or SQC (Statistical Quality Control) methods.

VIN = VOUT(NOM) + 500mV or VIN = +2.0V (whichever is greater), CIN = COUT = 4.7µF, EN = IN, TAMB = -40°C to +85°C (unless otherwise *specified). Typical values are at TAMB = +25*ºC*.*









1. Guaranteed by production test of load regulation and line regulation.

2. Dropout voltage is defined as VIN - VOUT, when VOUT is 100mV below the value of VOUT measured for VIN = (VOUT(NOM) + 500mV). Since the minimum input voltage is 2.0V, this specification is only valid when VOUT(NOM) > 2.0V. 1. Guaranteed by production test of load regulation and line regulation.<br>
2. Dropout voltage is defined as VIN - VOUT, when VOUT is 100mV below the value<br>
Since the minimum input voltage is 2.0V, this specification is only

### **7 Typical Operating Characteristics**

VIN = VOUT(NOM) + 0.5V, CIN = COUT =  $4.7\mu$ F, TAMB =  $25^{\circ}$ C (unless otherwise specified).



Datasheet - Typical Operating Characteristics



*Figure 11. PSRR vs. Frequency; IOUT = 10mA*



*Figure 9. Quiescent Current vs. Temperature Figure 10. Spectral Noise vs. Freq; IOUT = 10mA*



#### *Figure 12. Line Transient Response; VIN = 3.8V to 4.3V, IOUT = 100mA*



*Figure 14. Startup; VIN = 3.8V, IOUT = 100mA Figure 15. Startup; VIN = 3.8V, IOUT = 100mA*



*Figure 13. Load Transient Response; VIN = 3.8V, IOUT = 50mA to 500mA*





### **8 Detailed Description**

The AS1364 output voltage is factory-trimmed or is adjustable from +1.2V to +5V, and is guaranteed to supply 1A of output current. The device consists of a +1.20V internal reference, error amplifier, MOSFET driver, P-channel pass transistor, internal feedback voltage-divider and a comparator [\(see Figure 16\).](#page-9-0)

<span id="page-9-0"></span>



Figure 16 shows the block diagram of the AS1364. It identifies the basics of a series linear regulator employing a P-Channel MOSFET as the control element. A stable voltage reference (1.2V REF in Figure 16) is compared with an attenuated sample of the output voltage. Any difference between the two voltages (reference and sample) creates an output from the error amplifier that drives the series control element to reduce the difference to a minimum. The error amplifier incorporates additional buffering to drive the relatively large gate capacitance of the series pass Pchannel MOSFET, when additional drive current is required under transient conditions. Input supply variations are absorbed by the series element, and output voltage variations with loading are absorbed by the low output impedance of the regulator.

When in shutdown, a  $5k\Omega$  discharge path is connected between the output terminal and ground.

Datasheet - Detailed Description

#### **8.1 Output Voltage Selection**

At the factory trimmed versions of the AS1364 offering the bypass pin [\(see Figure \),](#page-1-1) the output voltage is then set to an internally trimmed voltage [\(see Ordering Information on page 18\).](#page-18-0)

For the adjustable AS1364-AD, an output voltage between +1.2V and +5V can be set by using two external resistors [\(see Figure 17\).](#page-10-0) In this mode, VOUT is determined by:

$$
V_{OUT} = V_{SETBYP} \times \left(1 + \frac{R_1}{R_2}\right) \tag{EQ1}
$$

Where:

VSET/BYP = 1.2V ±0.03V

A simplification of R1 and R2 selection is:

$$
R_1 = R_2 \times \left(\frac{V_{OUT}}{V_{SETBYP}} - 1\right)
$$

*(EQ 2)*

Since the input bias current at SET is less than 100nA, large resistance values can be used for R1 and R2 to minimize power consumption and therefore increasing efficiency.

Note: Up to 125kΩ is acceptable for R2. If the SET pin is connected to GND without a resistor, 3.3V will be set as output voltage.

In preset voltage mode, the impedance from SET to GND should be less than  $10k\Omega$  or spurious conditions may cause the voltage at SET to exceed the 50mV threshold.

<span id="page-10-0"></span>*Figure 17. Adjustable Output Voltage Typical Application*



#### **8.2 Shutdown**

If pin EN is connected to GND the AS1364 is disabled. In shutdown mode all internal circuits are turned off, reducing supply current to 10nA (typ). For normal device operation pin EN must be connected to IN. During shutdown, POK goes low.

When in shutdown, a  $5k\Omega$  (typ) discharge path is connected between the output pin and ground.

#### **8.3 Power-OK**

The AS1364 features a power-ok indicator that asserts when the output voltage falls out of regulation. The open-drain POK output goes low when output voltage at OUT falls 6% below its nominal value. A 100k $\Omega$  pull-up resistor from POK to a (typically OUT) provides a logic control signal.

POK can be used as a power-on-reset (POR) signal to a microcontroller or can drive an external LED to indicate a power failure condition.

**Note:** POK is low during shutdown.

### **9 Application Information**

#### <span id="page-11-0"></span>**9.1 Dropout Voltage**

Dropout is the input to output voltage difference, below which the linear regulator ceases to regulate. At this point, the output voltage change follows the input voltage change. Dropout voltage may be measured at different currents and, in particular at the regulator maximum one. From this is obtained the MOSFET maximum series resistance over temperature etc. More generally:

$$
V_{DROPOUT} = I_{LOAD} \times R_{SERIES}
$$
 (EQ3)

Dropout is probably the most important specification when the regulator is used in a battery application. The dropout performance of the regulator defines the useful "end of life" of the battery before replacement or re-charge is required.

<span id="page-11-1"></span>



Figure 18 shows the variation of VOUT as VIN is varied for a certain load current. The practical value of dropout is the differential voltage (VOUT-VIN) measured at the point where the LDO output voltage has fallen by 100mV below the nominal, fully regulated output value. The nominal regulated output voltage of the LDO is that obtained when there is 500mV (or greater) input-output voltage differential.

#### **9.2 Efficiency**

Low quiescent current and low input-output voltage differential are important in battery applications amongst others, as the regulator efficiency is directly related to quiescent current and dropout voltage. Efficiency is given by:

$$
\text{Efficiency} = \frac{V_{LOAD} \times I_{LOAD}}{V_{IN}(I_Q + I_{LOAD})} \times 100\% \tag{EQ4}
$$

Where:  $I<sub>O</sub>$  = Quiescent current of LDO Datasheet - Application Information

#### <span id="page-12-0"></span>**9.3 Power Dissipation**

Maximum power dissipation (PD) of the LDO is the sum of the power dissipated by the internal series MOSFET and the quiescent current required to bias the internal voltage reference and the internal error amplifier, and is calculated as:

$$
PD_{(MAX)}(Seriespass) = I_{LOAD(MAX)}(V_{IN(MAX)} - V_{OUT(MIN)})
$$
Watts (EQ 5)

Internal power dissipation as a result of the bias current for the internal voltage reference and the error amplifier is calculated as:

$$
PD_{(MAX)}(Bias) = V_{IN(MAX)}I_Q
$$
 Watts (EQ6)

Total LDO power dissipation is calculated as:

$$
PD_{(MAX)}(Total) = PD_{(MAX)}(Seriespass) + PD_{(MAX)}(Bias)
$$
 Watts (EQ7)

#### **9.4 Junction Temperature**

Under all operating conditions, the maximum junction temperature should not be allowed to exceed 125ºC (unless the data sheet specifically allows). Limiting the maximum junction temperature requires knowledge of the heat path from junction to case ( $\theta_{\text{JC}}$ °C/W fixed by the IC manufacturer), and adjustment of the case to ambient heat path ( $\theta_{CA}$ °C/W) by manipulation of the PCB copper area adjacent to the IC position.

#### *Figure 19. Package Physical Arrangements*



*Figure 20. Steady State Heat Flow Equivalent Circuit*



Datasheet - Application Information

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#### *Total Thermal Path Resistance:*

$$
R\Theta_{JA} = R\Theta_{JC} + R\Theta_{CS} + R\Theta_{SA} \tag{EQ}
$$

Junction Temperature (TJ°C) is determined by:

$$
T_J = (PD_{(MAX)} \times R\Theta_{JA}) + T_{AMB} \text{ }^{\circ}\text{C}
$$
 (EQ9)

#### **9.5 Explanation of Steady State Specifications**

#### **9.5.1 Line Regulation**

Line regulation is defined as the change in output voltage when the input (or line) voltage is changed by a known quantity. It is a measure of the regulator's ability to maintain a constant output voltage when the input voltage changes. Line regulation is a measure of the DC open loop gain of the error amplifier. More generally: **9.5 Explanation of Staady State Specifications**<br> **9.5 Explanation of Staady State Specifications**<br>
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Line Regulation =  $\frac{\Delta V_{OUT}}{V}$  and is a pure number  $\frac{\Delta V_{OUT}}{\Delta V_{IN}}$ 

In practise, line regulation is referred to the regulator output voltage in terms of % / VOUT. This is particularly useful when the same regulator is available with numerous output voltage trim options.

Line Regulation = 
$$
\frac{\Delta V_{OUT}}{\Delta V_{IN}} \times \frac{100}{V_{OUT}} \%
$$
 // (EQ 10)

#### **9.5.2 Load Regulation**

Load regulation is defined as the change of the output voltage when the load current is changed by a known quantity. It is a measure of the regulator's ability to maintain a constant output voltage when the load changes. Load regulation is a measure of the DC closed loop output resistance of the regulator. More generally: im options.<br>
Line Regulation =  $\frac{\Delta V_{OUT}}{\Delta V_{IN}} \times \frac{100}{V_{OUT}}$ %/V<br>
of the output voltage when the load current is changed<br>
utput voltage when the load changes. Load regulation is<br>
y:<br>
Load Regulation =  $\frac{\Delta V_{OUT}}{\Delta I_{OUT}}$  and

$$
Load Regulation = \frac{\Delta V_{OUT}}{\Delta I_{OUT}} \text{ and is units of ohms } (\Omega) \tag{EQ 11}
$$

In practise, load regulation is referred to the regulator output voltage in terms of % / mA. This is particularly useful when the same regulator is available with numerous output voltage trim options.

$$
Load Regulation = \frac{\Delta V_{OUT}}{\Delta I_{OUT}} \times \frac{100}{\Delta V_{OUT}} %
$$
 % / mA\n
$$
(EQ12)
$$

#### **9.5.3 Setting Accuracy**

Accuracy of the final output voltage is determined by the accuracy of the ratio of R1 and R2, the reference accuracy and the input offset voltage of the error amplifier. When the regulator is supplied pre-trimmed, the output voltage accuracy is fully defined in the output voltage specification.

When the regulator has a SET terminal, the output voltage may be adjusted externally. In this case, the tolerance of the external resistor network must be incorporated into the final accuracy calculation. Generally:

$$
V_{OUT} = (V_{SET} \pm \Delta V_{SET}) \left( 1 + \frac{R1 \pm \Delta R1}{R2 \pm \Delta R2} \right)
$$
 (EQ 13)

The reference tolerance is given both at 25ºC and over the full operating temperature range.

#### **9.5.4 Total Accuracy**

Away from dropout, total steady state accuracy is the sum of setting accuracy, load regulation and line regulation. Generally:

*Total % Accuracy = Setting % Accuracy + Load Regulation % + Line Regulation % (EQ 14)*

#### **9.6 Explanation of Dynamic Specifications**

#### **9.6.1 Power Supply Rejection Ratio (PSRR)**

Known also as Ripple Rejection, this specification measures the ability of the regulator to reject noise and ripple beyond DC. PSRR is a summation of the individual rejections of the error amplifier, reference and AC leakage through the series pass transistor. The specification, in the form of a typical attenuation plot with respect to frequency, shows up the gain bandwidth compromises forced upon the designer in low quiescent current conditions. Generally:

$$
PSSR = 20Log \frac{\delta V_{OUT}}{\delta V_{IN}} \text{ dB using lower case } \delta \text{ to indicate AC values}
$$
 (EQ 15)

Power supply rejection ratio is fixed by the internal design of the regulator. Additional rejection must be provided externally.

#### **9.6.2 Output Capacitor ESR**

The series regulator is a negative feedback amplifier, and as such is conditionally stable. The ESR of the output capacitor is usually used to cancel one of the open loop poles of the error amplifier in order to produce a single pole response. Excessive ESR values may actually cause instability by excessive changes to the closed loop unity gain frequency crossover point. The range of ESR values for stability is usually shown either by a plot of stable ESR versus load current, or a limit statement in the datasheet. o-tenent current contents. Generally<br>
The state of t

Some ceramic capacitors exhibit large capacitance and ESR variations with temperature. Z5U and Y5V capacitors may be required to ensure stability at temperatures below TAMB = -10°C. With X7R or X5R capacitors, a 4.7µF capacitor should be sufficient at all operating temperatures.

Larger output capacitor values (10µF max) help to reduce noise and improve load transient-response, stability and power-supply rejection.

#### **9.6.3 Input Capacitor**

An input capacitor at VIN is required for stability. It is recommended that a 4.7µF capacitor be connected between the AS1364 power supply input pin VIN and ground (capacitance value may be increased without limit subject to ESR limits). This capacitor must be located at a distance of not more than 1cm from the VIN pin and returned to a clean analog ground. Any good quality ceramic, tantalum, or film capacitor may be used at the input. pacitance and ESR variations with temperature. Z5U ar<br>10°C. With X7R or X5R capacitors, a 4.7µF capacitor sh<br>x) help to reduce noise and improve load transient-respectible<br>tability. It is recommended that a 4.7µF capacitor

#### **9.6.4 Noise**

The regulator output is a DC voltage with noise superimposed on the output. The noise comes from three sources; the reference, the error amplifier input stage, and the output voltage setting resistors. Noise is a random fluctuation and if not minimized in some applications, will produce system problems.

#### **9.6.5 Transient Response**

The series regulator is a negative feedback system, and therefore any change at the output will take a finite time to be corrected by the error loop. This "propagation time" is related to the bandwidth of the error loop. The initial response to an output transient comes from the output capacitance, and during this time, ESR is the dominant mechanism causing voltage transients at the output. More generally:

$$
\delta V_{TRANSIENT} = \delta I_{OUTPUT} \times R_{ESR}
$$
 Units are Volts, Amps, Ohms. (EQ 16)

Thus an initial +50mA change of output current will produce a -12mV transient when the  $ESR=240$ m $\Omega$ . Remember to keep the ESR within stability recommendations when reducing ESR by adding multiple parallel output capacitors.

After the initial ESR transient, there follows a voltage droop during the time that the LDO feedback loop takes to respond to the output change. This drift is approx. linear in time and sums with the ESR contribution to make a total transient variation at the output of:

$$
\delta V_{TRANSIENT} = \delta I_{OUTPUT} \times \left(R_{ESR} + \frac{T}{C_{LOAD}}\right)
$$
 Units are Volts, Seconds, Farads, Ohms. (EQ 17)

Where:

CLOAD is output capacitor

T = Propagation delay of the LDO

This shows why it is convenient to increase the output capacitor value for a better support for fast load changes. Of course the formula holds for t < "propagation time", so that a faster LDO needs a smaller cap at the load to achieve a similar transient response. For instance 50mA load current step produces 50mV output drop if the LDO response is 1usec and the load cap is 1µF.

There is also a steady state error caused by the finite output impedance of the regulator. This is derived from the load regulation specification discussed above.

Datasheet - Application Information

#### **9.6.6 Turn On Time**

This specification defines the time taken for the LDO to awake from shutdown. The time is measured from the release of the enable pin to the time that the output voltage is within 5% of the final value. It assumes that the voltage at VIN is stable and within the regulator Min and Max limits. Shutdown reduces the quiescent current to very low, mostly leakage values (<1µA).

#### **9.6.7 Thermal Protection**

To prevent operation under extreme fault conditions, such as a permanent short circuit at the output, thermal protection is built into the device. Die temperature is measured, and when a 170°C (AS1364) threshold is reached, the device enters shutdown. When the die cools sufficiently, the device will restart (assuming input voltage exists and the device is enabled). Hysteresis of 20ºC prevents low frequency oscillation between startup and shutdown around the temperature threshold. **Technique in a metric wall and the content start in a metric wall in a content start in a metric wall in a metric of the content start in a metric of the content start in a metric of the content start in a metric of the c** 

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### **10 Package Drawings and Markings**

The device is available in an 8-pin TDFN 3x3mm package.

<span id="page-16-0"></span>*Figure 21. 8-pin TDFN 3x3mm Package*









#### **Notes:**

- 1. Figure 21 is shown for illustration only.
- 2. All dimensions are in millimeters; angles in degrees.
- 3. Dimensioning and tolerancing conform to *ASME Y14.5 M-1994*.
- 4. N is the total number of terminals.

5. The terminal #1 identifier and terminal numbering convention shall conform to *JEDEC 95-1, SPP-012*. Details of terminal #1 identifier are optional, but must be located within the zone indicated. The terminal #1 identifier may be either a mold or marked feature.

- 6. Dimension b applies to metallized terminal and is measured between 0.15mm and 0.30mm from the terminal tip.
- 7. ND refers to the maximum number of terminals on side D.
- 8. Unilateral coplanarity zone applies to the exposed heat sink slug as well as the terminals

#### **Revision History**



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**Note:** Typos may not be explicitly mentioned under revision history.

### <span id="page-18-0"></span>**11 Ordering Information**

The device is available as the standard products shown in [Table 5](#page-18-1).

#### <span id="page-18-1"></span>*Table 5. Ordering Information*



#### \*Future product.

Non-standard devices are available between 1.4V and 4.6V in 50mV steps and between 4.6V and 5.0V in 100mV steps. For more information and inquiries contact http://www.austriamicrosystems.com/contact

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